of the rapid changes this value must be taken to be the LMT for the Greenwich meridian and must be corrected for longitude. The longitude correction to apply is given by:

daily change × longitude 360

The longitude correction may also be obtained from Table II which is directly under Table I referred to above. After correction of the LMT the longitude in time must be applied to get the UT as for the sun.

Procedure

1. Extract the LMT tabulated for the date in question interpolating for latitude using Table I.

2. Extract the LMT for the following day if in west longitude or the preceding day if in east longitude and find the daily change.

3. Find the longitude correction from the formula above or from Table II.

4. Apply the longitude correction to the LMT in 1 normally adding if in west longitude and subtracting in east longitude. (This applies only if the times are getting later each day as is usually the case, but if not the rules must be reversed.) The result should always lie between the values found in 1 and 2.

5. Apply longitude in time +ve for west longitude and -ve for east longitude to give the UT.

Example 1

Find the UT of moonrise on 9th January to an observer in position 20° 30′ S 100° 00′ E

LMT moonrise 9th long 0 LMT moonrise 8th long 0 difference	11h 17m (interpolating for latitude 10h 28m between 20 and 30) 49m
longitude correction $\frac{(49\times100)}{360}$	14m
LMT moonrise 9th long 0 longitude correction LMT moonrise 9th long 100 E longitude in time UT	11h 17m

Example 2

Find the UT of moonset on 28th June to an observer in position 33° N 170° W

LMT moonset 28th long 0 LMT moonset 29th long 0	18h 25m 19h 21m
difference	56m
longitude correction $\frac{56 \times 170}{360}$	26m
LMT moonset 26th long 0	18h 25m
longitude correction	26m
LMT moonset 26th long 170 W	18h 51m
longitude in time	11h 20m
UT	30h 11m 28th
=	06h 11m 29th

For the purpose of the amplitude problem there is no reason why the UT cannot be read from the chronometer at the moment when the body is seen to be rising or setting.

Procedure

- 1. Obtain LMT and UT of rising (or setting) from the almanac.
- 2. Take the declination for the time of the UT from the almanac.
- 3. Observe the compass bearing at the time of rising or setting.
- 4. Obtain the true amplitude by calculator from the formula (or from amplitude tables).
- 5. Convert the amplitude to a bearing and compare with the observed compass bearing.

Example 1

On 1st November in DR position 36° 10′ N 28° 20′ W at 06h 22m LMT the sun rose bearing 102° C. Find the true amplitude and the error of the compass. If the variation was 3°W find the deviation for the ship's head.

LMT sunrise 1st	06h 22m	declination 07h	14° 19.9′ S
Longitude in time	01h 53m	d corr	+0.2'
UT	08h 15m	declination	14° 20.1′ S

sine amplitude =
$$\sin 14^{\circ} 20.1' \sec 36^{\circ} 10'$$

amplitude = 17.9

true amplitude = E 17.9° S true bearing $=107.9^{\circ}$ compass brg $=102^{\circ}$ compass error = 5.9° E $= 3.0^{\circ} \text{ W}$ variation $= 8.9^{\circ} E$ deviation

Example 2

On 8th January at ship in position 30° 45' S 166° 15' W, the sun set bearing 240° by compass. If the variation was 6°E find the compass error and the deviation for the ship's head.

LMT sunset lat 30 S 8th 19h 06m diff=12m Table I corr +01mLMT sunset lat 30 45' S 19h 07m longitude in time 11h 05m 06h 12m 9th Jan. declination 22° 09.3′ S UT d corr declination 22° 09.2′ S

sin amplitude = sine declination sec latitude \sin amplitude = $\sin 22^{\circ} 09.2' \sec 30^{\circ} 45'$ $=26^{\circ} 01.5'$

true amplitude = W 26° S true bearing $=244^{\circ}$ compass brg $= 240^{\circ}$ compass error = 4° E variation deviation

EXERCISE 2.3.3

- 1. On 30th September in DR position 20° 52' N 153° 10' W, the sun rose bearing 089° C. Find the error of the compass.
- 2. On 19th September the observed bearing by compass of sunrise was 085. DR position 39° 53' N 51° 00' E. Find the error of the compass and the deviation for the ship's head if the variation was 5° E.
- 3. On 27th June at the ship in DR position 40° 20' S 00° 00', the sun set bearing 301° C. Find the error of the compass and the deviation if the variation was 6° W.

- 4. On 18th December at a ship in DR position 38° 30'N 32° 15'W the sun rose bearing 126°C. Find the error of the compass.
- 5. On 5th January the sun set bearing 235° by gyro compass to an observer in DR position 49° 10' S 98° 45' W. Find the error of the gyro.
- 6. On 28th June the sun rose bearing 060° by gyro to an observer in position 42° 30' N 142° 30' W. Find the error of the gyro.

MODULE 2.4

Altitude and Azimuth. Correction of Altitudes

Definitions (see Figure 2.4.1)

Visible Horizon. This is the circle which bounds the observer's view of the earth's surface in a clear atmosphere. The range of the visible horizon will depend upon the observer's height of eye.

Sensible Horizon. This is a plane which passes through the observer's eye and is at right angles to the vertical of the observer.

Rational Horizon. This is the plane which passes through the centre of the earth and is at right angles to the observer's vertical and therefore parallel to the sensible horizon.

Zenith. The point on the celestial sphere directly above the observer.

Nadir. The point on the celestial sphere diametrically opposed to the zenith.

Vertical circle. A great circle passing through the zenith and the nadir, hence cutting the rational horizon in a right angle.

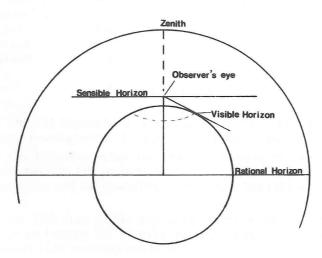


Fig. 2.4.1

The coordinates used to define a position on the celestial sphere with reference to an observer on the earth are altitude and azimuth. These can be measured by the observer, the altitude with a sextant and the azimuth with a compass.

The true altitude is defined as the angle at the centre of the earth between the plane of the rational horizon and a line joining the centre of the earth to the body. Alternatively it can be defined as the arc of a vertical circle between the body and the rational horizon. The zenith distance of the body is the arc of the vertical circle between the body and the zenith and will be equal to (90° – true altitude).

The azimuth is defined as the arc of the horizon between the vertical circle through the elevated pole and the vertical circle passing through the body. Thus the terms azimuth and bearing are stating the same thing in different ways (see Module 2.3).

The true altitude (or zenith distance) and the azimuth define the position of the body unambiguously with reference to the observer. This is referred to as the Horizon system of coordinates.

Conversion between the horizon system and the equinoctial system. The essential element of the methods of sight reduction to find the observer's position on the earth, which will be discussed in Module 2.7, is a conversion between the horizon system coordinates of altitude and azimuth and the equinoctial system of declination and hour angle (LHA). This may be done by the solution of a spherical triangle formed by the intersection of the three great circles:

- (i) the observer's meridian
- (ii) the meridian through the body
- (iii) the vertical circle through the body.

In Figure 2.4.2 this triangle is shown as triangle PZX, P being the pole, Z the zenith of an observer in latitude 50° N and X, a body with northerly declination.

The sides of the triangle will be the observer's co-lat (90°-latitude), the co-dec of the body (90°-declination) and the zenith distance of the body.

The main object of celestial navigation is to find the observer's position. The side PZ would enable the latitude to be known and the angle P (LHA) would enable the longitude to be found from the GHA. However three parts of the triangle must be known for a solution and without knowing the observer's position only one

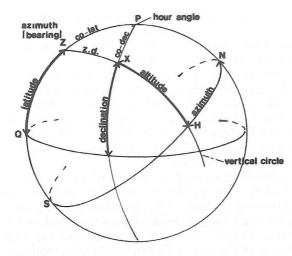


Fig. 2.4.2

part is actually known, that is the side PX or (90°-declination). However the side ZX can be measured or more correctly it can be found from the true altitude. But a third part of the triangle is still required. The azimuth can be measured with a compass but alas not with sufficient accuracy to be used for this purpose. The way in which this problem is dealt with is the subject of Module 2.7. The rest of this module is concerned with the way in which the true altitude and zenith distance are obtained from the sextant observation of a bodies altitude above the visible horizon.

Observed altitude

If an observer measures the altitude of a heavenly body he will measure the angle at his eye between a line from the eye to the body observed, and a line from the eye to the visible horizon directly beneath the body. This is referred to as the observed altitude and will be obtained from the sextant altitude with any error of the sextant allowed for (index error).

This is defined as the angle at the observer's eye between the plane of the sensible horizon and a line joining the observer's eye to the visible horizon, or alternatively the depression of the visible horizon below the sensible horizon.

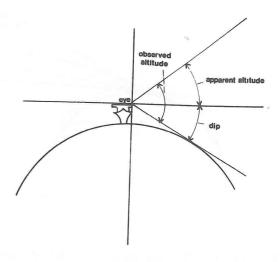


Fig. 2.4.3

The dip is subtracted from the observed altitude to give an altitude above the sensible horizon. The observed altitude corrected for dip is called the apparent altitude. This is illustrated in Figure 2.4.3.

It should be apparent from Figure 2.4.3 that:

apparent altitude = observed altitude - dip

Dip is always negative and must be applied to altitudes of all bodies. Values of dip are tabulated against height of eye in nautical tables and also in the Nautical Almanac. The table in the Nautical Almanac is usually the most convenient to use.

It should be noted that the value of the dip is affected by the amount of refraction of the observer's line of sight to his horizon. Uncertainty in the amount of refraction makes the dip correction the least accurate of all the corrections to altitude. Dip tables are based upon the formula:

 $dip = 1.77\sqrt{h}$ (where h is the observer's height of eye in metres)

Refraction

A ray of light entering a medium of greater density than that in which it has been travelling will be bent or refracted towards the

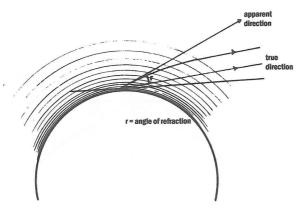


Fig. 2.4.4

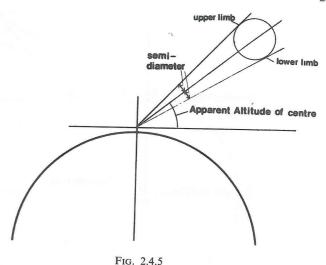
normal. The normal is the perpendicular to the interface between the two mediums at the point of entry of the light.

Light entering the earth's atmosphere from the celestial body is entering a progressively more dense medium as it approaches the earth's surface. The light is therefore being continually refracted as it travels through the atmosphere. This causes the light to be coming apparently from a higher altitude than is really the case. This is shown in Figure 2.4.4. The correction for refraction is therefore negative. The refraction is greatest at low altitudes and decreases to zero when the light is entering the atmosphere at 90°, that is from the zenith. Uncertainty in the amount of refraction makes it inadvisable to take low altitude observations unless unavoidable.

Values for the refraction are tabulated against altitude in nautical tables. The correction is applied to the altitude of all bodies.

Semi Diameter

In the case of the sun and moon it is easier and more accurate to observe the altitude of the upper or lower edge or limb of the body than to observe the estimated centre of the body. A correction for the radius of the visible disc must therefore be applied to obtain the altitude of the centre of the body. This correction is called the semi diameter. The value will be the angle at the observer's eye subtended by the radius of the body. From Figure 2.4.5 it can be seen that the correction will be positive if the lower limb is observed and negative if the upper limb is observed.



Semi diameter varies as the distance of the body from the earth and therefore will change due to the elliptical orbits of the earth around the sun and the moon around the earth. Values are given in the daily pages of the Nautical Almanac at the foot of the appropriate columns. One value is given for the sun for the three days on the page, but three values are given for the moon. The values are in minutes of arc.

There is no semi diameter correction for stars or planets.

Parallax

This is defined as the angle at the centre of the body subtended by a line from the centre of the earth and a line to the observer's eye. The parallax is maximum when the body is on the sensible horizon and then is called the **Horizontal Parallax**.

The application of the parallax corrects the altitude from that which is observed at the observer's position to that which would be observed at the centre of the earth, that is the true altitude.

In Figure 2.4.6

angle CSO is the angle of parallax, angle AOS is the apparent altitude uncorrected for parallax, angle ACH is the altitude after correction for parallax, that is the true altitude.

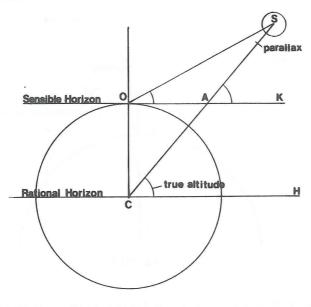


Fig. 2.4.6

Thus angle ACH = angle SAK and angle SAK = angle CSO + angle AOS (exterior angle of a triangle is equal to the two interior and opposite angles).

Thus true altitude = apparent altitude + parallax.

The parallax correction is always positive to the apparent altitude and its value will vary with the altitude, being maximum when the body is in the horizon and zero when the body is in the zenith.

Values for the sun are tabulated against altitude in nautical tables. Parallax must be applied to altitudes of the sun and moon, although the moon's parallax requires a further correction (see correction of the moon's altitude). There is no parallax correction necessary for stars due to their great distance. Planets parallax may sometimes be negligible but sometimes be considerable, sometimes greater than the sun. A planet's minimum parallax value will occur at conjunction (superior conjunction for an inferior planet). The maximum value will occur at opposition for a superior planet and inferior conjunction for an inferior planet. The parallax correction for a planet is conveniently ignored when correcting

altitudes by individual corrections, but it is allowed for in total correction tables which will be introduced at the end of this module.

Correction of the Moon's Altitude

Due to the proximity of the moon to the earth there are two additional corrections to the moon's altitude which are negligible for other bodies and are therefore ignored.

Reduction to the moon's horizontal parallax for latitude

The horizontal parallax for the moon is given in the daily pages for each hourly entry in the column headed H.P.

This is in fact the moon's equatorial horizontal parallax, that is the angle at the moon's centre subtended by the earth's equatorial radius. The oblate shape of the earth however means that the lesser polar radius will subtend a smaller angle. Thus the parallax must be reduced for latitude. This is shown in Figure 2.4.7.

The value of the 'Reduction to the Moon's Equatorial Horizontal Parallax for Latitude' is tabulated in nautical tables against latitude. The parallax in altitude can then be found by:

Parallax in altitude = horizontal parallax \times cos altitude.

The parallax in altitude is then added to the apparent altitude as for the sun.

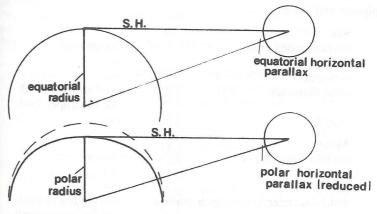


Fig. 2.4.7

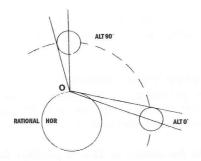


Fig. 2.4.8

Augmentation of the moon's semi diameter

The only variable which determines the semi diameter of any given body is its distance from the observer. A body will be closest to the observer when it is at his zenith, that is with altitude 90°. The distance and therefore the semi diameter decreases as the altitude decreases as illustrated in Figure 2.4.8. In the case of the sun the earth's radius is extremely small compared to the distance of the sun and therefore has a negligible effect. This is not so in the case of the moon. The values for semi diameter of the moon which are given in the almanac are for when the body is on the rational horizon, that is with altitude 0°. The Augmentation of the Moon's Semi-diameter is a positive correction to these values. The augmentation is tabulated in nautical tables against altitude.

To summarize the corrections required for the sun, the moon, the planets and stars

Sun	1,410,011,140
sextant index error	+ve or $-$ ve
dip	-ve
refraction	-ve
semi diameter	+ve for lower limb, -ve for upper limb
parallax	+ve
Moon	
sextant index error	+ve or -ve
dip distributed	-ve
refraction	-ve
semi-diameter after augmentation	+ve for lower limb, -ve for upper limb

parallax after reduction of the h.p. for latitude

Stars and Planets

sextant index error +ve or -ve dip -verefraction -ve

Example 1

If the sextant altitude of the sun's lower limb was 45° 20', sextant index error 1.2' on the arc, height of eye 15.4 metres and date 5th January, find the true altitude.

sext. alt.	$45^{\circ}\ 20.0'$	
i.e.	-1.2'	
obs. alt.	45° 18.8′	
dip	-6.9'	from table in almanac
app. alt.	45° 11.9′	
refr.	-0.9'	from table in Norie's Tables
	45° 11.0′	
semi diam.	+16.3'	from almanac for 5th Jan.
	45° 27.3′	
parallax	$\pm 0.1'$	from table in Norie's Tables
true alt.	45° 27.4′	

Example 2

The sextant altitude of the moon's lower limb was 36° 58.2'. Index error 0.8' off the arc. ht. of eye 5.4 metres. Date 8th January at 1200. DR position 32° 50′ N 34° 00′ W. Find the true altitude.

sextant altitude	36° 58.2′	semi-diameter	14.9'
index error	$\pm 0.8'$	augmentation	0.1'
observed altitude	36° 59.0′	semi diameter	15.0'
dip	-4.1'		
	36° 54.9′	equ. h.p.	54.8'
refraction	-1.3'	red for lat.	0.1'
	36° 53.6′	h.p.	54.7
semi diameter	$\pm 15.0'$	a tilbanasi 💎 🔻 🔻 🔻 💮 💮 💮 💮	
	37° 08.6′	parallax in alt. 5	4.7' cos alt.
parallax in alt.	+43.7'	=43.7'	
true altitude	37° 52.3′		

14 metres.

sextant alt.	29° 17.2′
index error	+1.8'
observed alt.	29° 19.0′
dip	-6.6'
•	29° 12.4′
refr.	-1.7'
true altitude	29° 10.7′

EXERCISE 2.4.1

Find the true altitude in the following cases using individual corrections. Answers given are worked using Burton's nautical tables.

Body	Sext. alt.	I.E. 2.2' on the arc	Ht. eye 8.3m	Date 4th Jan.
1. Sun LL	52° 31.2′			
2. Sun LL	33° 10.8′	1.0' off the arc	12.0m	27th June
3. Sun UL	71° 53.5′	1.8' off the arc	11.0m	20th Sept.
4. Sun UL	27° 46.7′	nil	7.7m	30th Sept.
5. Sun LL	62° 34.3′	2.2' off the arc	9.0m	18th Dec.
6. Sun UL	55° 55.8′	1.0' on the arc	7.4m	28th June

EXERCISE 2.4.2

Find the true altitude in the following cases using individual corrections.

Body	Sext. alt.	I.E.	Ht. eye
1. Altair	47° 29.6′	1.0' on the arc	11.2m
2. Canopus	32° 24.2′	0.8' on the arc	7.3m
3. Arcturus	21° 13.6′	0.4' off the arc	11.6m
4. Polaris	47° 15.8′	1.4' on the arc	15.3m
5. Dubhe	37° 10.4′	1.8' on the arc	8.4m

	6	Catron	100 17 0/	2.0/ 00.1	140
	0.	Saturn	12° 17.0′	2.0' off the arc	14.0m
	7.	Venus	53° 20.2′	0.6' on the arc	7.7m
	8.	Jupiter	23° 14.0′	2.2' off the arc	11.0m
	9.	Mars	51° 56.0′	0.4' on the arc	17.0m
į	10.	Venus	14° 38.2′	2.8' on the arc	9.9m

EXERCISE 2.4.3

Find the true altitude in the following cases using individual corrections.

Body	Sext. alt.	I.E.	Ht. eye (m)	Date (UT)	Latitude
1. Moon LL	63° 12.8′	1.6' off the arc	7.3	2200 18th Dec.	44° 56.3′ N
2. Moon LL	34° 14.8′	2.2' on the arc	13.0	0800 30th Sept.	34° 23.0′ S
3. Moon UL	58° 16.2′	1.0' on the arc	10.4	1900 19th Sept.	50° 00′ N
4. Moon UL	77° 51.6′	1.2' off the arc	14.8	1500 27th June	56° 30′ N
5. Moon LL	21° 38.8′	3.4' on the arc	11.5	0200 9th Jan.	23° 00′ S
6. Moon LL	$38^{\circ}\ 21.8'$	2.4' off the arc	9.0	1600 28th June	34° 30′ N
7. Moon UL	51° 17.0′	1.6' on the arc	16.0	1200 19th Sept.	$40^{\circ}~00'~N$
8. Moon LL	43° 18.4′	nil	13.7	0300 2nd Nov.	$2^{\circ}~00'~S$

Total Correction Tables

In practice correction of altitude is simplified by the use of total correction tables, which combine individual corrections. Nautical tables contain their own versions of total correction tables but the most commonly used, and described here, are the convenient tables included in the Nautical Almanac. These are in three tables, one for the sun, one for the moon, and one for the stars and planets. Each table is compiled with the apparent altitude as the argument so that the dip correction must be first applied to the observed altitude. A dip table is included.

The dip table is tabulated against height of eye and is based upon the formula:

$1.76\sqrt{\text{ht of eye in metres}}$

The table is arranged as a critical entry table which means that one value of the correction is given for an interval of the argument. This means that no interpolation is required and it should be remembered that if the height of eye is a tabulated value the upper of the two figures should be extracted. Thus a height of 13.0 metres gives a dip correction of −6.3′ (see extracts from Nautical Almanac).

Sun's total correction table

The sun's correction table found on the first page of the almanac. corrects for mean refraction, semi diameter and parallax. The argument is the apparent altitude, that is the observed altitude corrected for dip. Two separate tables are used, one for the months April to September and one for the months October to March. This allows for annual variations in the semi-diameter to be allowed for. Each table contains corrections for the lower limb in bold type and corrections for the upper limb observations in feint type. The tables are arranged as critical entry tables as described for the dip table. For example an argument of 51° 08' for the apparent altitude will give a correction of +15.5' for the lower limb in the October to March table, while a value of 50° 46' will give a correction of +15.4'.

Example

The sextant altitude of the sun's lower limb was 48° 56.3'. Index error 1.2' on the arc. Height of eye 7.2 metres. Date 16th June. Find the true altitude.

sextant altitude	48° 56.3′
index error	-1.2'
observed altitude	48° 55.1′
dip	-4.7'
apparent altitude	48° 50.4′
total correction	+15.1'
true altitude	49° 05.5′

Stars and planets

The correction table for stars and planets found on the first page of the almanac, corrects for the refraction only. Again it is arranged as a critical entry table with the argument apparent altitude, that is observed altitude corrected for the dip.

Additional corrections for planets are given for some dates and for some apparent altitudes. These correct for parallax when its value cannot be considered negligible.

Example

The sextant altitude of the star Procyon was 57° 18.9'. Index error 1.0' off the arc. Height of eye 6.5 metres. Find the true altitude.

sextant altitude	57° 18.9′
index error	+1.0'
observed altitude	57° 19.9′
dip	-4.5'
apparent altitude	57° 15.4′
total correction	-0.6'
true altitude	57° 14.8′

Example

The sextant altitude of the Venus on 1st December was 38° 06.5'. Index error 0.5' off the arc. Height of eye 5.0 metres. Find the true altitude.

sextant altitude	38° 06.5′
index error	$\pm 0.5'$
observed altitude	38° 07.0′
dip	-3.9'
apparent altitude	38° 03.1′
total correction	-1.2'
	38° 01.9′
additional correction	-+0.3'
true altitude	38° 02.2′

Moon's total correction table

The moon's total correction table is found on the last pages of the almanac and is in two parts. The main correction in the upper part of the table corrects for refraction, semi diameter and parallax, using mean values. It is tabulated against apparent altitude and some interpolation is required to obtain the accuracy to within one decimal place.

The second correction allows for variations in the semi diameter and parallax, both of which depend upon the horizontal parallax. The arguments are therefore apparent altitude and horizontal parallax. Two values are given one for lower limb and one for upper limb observations. They are arranged in columns the correction being taken from the same column as that from which the main correction was taken, and against the H.P.

All corrections for the moon are additive to the apparent altitude but those for the upper limb observations have had 30' added to them to maintain them positive. This 30' must therefore be subtracted from the final result.

Example

The sextant altitude of the moon's lower limb was 16° 58.2′. Index error 10.8′ off the arc. Height of eye 5.4 metres. GMT 1400 on 27th June. Find the true altitude.

from the almanac H.P.	54.5′
sextant altitude	16° 58.2′
index error	+0.8'
observed altitude	16° 59.0′
dip	-4.1'
apparent altitude	16° 54.9′
main correction	+62.7'
second correction	+1.1'
true altitude	17° 58.7′

Exercises 4, 5 and 6 are the same as exercises 1, 2 and 3 but to be worked with total correction tables. Answers given have been found using the correction tables in the almanac. Small variations may be found between solutions using individual corrections and total corrections.

EXERCISE 2.4.4

Find the true altitude in the following cases using total corrections.

Body	Sext. alt.	I.E.	Ht. eye	Date
1. Sun LL	52° 31.2′	2.2' on the arc	8.3m	4th Jan.
2. Sun LL	33° 10.8′	1.0' off the arc	12.0m	27th June
3. Sun UL	71° 53.5′	1.8' off the arc	11.0m	20th Sept.
4. Sun UL	27° 46.7′	nil	7.7m	30th Sept.
5. Sun LL	62° 34.3′	2.2' off the arc	9.0m	18th Dec.
6. Sun UL	55° 55.8′	1.0' on the arc	7.4m	28th June

EXERCISE 2.4.5

Find the true altitude in the following cases using total corrections.

Body	Sext. alt.	I.E.	Ht. eye
1. Altair	47° 29.6′	1.0' on the arc	11.2m
2. Canopus	32° 24.2′	0.8' on the arc	7.3m
3. Arcturus	21° 13.6′	0.4' off the arc	11.6m
4. Polaris	47° 15.8′	1.4' on the arc	15.3m
5. Dubhe	37° 10.4′	1.8' on the arc	8.4m
6. Saturn	12° 17.0′	2.0' off the arc	14.0m
7. Venus	53° 20.2′	0.6' on the arc	7.7m
8. Jupiter	23° 14.0′	2.2' off the arc	11.0m
9. Mars	51° 56.0′	0.4' on the arc	17.0m
10. Venus	14° 38.2′	2.8' on the arc	9.9m

EXERCISE 2.4.6

Find the true altitude in the following cases using total corrections.

Body	Sext. alt.	I.E.	Ht. eye (m)	Date (UT)
1. Moon LL	63° 12.8′	1.6' off the arc	7.3	2200 18th Dec.
2. Moon LL	34° 14.8′	2.2' on the arc	13.0	0800 30th Sept.
3. Moon UL	58° 16.2′	1.0' on the arc	10.4	1900 19th Sept.
4. Moon UL	77° 51.6′	1.2' off the arc	14.8	1500 27th June
5. Moon LL	21° 38.8′	3.4' on the arc	11.5	0200 9th Jan.
6. Moon LL	$38^{\circ} 21.8'$	2.4' off the arc	9.0	1600 28th June
7. Moon UL	51° 17.0′	1.6' on the arc	16.0	1200 19th Sept.
8. Moon LL	43° 18.4′	nil	13.7	0300 2nd Nov.

MODULE 2.5

Position Lines and Position Circles

One timed observation of the altitude of a heavenly body will give a position circle. There will be many positions from which the same altitude would be observed at any one time. If all these positions were joined they would form a circle on the earth's surface and this circle could be drawn around the geographical position of the body as shown in Figure 2.5.1. The radius of the circle as measured as an arc along the earth's surface is the zenith distance (90° – true altitude). To obtain a position we will need at least two observations of two different bodies so that the two position circles intersect to define the observer's position.

It is not practical to simply draw the circle or circles on a chart. The scale of the chart would have to be far too small, and such large circles would be distorted by the projection of the chart.

If one position circle is considered then although we do not know at which point on the circle the ship lies, we can say fairly confidently that it will be reasonably close to the DR position. Furthermore the area over which the ship is likely to be should be small compared to the radius of the circle (as long as the body observed is not too close to the zenith), and over this small area the curve of the position circle can be represented by a straight line without too much error. The problem becomes to find a position

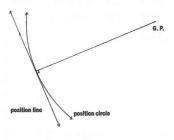


Fig. 2.5.1

through which the position line passes and the direction in which it runs at that position, so that it can be drawn on a navigator's chart and used as a position line. The direction of the position line will be perpendicular to the bearing of the body at the time of the observation which can be found as described in Module 2.3. The position through which it passes near to the DR position requires some calculation and there are various methods of obtaining this. The calculations will be dealt with in Module 2.7. Here we will concern ourselves only with the manipulation of the position lines.

The Intercept Method (Marcq St. Hilaire Method)

It may be said that the intercept method is the only method which the navigator needs to know as any observation may be worked by this method. The only case when it would not be used is the case when the body is bearing due north or due south when the calculations can be made much shorter and easier. This case will be dealt with in Module 2.6.

A position is assumed, probably the DR position but not necessarily so as long as it is reasonably close to the true position. Calculations are then made to find the zenith distance that would have been observed from that position. The bearing of the body is also calculated. If the ship was actually in the assumed position the position line could be drawn through it in a direction at right angles to the bearing. However by taking the real or true zenith distance from the observation, it will be seen whether the ship lies closer to or further away from the geographical position than the assumed position. If the true zenith distance is greater than the calculated zenith distance then the ship must be further from the geographical position than was assumed. If the true zenith distance is less than the calculated zenith distance then the ship must lie towards the geographical position from the assumed position. The difference between the true and calculated zenith distances is called the intercept and it is named either away or towards depending on the foregoing considerations.

The true position should be close enough to the assumed position that the true bearing may be taken to be the same as the calculated bearing. The calculated and the true position lines should therefore be parallel.

In practice only the true position line need be drawn. This is done by plotting the assumed position and drawing the intercept either towards or away from the body in the direction or

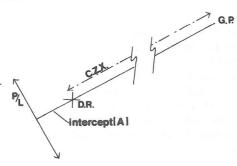


Fig. 2.5.2

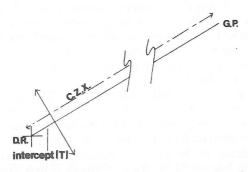


Fig. 2.5.3

reciprocal of the bearing, marking off the intercept along this line, and drawing the true position at right angles at this intercept terminal position. (ITP). Figure 2.5.2 shows a DR or assumed position with the GP. The distance between them will be the calculated zenith distance (CZX). The intercept is away (TZX greater than CZX). Similarly Figure 2.5.3 shows the intercept towards (TZX less than CZX).

It is necessary to plot only the intercept and true position line so that the plot for one observation may look like Figure 2.5.4.

If two such position lines are plotted to scale on a plotting sheet, the intersection of the two position lines can be taken to be the observed position and the latitude and longitude obtained by measuring its d'lat and d'long from the assumed position. It is sensible to use the same assumed position when calculating the two (or more) position lines.

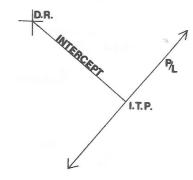


Fig. 2.5.4

To find the position by plotting the position lines of two simultaneous sights

Procedure

- 1. On a plotting sheet or graph paper plot a convenient point to represent the assumed position.
- 2. From this point draw the intercepts in the direction (if named towards), or in the opposite direction (if named away) of the respective bearings.
 - 3. Mark off along these lines the lengths of the intercepts.
- 4. Through the intercept terminal positions draw the position lines at right angles to the intercepts, and mark with a small circle where the two position lines cross.
- 5. Measure the d'lat and the departure between the assumed position and the plotted observed position.
- 6. Convert departure to d'long and apply d'lat and d'long to the assumed position to obtain the observed position.

Example 1

Two simultaneous observations, when worked using an assumed position of 52° 15′ N 40° 30′ W gave the following results:

> Observation 1; intercept 5.5' away, bearing 175° T. Observation 2; intercept 4.2' towards, bearing 250° T.

Find the ship's observed position. By measurement from Figure 2.5.5

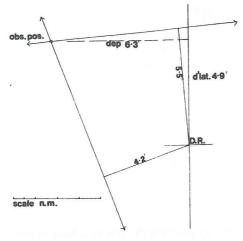


Fig. 2.5.5

d'lat =
$$4.9'$$
 N
dep = $6.3'$ W
d'long = 6.3 sec 52° 15'
= $10.3'$ W

assumed position		52° 15.0′ N			30.0′ W
45.00	d'lat	4.9' N	d'long		10.3′ W
observed position		52° 19.9′ N		40°	40.3′ W

In practice it is usual to observe if possible at least three bodies. More if available can be used as checks. This is the practice when taking star sights at morning and evening twilight. However it is rarely possible during daylight when the sun, sometimes the moon, and occasionally a planet are the only available bodies. In these circumstances transferred position lines are used to obtain positions.

Transferring the position line

During daylight hours if there is only one body available for observation, usually the sun, a position may be obtained by using a position line from one observation and transferring it to a later time by applying a course and distance run. At this later time the sun will have changed its bearing and another position line can be obtained to cross with the transferred or 'run up' position line. The transferred position line is marked by double arrows at each end. The run up position can be used as the assumed position for the second

observation so that the two position lines can be plotted from the same position. The running up of the first position is done by calculation so that it is not necessary to plot the run.

Example 2

From an observation of a body bearing 132°T an intercept of 6.2' towards is obtained, using an assumed position of 25° 18' S 38° 20' E. The ship then steamed 245° T for 45 miles when a second observation gave an intercept of 5.0' towards bearing 205° T. The DR position obtained by running up the first assumed position by plane sailing was used to calculate the second intercept. Find the ship's position at the time of the second observation.

Run 245 by 45 mi d'lat made good departure made	1	$45 \cos 245^\circ = 19.0' \text{ S}$ $45 \sin 245^\circ = 40.8' \text{ W}$
difference of lor	igitude	$40.8 \sec 25^{\circ} \ 28' = 45.2' \text{ W}$
assumed position d'lat DR position	25° 18.0′ S 19.0′ S 25° 37.0′ S	d'long 38° 20.0′ E 45.2′ W 37° 34.8′ E (Used as the assumed position for the second observation)

From Figure 2.5.6

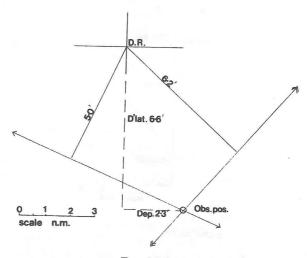


Fig. 2.5.6

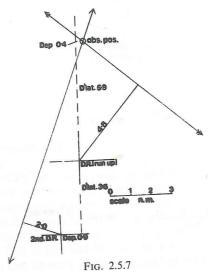
between the observed position and the DR

DR position d'lat	eparture = $2.3' \text{ E}$ $25^{\circ} 37.0' \text{ S}$ $\frac{6.6' \text{ S}}{25^{\circ} 43.6' \text{ S}}$	d'long = 2. d'long	3 sec 25° 37′ = 2.6′ E 37° 34.8′ E 2.6′ E 37° 37.4′ E
observed pos.	25° 43.0 S		5, 5,

Example 3

From an assumed position 32° 48'S 15° 35'W a body bearing 220° T was observed and an intercept of 4.8' away was calculated. The ship then steamed 335° T for 68 miles. A second observation then gave an intercept of 2.0' towards bearing 290°T using an assumed position of 31° 50′ S 16° 10′ W. Find the ship's position at the time of the second observation.

From Figure 2.5.7



between observed position and DR (run up) position:

$$\begin{array}{lll} \mbox{d'lat} = 5.9' \, \mbox{N} & \mbox{departure} = 0.4' \, \mbox{E} & \mbox{d'long} = 0.4 \, \mbox{sec} & 31^{\circ} & 46' = 0.5' \, \mbox{Run up position} & 31^{\circ} & 46.4' \, \mbox{S} & \\ \mbox{d'lat} & & \mbox{5.9' N} & \mbox{d'long} & \frac{16^{\circ} & 08.9' \, \mbox{W}}{16^{\circ} & 08.4' \, \mbox{W}} \\ \mbox{observed position} & & \mbox{31^{\circ}} & 40.5' \, \mbox{S} & \mbox{d'long} & \frac{0.5' \, \mbox{E}}{16^{\circ} & 08.4' \, \mbox{W}} \end{array}$$

It is common practice at sea to obtain a position line during the forenoon when the sun is bearing near to east and then run this position line up to the time of noon. The transferred position line would then be crossed with a latitude by meridian altitude (see Module 2.6). At this time the sun is bearing south or north and the position line runs east-west along a parallel of latitude. The full calculations for this problem are given in Module 2.7.

Longitude by chronometer method

It has been said that the intercept method can be used for all observations out of the meridian. The alternative longitude by chronometer method of reducing a sight has been popular in the past because the problem of finding a noon position by a forenoon observation of the sun combined with a meridian altitude can be done without any plotting with slightly less work than by the intercept method. It should be noted however that the method is not suitable for bodies which are close to the meridian when the bearing is close to north or south.

An assumed latitude is used, and the longitude in which the position line cuts that parallel is calculated (see Module 2.7). This is a position through which the position line passes albeit a different position from the intercept terminal position which is obtained by the intercept method. The bearing is calculated to give the direction of the position line at right angles to it. The plotting of the position line only requires the assumed latitude and the calculated longitude to be plotted and the position line drawn through it. If two observations are obtained simultaneously it makes sense to use the same latitude for both calculations, but clearly two different longitudes will be calculated.

Procedure

1. Plot the two positions through which the position lines pass. These two positions will be on the same parallel as long as the same latitude has been used for both calculations but a different longitude will result from each calculation. The departure will

have to be obtained between the two longitudes so that they are plotted in the correct position relative to each other.

2. Draw the two positions through their respective positions in

the appropriate directions.

3. Measure the d'lat and the departure between the observed position where the position lines cross and one of the other positions to obtain the latitude and longitude of the observed position.

Example 4

By using an assumed latitude of 49° 00′ N simultaneous observations of two stars gave longitudes of 9° 46.5′ W and 9° 52.4′ W bearing 135° T and 215° T respectively. Find the ship's position.

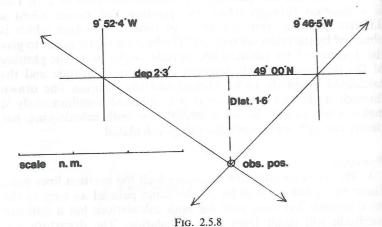
d'long between the two longitudes = 5.9' departure = $5.9 \cos 49^{\circ} 00' = 3.9'$

From Figure 2.5.8

d'lat between observed position and position 49° 00' N 9° 52.4' W = 1.6' S

departure = 2.3' E

 $d'long = 2.3 sec 49^{\circ} = 3.5' E$



Example 5

An observation of a body bearing 100°T when worked by longitude by chronometer gave a longitude of 179° 45′E when using an assumed latitude of 10° 07′N. The ship then steamed 095°T for 38 miles and a second observation of a body bearing 152°T gave an intercept of 4.8′ towards. The position assumed for the second observation was obtained by running up the first assumed latitude and calculated longitude by plane sailing. Find the ship's position at the time of the second observation.

Run 095° T by 38 miles

d'lat 3.3' S departure 37.9' E d'long 38.5' E

first assumed latitude d'lat	3.3′S	calculated longitude d'long	179°	45.0' E 38.5' E
DR position	10° 03.7′ N		180°	23.5' E
			179°	36.5' W

From Figure 2.5.9

between observed position and position $10^{\circ}~03.7'~N~179^{\circ}~36.5'~W$ and the observed position:

d'lat = 6.0' S	departure = d'long = 1.1		1′ W	
DR position d'lat observed position	10° 03.7′ N 6.0′ S 9° 57.7′ N	d'long		36.5' W 1.1' W 37.6' W

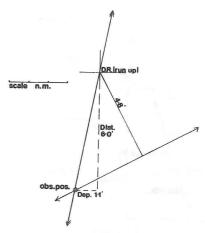


Fig. 2.5.9

Latitude by Meridian Altitude method

The meridian altitude is the altitude of the body when it is on the observer's meridian and bearing either north or south. The position line will therefore run east and west and can represent the parallel of latitude of the observer. The calculations involved to find the latitude are very quick and easy and invariably at sea the noon latitude will be obtained from the sun's meridian passage. This position line is then crossed with a transferred position line run up from an earlier sight of the sun when it was bearing to the east.

Example 7

An observation of the sun bearing 110° T during the forenoon gave an intercept of 5.5′ towards using an assumed position of 40° 15′ N 36° 40′ W. The ship then steamed 250° T for 20 miles when the latitude by meridian altitude of the sun was found to be 40° 01.5′ N. Find the ship's position at noon.

A plot of the complete problem would appear as in Figure 2.5.10. However the course and distance run is calculated and only that part of the figure inside the dotted lines would be plotted and will appear as in Figure 2.5.11.

Procedure

1. Calculate and apply the course and distance run to the assumed position used for the forenoon sight to obtain a DR for noon.

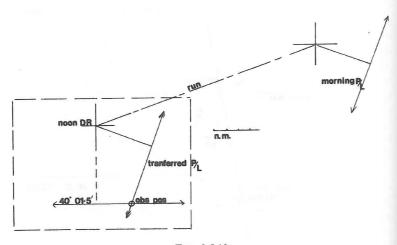


Fig. 2.5.10

2. When the latitude by meridian altitude is obtained plot the noon DR position and lay off the transferred intercept and position line from the morning observation.

3. Take the d'lat between the DR latitude and the observed latitude and plot the noon position line in the east/west direction. The observed position is where the transferred position line cuts the noon latitude.

4. Measure the departure between the DR and the observed position, convert to d'long to give the noon longitude.

forenoon assumed position 250° by 20 miles	40° 15.0′ N 6.8′ S	36° 40.0′ W 24.6′ W
noon DR position	40° 08.2′ N	37° 04.6′ W

From Figure 2.5.8

between the observed position and noon DR departure = 3.4' E d'long = 3.4 sec 40° = 4.4' E

noon DR longitude d'long	37° 04.6′ W 4.4′ E
noon longitude	37° 00.2′ W

noon position 40° 01.5′ N 37° 00.2′ W

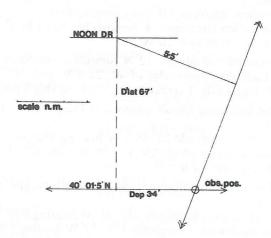


Fig. 2.5.11

Note: If this problem is done using the longitude by chronometer method for the forenoon sight then the necessity for this type of plot at noon is removed as there is a simple solution to find the longitude using the value 'C' from the computation of the bearing (see Module 2.6).

EXERCISE 2.5.1

1. From the following simultaneous observations find the observed position.

First observation intercept 6.0' away bearing 050° T. Second observation intercept 2.0' towards bearing 290° T.

DR position 47° 00′ N 6° 40′ W.

2. Using assumed position 36° 05′ S 122° 15′ E, simultaneous observations were made which gave intercepts of 9.5' away and 4.3' towards bearing 342° T and 035° T respectively. Find the ship's position.

3. From the following simultaneous observations find the ob-

served position.

First observation intercept 2.5' towards bearing 175° T. Second observation intercept 2.5' towards bearing 270° T. DR position 9° 30′ N 177° 50′ E.

4. From the following simultaneous observations find the observed position.

First observation intercept 1.0' away bearing 080° T. Second observation intercept 6.8' towards bearing 140° T. DR position 52° 20′ N 164° 16′ W.

5. Using assumed latitude 34° 12′ N, simultaneous observations were made which gave longitudes of 40° 27.4' W and 40° 31.9' W bearing 255.5° T and 140° T respectively. Find the ship's position.

6. From the following simultaneous observations find the observed position.

First observation longitude 25° 46.3′ W bearing 093° T. Second observation longitude 25° 44.7′ W bearing 327° T. DR latitude used 10° 14' S.

7. From the following simultaneous observations find the observed position.

First observation gave longitude 159° 18' W bearing 095° T. Second observation gave longitude 159° 12' W bearing 050° T. DR latitude used 15° 20' S.

8. From the following simultaneous observations find the observed position.

First observation gave longitude 146° 59' E bearing 310° T. Second observation gave longitude 147° 10' E bearing 260° T. DR latitude used 36° 40′ N.

- 9. From assumed position 23° 40' N 52° 30' W a stellar observation gave an intercept of 4.0' towards bearing 040° T. The ship then steamed 090°T for 24 miles through a current setting 000° T. Drift experienced was 5 miles. A second observation then gave an intercept of 5.0' towards bearing 120°T when using an assumed position obtained by applying the run and the current to the first assumed position. Find the ship's position at the time of the second observation
- 10. From assumed position 6° 18'S 42° 19'W an observation of the sun gave an intercept of 5.6' away bearing 130° T. The ship then steamed 145°T for 53 miles. A second observation of the moon then gave an intercept of 1.6' towards bearing 200° T when using an assumed position obtained by applying the run to the first assumed position. Find the ship's position at the time of the second observation.
- 11. From assumed position 41° 10'S 114° 00'E an observation of venus gave an intercept of 1.0' away bearing 100° T. The ship then steamed 100° T for 30 miles. A second observation of the sun then gave an intercept of 4.0' away bearing 314° T when using an assumed position obtained by applying the run to the first assumed position. Find the ship's position at the time of the second observation.
- 12. From assumed position 19° 18′ N 160° 42′ W an observation of Jupiter gave an intercept of 4.0' towards bearing 100°T. The ship then steamed 289° T for 34 miles. A second observation of the sun then gave an intercept of 7.0' away bearing 200° T when using an assumed position obtained by applying the run to the first assumed position. Find the ship's position at the time of the second observation.
- 13. In assumed latitude 52° 50' N an observation when worked by longitude by chronometer gave a longitude of 136° 10'W bearing 285° T. The ship then steamed 150° T for 15 miles when a second observation using assumed latitude 52° 40' N gave a longitude of 136° 05' W bearing 205° T. Find the ship's position at the time of the second observation.

- 14. In assumed latitude 52° 20′ N an observation when worked by longitude by chronometer gave a longitude of 164° 20′ W bearing 080° T. The ship then steamed 240° T for 10 miles when a second observation using assumed latitude obtained by running up the first assumed latitude gave a longitude of 164° 29′ W bearing 140° T. Find the ship's position at the time of the second observation.
- 15. In assumed position 50° 24′ N 22° 26′ W a forenoon sight of the sun gave an intercept of 3.1′ away bearing 102° T. The ship then steamed 265° T for 48 miles when a latitude by meridian altitude of the sun gave 50° 21.8′ N. Find the ship's position at noon.
- 16. In assumed position 5° 57′N 88° 16′E a forenoon sight of the sun gave an intercept of 4.4′ towards bearing 121°T. The ship then steamed 088°T for 33 miles when a latitude by meridian altitude of the sun gave 5° 55.8′N. Find the ship's position at noon.
- 17. In assumed position 30° 45′ N 46° 40′ W a forenoon sight of the sun gave an intercept of 6.5 towards bearing 110° T. The ship then steamed 115° T for 20 miles when a latitude by meridian altitude of the sun gave 30° 30′ N. Find the ship's position at noon.
- 18. An observation of a celestial body gave an intercept of 3.5' away bearing 220° T using an assumed position of 32° 00′ S 115° 00′ E. The ship then steamed 145° T for 17 miles and then 063° T for 12 miles when a point of land in position 32° 05′ S 115° 31′ E then bore 070° T. Find the ship's position at the time of the second position line.

MODULE 2.6

Latitude by Meridian Altitude

An observation of a body when crossing the observer's meridian is of particular value to the navigator as it provides a quick and easy method of finding a position line which will run east/west near the observer's position and will therefore be coincident with the observer's parallel of latitude. At this time the altitude of a body with constant declination is maximum to a stationary observer and the observation is made by watching the altitude climb to a maximum and recording the value. A closing or opening of the declination and latitude will retard or advance maximum altitude relative to meridian passage, but this effect is often ignored. The accurate time is not required but a time to the nearest minute must be predicted beforehand in order to extract the declination and in order to know at what time to take the observations. It is common practice to take a noon observation of the sun's meridian passage and it is convenient if a star can be found whose meridian passage occurs during morning or evening twilight.

Maximum and meridian altitude

As stated above if the ship's speed and the rate of change of declination are causing the latitude and declination to close then maximum altitude will occur after meridian passage. If latitude and declination are opening then maximum altitude will occur before meridian passage. An appreciation of the magnitude of this effect is given by considering the formula:

$$\frac{15.3 \text{ y (tan lat} \pm \text{tan dec})}{60}$$

which gives the time interval in minutes between meridian and maximum altitude for a vessel steaming north or south when y is the combined change of latitude and declination. Any east or west motion of the vessel will also have an effect and modify the factor y by a small amount positive if going west and negative if going east. A vessel in latitude 60°N steaming north at 19 knots observing the sun with declination 5°S and changing south by 1.0′ per hour, will have maximum altitude 9.3 minutes before meridian passage. In latitude 20°N this would reduce to 2.3 minutes. If this is not taken into account when observing meridian altitudes then the former case will result in an error in the latitude of about 1.5′ and the latter case of less than 0.5′. In practice in the open ocean these errors are not substantial and are often ignored. On fast vessels however they should be considered and if appropriate reduced by observing the meridian altitude at the correct time of meridian passage rather than observing the maximum altitude.

Time of meridian passage

There are two methods of finding the time of meridian passage from the Nautical Almanac.

Method 1

At meridian passage, by definition the Local Hour Angle (LHA) of the body is zero. The Greenwich Hour Angle (GHA) is therefore equal to the longitude of the observer. Longitude must be expressed westerly from Greenwich as is the GHA.

GHA = W Longitude

Thus the time of the meridian passage can be found by inspection of the Nautical Almanac to find the time at which the particular GHA occurs. Care must be taken to use the correct date at Greenwich. By convention all dates given are at the ship as would be the case in practice. The date at Greenwich may be the following date if the observer's longitude is west and the preceding date if in east longitude.

Procedure

1. Write down the GHA (west longitude or (360 - east longitude)).

2. Inspect the almanac on the date in question to extract the hour when the GHA is the next value below the value in 1. Take the difference between the two values which will be the increment.

3. Inspect the increment tables to find the minutes and seconds of the time. For appropriate bodies the increment should be adjusted for the v correction if absolute accuracy is required but in practice this can be ignored.

4. The hour from 2 and the minutes and seconds from 3 give the UT of meridian passage.

5. Check that the UT with the longitude in time applied still give the correct date at the ship. If not the problem must be reworked using the preceding Greenwich date if in east longitude or the following Greenwich date if in west longitude. With practice this check can be done mentally before starting.

Example 1

Find the UT and LMT of meridian passage of the sun over the meridian of an observer in longitude 50° 14′ W on 5th January.

GHA = W longitude	50°	14.0'
For UT 15h on 5th GHA	43°	40.1'
difference (increment)	6°	33.9

from sun increment tables 6° 33.9' corresponds to an increment of 26m 15s

UT mer pass.	15h 26m 15s 5th Jan.
longitude in time	_3h 20m 56s
LMT for long 50° 14′ W	12h 05m 19s 5th Ian

Example 2

Find the UT and LMT of meridian passage of the moon over the meridian of 168° 30′ E on 19th December.

GHA = W longitude GHA for UT 20h on 18th difference	$\begin{array}{c} 191^{\circ} \ 30.0' \\ \underline{184^{\circ} \ 37.6'} \\ 6^{\circ} \ 52.4' \end{array}$
increment	$\frac{-5.4'}{6^{\circ} 47.0'}$

from increment tables increment = 28m 26s

GHA meridian passage	20h 28m 26s 18th Dec.
longitude in time	11h 14m 00s
LMT for longitude 40° 38′ E	31h 42m 26s
	07h 42m 26s 19th Dec.

Notes:

1. The longitude in time added to the UT for E longitude was going to produce a change in date. The previous date at Greenwich was therefore used.

2. In practice the 'v' correction may be ignored and this will not produce any significant error. To get the time to the nearest second however it must be applied in the opposite way to that when taking out the GHA.

Example 3

Find the UT and LMT of meridian passage of the star Aldebaran over the meridian of 150° 30′ W on 31st October.

GHA star	150° 30.0′
and the state of the state of	360°
	510° 30.0′
SHA star	290° 57.8′
GHAΥ	219° 32.2′
GHAΥ 12h 31st	219° 22.7′
difference = increment	0° 09.5′
from Aries increment table	increment = 0m 40s
UT meridian passage	12h 00m 40s 31st Oct.
longitude in time	10h 02m 00s
LMT for 150° 30′ W	01h 58m 40s 31st Oct.

Note: For a star the SHA must be subtracted from the GHA to get GHA Aries.

Method 2

The daily pages of the Nautical Almanac give times to the nearest minute for meridian passage of the sun, moon, planets, and the first point of Aries. The sun's and the moon's meridian passage is given in a box at the lower right of the right hand page once for each day on the page. For the planets it is given in a box at the lower right hand corner of the left page, once for the three days, and for Aries at the foot of the Aries GHA column. These times are local mean times and require correction for longitude to give the UT.

Sun

The values given under the heading 'Sun mer pass.' vary between 1144 and 1216 and may be taken to be the LMT of meridian passage of the sun across any meridian. The difference between the figure given and 1200 will be the Equation of Time to the nearest minute. The UT of the sun's meridian passage may very quickly be found by applying the longitude in time to this figure.

The examples that were used for Method 1 will be repeated here.

Example 1

Find the UT and LMT of meridian passage of the sun over the meridian of an observer in longitude 50° 14′ W on 5th January.

From almanac for 5th LMT mer pass.	1205
longitude in time	0321
UT meridian passage	1526

The time to the nearest minute is acceptable considering the moderate rate of change of declination of the sun, and is clearly quicker and easier than Method 1.

Moon

The LMT of meridian passage of the moon is given once for each day at the foot of the right hand daily page for upper and lower meridian passages. It will be seen that the times given get later each day by an average of about 50 minutes. The figures given must be taken to apply only to the Greenwich meridian and a longitude correction which is a proportion of the daily retardation must be applied, that proportion being the longitude divided by 360°.

Thus

longitude correction =
$$\frac{\text{daily retardation} \times \text{longitude}}{360}$$

Any meridian in easterly longitude will pass beneath the sun before the meridian of Greenwich. In this case the daily retardation is taken as the difference between meridian passages on the day in question and the previous day, and the longitude correction is negative. For a meridian in westerly longitude the daily retardation is taken as the difference between meridian passages for the day in question and the following day, and the correction is positive. The longitude correction is tabulated in the Nautical Almanac under the name of Table II on the penultimate page of the almanac. Tabulation is against longitude and daily retardation. It must however be quicker to obtain the solution from a calculator using the above formula.

The correction will give the LMT for the observer's meridian. After correction the longitude in time is applied in the usual way to obtain the UT

Procedure

1. Write down the time of the moon's meridian passage for the day in question.

2. Under this write the time of the preceding meridian passage if in east longitude or the following meridian passage if in west longitude. Note that as there is more than 24 hours between meridian passages the two times written down do not necessarily occur on consecutive dates.

3. Take the difference between the two meridian passage times and calculate the longitude correction by:

$$correction = \frac{longitude \times difference}{360}$$

4. Apply the longitude correction to the LMT of meridian passage for the day in question positive if in west longitude and negative if in east longitude (the result must lie between the two times extracted).

5. Apply the longitude in time to obtain the UT.

Example 2

Find the UT and LMT of meridian passage of the moon over the meridian of 168° 30′ E on 19th December.

LMT meridian passage for longitude 0° on 19th Dec.	0806
LMT meridian passage for longitude 0° on 18th Dec.	0717
difference = retardation	49m

longitude correction =
$$\frac{49 \times 168.5'}{360}$$
 = 23m

LMT meridian passage for longitude 0° on 2nd Nov.	0806	
longitude correction	23	
LMT meridian passage for longitude 168° 30' E	0743	
longitude in time	1114	
UT meridian passage longitude 168° 30' E	2029	18th Dec.

Planets

The LMT of meridian passage for the four navigational planets are given at the foot of the left hand page in the almanac. One figure is given for the three days for each planet referring to the middle day on the page. Again this is an LMT for the Greenwich meridian and theoretically a longitude correction should be applied. However the amount of change over a day is never more

than a few minutes and the rate of change of declination of the planets is small. Any error by not applying the longitude correction will be negligible and the correction may be ignored. It only remains to apply the longitude in time to obtain the UT.

Example 3

Find the UT and LMT of meridian passage of the planet Mars over the meridian of 165° 15′ E on 31st October.

LMT meridian passage Mars 31st	2000
longitude in time	1101
UT meridian passage Mars	0859 31st

Stars

The time of meridian passage of a star is required only to enable the navigator to know when to commence his observations. The declination of a star remains constant over long periods and therefore extreme accuracy in the time of meridian passage is not required.

The LMT of the meridian passage of the First Point of Aries is given at the foot of the Aries column in the almanac. This will always get approximately four minutes earlier each successive day. The time given refers to the middle day of the page and the time for the first day can be found by adding four minutes and that for the third day by subtracting four minutes. The longitude correction will never exceed two minutes and can be ignored.

A star will cross any meridian earlier than Aries by the amount of its SHA in time. Strictly speaking this should be calculated by:

SHA 15° 02.5′

as 15° 02.5′ is the hourly rotation of the earth. No significant error will be caused if 15° is used.

Example 4

Find the UT and LMT of meridian passage of the star Aldebaran over the meridian of 150° 30′ W on 31st October.

LMT meridian passage \gamma 31st	2121 (2117 + 4 minutes)
SHA in time	1924
LMT meridian passage star	0157
longitude in time	1002
UT meridian passage star	1159 31st

To find if any stars will cross the observer's meridian during the period of twilight

If the SHA of the celestial meridian of the observer is found for the beginning of twilight and also for the end of twilight, then any star with an SHA between the two values will cross the observer's meridian during twilight and can be observed as part of star sights.

Example

Find any stars which will cross the meridian of 161°W during the period 1712 to 1750 LMT on 31st October.

LMT beginning of twilight	1712	
longitude in time	1044	
UT beginning of twilight	0356	1st November

GHA γ 03h	84° 59.6′
increment 56m	14° 02.3′
GHA γ 0356	98° 01.9′
GHA star = W'ly long	<u>161° 00.0′</u>
SHA star	62° 58.1′ will cross meridian at 1712

At 1750, that is 38 minutes later the earth will have rotated through:

$$\frac{38 \times 15^{\circ} \text{ } 02.5'}{60} = 9.5 \text{ approximately}$$

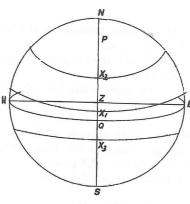
Hence at 1750 the meridian of SHA 62° $58.1' - 9^{\circ}$ 30' will cross the observer's meridian.

Thus between 1712 and 1750 any stars with SHA between 62° 58.1′ and 53° 28.1′ will cross an observer's meridian in 161° W.

By inspection of the almanac the star Peacock with SHA 53° 31.1′ and the star Altair with SHA 62° 15.7′ will be suitable.

Finding the Latitude

When a celestial body is on the observer's meridian then the three arcs which represent declination, zenith distance and latitude are all measured along the same meridian, in other words the meridians of the observer and the body are coincident. In this case there is a simple relationship between declination, zenith distance and latitude, which enables the unknown, the latitude to be found. The relationship is shown in Figure 2.6.1.



MODULE 2.6

Fig. 2.6.1

In Figure 2.6.1.

Z is the observer's zenith.

WQE is the equinoctial.

ZQ represents the observer's latitude.

NS is the observer's meridian.

P is the elevated pole.

 X_1 , X_2 and X_3 are three bodies which are on the observer's meridian.

 X_1 has declination the same name as the latitude but less than the latitude, and its zenith distance is ZX_1 , and declination QX_1 .

 X_2 has declination the same name and greater than the latitude, and its zenith distance is ZX_2 , and declination QX_2 .

 X_3 has declination of opposite name to the latitude, and its zenith distance is ZX_3 and declination QX_3 .

From Figure 2.5.1 it can be seen that:

for body X_1 the latitude will be given by:

$$ZQ = ZX_1 + QX_1$$
 (latitude = zenith distance + declination)

for body X_2 the latitude will be given by:

$$ZQ = QX_2 - ZX_2$$
 (latitude = declination - zenith distance)

for body X₃ the latitude will be given by:

$$ZQ = ZX_3 - QX_3$$
 (latitude = zenith distance – declination)

These circumstances and results are difficult to remember but may easily be deduced in each problem as shown in the following examples.

Procedure

- 1. Find the time of meridian passage of the body and extract the declination from the almanac.
- 2. Correct the sextant altitude to true altitude and subtract from 90° to give the zenith distance.
 - 3. Deduce and apply the appropriate formula to give latitude.

Example 1

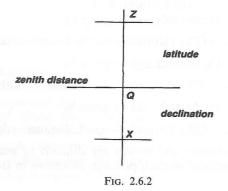
On 18th December the sextant altitude of the star Diphda whilst on the meridian bearing south was 46° 15.4′. Index error 1.4′ on the arc. Height of eye 12 metres. DR position 25° 33′ N 33° 52′ W. Find the latitude and the direction of the position line.

Sextant altitude	46° 15.4′
index error	-1.4'
observed altitude	46° 14.0′
dip	-6.1'
apparent altitude	46° 07.9′
total correction	-0.9'
true altitude	46° 07.0′
	90°
zenith distance	43° 53.0′
declination	17° 58.0′ S
latitude	25° 55.0′ N

position line was 090/270

Notes: No time for the meridian passage was necessary because the declination is the same for the three days on the daily page.

The Figure 2.6.2 was drawn to represent a small sketch of the meridian as shown in Figure 2.6.1 in order to establish the



appropriate rule to apply to find latitude. If the point Q is inserted first to represent the point on the equinoctial where it crosses the observer's meridian, the point X can be inserted, but it must be to the south of Q because the declination is south. The point Z representing the observer's zenith can then be inserted. This must be to the north of X because the bearing of the body was south when it was on the meridian. The point Z must also be to the north of Q because the zenith distance was more than the declination. Hence Z is to the north of Q denoting that the latitude is north and equal to (zenith distance – declination).

Example 2

On 5th January the sextant altitude of the star Fomalhaut whilst on the meridian bearing south was 77° 52.4′. Index error 3.0′ off the arc. Height of eye 11 metres. Find the latitude and the direction of the position line.

Sextant altitude	77° 52.4′
index error	+3.0'
observed altitude	77° 55.4′
dip	-5.8'
apparent altitude	77° 49.6′
total correction	-0.2'
true altitude	77° 49.4′
	90°
zenith distance	12° 10.6′
declination	29° 36.7′ S
latitude	17° 26.1′ S

position line was 090/270

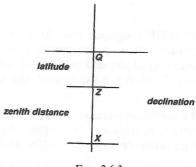


Fig. 2.6.3

Note: The diagram was drawn in the same way as for the previous example but because the zenith distance was less than the declination, Z, the zenith, must lie to the south of Q giving a south latitude.

EXERCISE 2.6.1

- 1. On 19th September the sextant altitude of the star Aldebaran on the meridian was 71° 22.8′. Index error 1.4′ off the arc. Height of eye 14.5 metres. The star was bearing south. Find the latitude and the direction of the position line.
- 2. On 19th December the sextant altitude of the star Dubhe on the meridian was 28° 06.2′. Index error 0.6′ on the arc. Height of eye 15.3 metres. The star was bearing north. Find the latitude and the direction of the position line.
- 3. On 5th January the sextant altitude of the star Regulus on the meridian was 28° 14.4′. Index error 1.4′ off the arc. Height of eye 14.4 metres. The star was bearing north. Find the latitude and the direction of the position line.
- 4. On 20th September the sextant altitude of the star Rigel on the meridian was 71° 22.8′. Index error 0.4′ on the arc. Height of eye 14.5 metres. The star was bearing north. Find the latitude and the direction of the position line.
- 5. On 27th June the sextant altitude of the star Alioth on the meridian was 34° 03.5'. Index error 1.8' off the arc. Height of eye 12.0 metres. The star was bearing north. Find the latitude and the direction of the position line.

In the following examples using the sun and the moon, the time of meridian passage must first be found to obtain the declination.

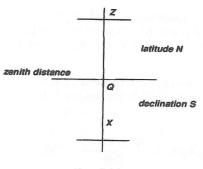
Example 3

On 18th December in DR longitude 154° 20′ W the sextant altitude of the sun's lower limb when on the meridian bearing south was 44° 20.8′. The index error of the sextant was 0.4′ off the arc. Height of eye 15.3 metres. Find the latitude and the direction of the position line.

LMT meridian passage	11h 56m
longitude in time	10h 17m
UT meridian passage	22h 13m
declination	23° 23.7′ S

sextant altitude	44° 20.8′
index error	+0.4'
observed altitude	44° 21.2′
dip	-6.9'
apparent altitude	44° 14.3′
total correction	-+15.3'
true altitude	44° 29.6′
	90°
zenith distance	45° 30.4′
declination	23° 23.7′ S
latitude	22° 06.7′ N

position line runs 090/270 through 22° 06.7′ N 154° 20′ W



MODULE 2.6

Fig. 2.6.4

EXERCISE 2.6.2

- 1. On 18th December in DR position 00° 20′ N 162° 20′ W the sextant altitude of the sun's lower limb when on the meridian was 66° 10.4′ bearing south. Sextant index error was 1.2′ on the arc. Height of eye 13.2 metres. Find the latitude and the direction of the position line.
- 2. On 28th June in DR position 25° 10′S 40° 20′W the sextant altitude of the sun's lower limb when on the meridian was 41° 26.4′ bearing north. Sextant index error was 2.4′ off the arc. Height of eye 7.3 metres. Find the latitude and the direction of the position line.
- 3. On 6th January in DR position 51° 30′S 96° 35′W the sextant altitude of the sun's upper limb when on the meridian was 61° 25.0′ bearing north. Sextant index error was 1.4′ on the arc.

Height of eye 11.5 metres. Find the latitude and the direction of the position line.

- 4. On 30th September in DR position 36° 55′N 165° 30′E the sextant altitude of the sun's lower limb when on the meridian was 50° 11.8′ bearing south. Sextant index error was 1.6′ off the arc. Height of eye 14.0 metres. Find the latitude and the direction of the position line.
- 5. On 19th September in DR longitude 141° 10.8′E the sextant altitude of the sun's lower limb when on the meridian was 36° 37.6′ bearing 000° T. Sextant index error was 1.6′ off the arc. Height of eye 13.0 metres. Find the latitude and the direction of the position line.

Example 4

On 27th June in longitude 58° 45′W the sextant altitude of the moon's lower limb was 67° 48.6′ to the north of the observer. The sextant index error was 2.0′ off the arc and the height of eye 9.5 metres.

LMT meridian passage 27th for longitude 0	10h 08m
LMT meridian passage 28th for longitude 0	10h 57m
difference	49m

correction for longitude
$$\frac{49 \times 58^{\circ} 45'}{360^{\circ}} = 8 \text{m}$$

LMT meridian passage 27th for longitude 0°	10h 08m
longitude correction	8m
LMT meridian passage for longitude 58° 45′ W	10h 16m
longitude in time	3h 55m
UT meridian passage for longitude 58° 45′ W	14h 11m 27th

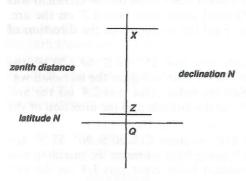


Fig. 2.6.5

declination	23° 06.9′ N H.P. 54.5
'd' corr	$\frac{+1.3'}{222.222}$
declination	23° 08.2′ N
sextant altitude	67° 48.6′
index error	+2.0'
observed alt.	67° 50.6′
dip	-5.4'
apparent alt.	67° 45.2′
main corr.	+32.1'
2nd corr.	2.9′
true altitude	68° 20.2′
zenith distance	21° 39.8′ N
declination	23° 08.2′ N
latitude	1° 28.4′ N

position line runs 090/270 through 1° 28.4′ N 58° 45′ W

EXERCISE 2.6.3

- 1. On 5th January in DR longitude 45° 20' E the sextant altitude of the moon's lower limb when on the meridian was 40° 18.5' bearing south. Sextant index error was nil. Height of eye 5.5 metres. Find the latitude and the direction of the position line.
- 2. On 19th September in DR longitude 162° 45' W the sextant altitude of the moon's upper limb when on the meridian was 30° 30.5' bearing north. Sextant index error was 1.5' on the arc. Height of eye 10 metres. Find the latitude and the direction of the position line.
- 3. On 19th December in DR longitude 130°E the sextant altitude of the moon's upper limb when on the meridian was 70° 30′ bearing north. Sextant index error was nil. Height of eye 9.0 metres. Find the latitude and the direction of the position line.
- 4. On 30th September in DR longitude 0° the sextant altitude of the moon's lower limb when on the meridian was 68° 18.6′ bearing south. Sextant index error was nil. Height of eye 8.6 metres. Find the latitude and the direction of the position line.

Computing the sextant altitude of a star when on the meridian If it is required to observe the meridian passage of a star then not only is it necessary to find the time when the star is on the meridian, in order to know when to commence observation, but it is advisable to know the approximate sextant altitude to set on the sextant to facilitate finding the star. It should be realised that this applies to all star observations. If the navigator waits until he can find a star with his naked eye the horizon will be too dark to observe (at evening twilight). At morning twilight by the time it is light enough to see the horizon then it will be difficult to see the constellations and find and identify a star.

In this example the time of meridian passage is found and then the altitude correction worked backwards from true altitude to sextant altitude. This altitude can then be set on the sextant and the star found in the star telescope.

Example

Compute the sextant altitude and find the LMT when the star Aldebaran is on the meridian to an observer in DR position 55° 18' N 142° 10'W on 19th September. Sextant index error 0.6' off the arc. Height of eye 13.3 metres.

(7)	
At meridian passage	GHA = W'ly longitude
GHA star SHA star GHA \gamma GHA 14h 19th increment	142° 10.0′ 290° 58.1′ 211° 11.9′ 208° 03.8′ 3° 08.1′ = 12m 30s
UT mer pass star	14h 12m 30s 19th
longitude in time	9h 28m 40s
LMT mer pass sta	o4h 43m 50s 19th
Latitude declination zenith distance	55° 18.0′ N 16° 31.1′ N 38° 46.9′ bearing south
true altitude total corr. apparent alt. dip observed alt. index error sextant altitude	$51^{\circ} 13.1' \\ +0.8' \\ \hline 51^{\circ} 13.9' \\ +6.4' \\ \hline 51^{\circ} 20.3' \\ -0.6' \\ \hline 51^{\circ} 19.7'$

Note: All the altitude correction are applied with reversed sign.

Lower Meridian Passage

The apparent daily motion of any celestial body is to describe a circle around the celestial pole, once in a sidereal day. During this period the body will not only cross the observer's meridian but will also cross the observer's anti-meridian. (The meridian 180° removed in longitude from the observer.). Under certain circumstances the body will remain visible during the whole period, never setting below the horizon. Such a body is called a circumpolar body. The condition for circumpolarity is that the latitude is greater than the polar distance (90° – declination).

A circumpolar body will therefore be visible when it crosses the observer's anti-meridian, this occurrence being called 'lower meridian passage' or 'on the meridian below the pole'. The latitude can be found easily from a lower meridian passage observation.

At lower meridian passage:

latitude = true altitude + (90 - declination)

that is

latitude = true altitude + polar distance of body.

In normal navigable latitudes it is usually stars which are circumpolar as the navigator has to go to high latitudes to cause the sun or the moon to become circumpolar. He must of course be above the latitude of the arctic or antarctic circles for the sun ever

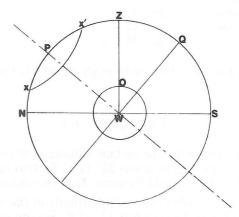


Fig. 2.6.6

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to be circumpolar. In order to find the time of a stars lower meridian passage then the almanac should be consulted for the time when the stars GHA is equal to the (observer's westerly longitude + 180°). Otherwise the procedure is the same as described for finding the time of upper meridian passage.

Procedure

1. Find the LMT of lower meridian passage in order to know at what time to commence observation.

2. Extract the star's declination from the almanac.

3. Correct the altitude of the star.

4. Add the polar distance of the star to the true altitude. The latitude must be named the same as the declination.

Example

On 18th September, the sextant altitude of Atria on the meridian below the pole was 19° 41.8'. The observer's longitude was 138° 30'E. The index error was 0.8' on the arc and the height of eye 9.7 metres. Find the latitude and the direction of the position line.

sextant altitude index error observed altitude dip apparent altitude total corr true altitude polar distance latitude index error $\frac{-0.8'}{19^{\circ} 41.0'}$ $\frac{-5.5'}{19^{\circ} 35.5'}$ $\frac{-2.7'}{19^{\circ} 32.8'}$ $\frac{20^{\circ} 57.7'}{40^{\circ} 30.5'}$ S	declination polar dist.	69° 02.3′ S 90° 20° 57.7′
--	-------------------------	---------------------------------

position line runs 090/270 through 40° 30.5′ S 138° 30′ E

EXERCISE 2.6.4

- 1. On 18th December the sextant altitude of the star Dubhe on the meridian below the pole was 22° 19.5'. Sextant index error 2.2' on the arc. Height of eye 12.8 metres. Find the latitude.
- 2. On 19th December the sextant altitude of the star Alkaid on the meridian below the pole was 12° 27.9'. Sextant index error 2.4' on the arc. Height of eye 12.8 metres. Find the latitude.

- 3. On 7th January the sextant altitude of the star Schedar on the meridian below the pole was 21° 48.0′, Sextant index error 0.8′ off the arc. Height of eye 13.2 metres. Find the latitude.
- 4. On 20th September the sextant altitude of the star Avior on the meridian below the pole was 19° 32.4′. Sextant index error 1.2′ off the arc. Height of eye 14 metres. Find the latitude.
- 5. On 28th June the sextant altitude of the star Achernar on the meridian below the pole was 13° 00.4′. Sextant index error 1.4′ on the arc. Height of eye 12.5 metres. Find the latitude.

MODULE 2.7

Calculation of position lines from bodies out of the meridian

There have been many methods devised in the past of obtaining position information from astronomical observations. Most of them have been devised with the quickest possible solution in mind. Many have been in tabular form to reduce the amount of calculation required of the navigator and these have been known as short method tables or sight reduction tables. They are no doubt still in use and most navigators have found his most favoured tabular method. In professional examinations these tables have traditionally not been allowed and full solution of the PZX triangle has been taught in navigation schools. Before the ubiquitous hand held calculator a logarithmic solution was used and the haversine formula best suited this method. With the availability of calculators the importance of 'short method' tables has decreased and the haversine formula is no longer the most convenient for manual solution. Here basic principles are best demonstrated by reverting back to manual solution using the fundamental spherical cosine formula. The calculations are no longer onerous and this is probably the quickest way of producing a result. It is now accepted in professional examinations and is used here.

The navigator may want to experiment himself with his personal programmable calculator or with his computer. It is within the abilities of most competent computer owners to programme the mathematics and for this purpose the fundamental formula described is the best basis for the calculations. The Nautical Almanac gives instructions on one efficient approach to this in its explanation pages and also gives a tabular method. Commercial software is available which stores almanac data to further ease the navigator's task. Most people would agree however that complete reliance on the microchip in not desirable, certainly not without understanding the basic principles involved. It is these basic principles with which we are concerned here.

Definitions

Vertical circle. A great circle on the celestial sphere which passes through the observer's zenith.

Prime vertical. The vertical circle whose direction is east/west.

The reduction of sights of bodies out of the meridian is essentially the solution of a spherical triangle on the celestial sphere. This triangle is formed by the intersection of the three great circles, the observer's celestial meridian, the celestial meridian of the body observed and the vertical circle through the body. This triangle is represented in Figure 2.7.1.

The angles of the triangle will be:

- 1. Angle P. The angle at the pole between the meridians of the observer and that of the body. This is the Local Hour Angle of the body when the body is to the west of the observer's meridian and $(360^{\circ}-\text{Local Hour Angle})$ when the body is to the east of the observer's meridian.
- 2. Angle Z. The angle at the zenith between the observer's meridian and the vertical circle through the body. This is the azimuth of the body.
- 3. Angle X. The parallactic angle. This is not used in the calculations.

The three sides of the triangle will be:

- 1. Side PZ. The angular distance of the zenith from the pole. This is the complement of the latitude or co-lat. (90° latitude).
- 2. Side PX. The angular distance of the body from the pole. This is called the polar distance and will be equal to (90° declination).
- 3. Side ZX. The angular distance of the body from the zenith. This is the zenith distance and will be equal to (90° true altitude).

Figure 2.7.1 represents the celestial sphere drawn on the plane of the rational horizon, that is looking down from above the observer's zenith. The great circle WZE is the prime vertical and any great circle passing through Z will be a vertical circle. NS is the observer's meridian with the elevated pole in this case the north pole shown at P. The great circle WQE is the equinoctial or celestial equator. The declination circle of a body in north latitude with declination less than the latitude is shown with the body at X. Because the declination is less than the latitude the declination circle will pass closer to the equinoctial than the zenith and the body will be to the south of the observer at meridian passage. This figure is the usual projection used to illustrate the PZX triangle. As for any triangle in

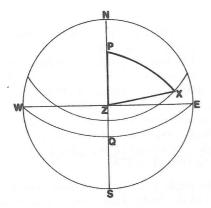


Fig. 2.7.1

order to solve we need to know, or be able to find, at least three parts either angles or sides. In fact we can only know two of its parts. PX is the complement of the declination which we can obtain from the nautical almanac as long as we have taken an accurate time of the observation. The observation of altitude when corrected will give the side ZX, the zenith distance, that is (90°-true altitude). The triangle can only be solved by making assumptions about one or more parts of the triangle, and therefore the solution will only be correct if the assumptions made are correct. The part or parts assumed will depend upon the method used.

The Intercept Method (Marcq St. Hilaire)

Module 2.5 (Position Lines and Position Circles) should have been studied and understood before reading the explanation of the calculations involved in this method.

It has been stated that any observation may be solved by this method. There are other methods which have been favoured in the past and one of these will be looked at later.

In the intercept method the arguments used are:

Side PX, the complement of the declination.

Angle P, derived by assuming a longitude which is applied to the GHA to find LHA.

Side PZ, derived by assuming a latitude and subtracting it from 90°.

The solution is made for ZX, the zenith distance and Z, the azimuth or bearing. In order to find LHA and the declination an

accurate Greenwich time of observation to the nearest second is required. This has traditionally been taken from a chronometer keeping UT, but the importance of chronometers has been reduced by the high quality of modern personal time pieces, and any good watch can be used. The important thing is that the error in the watch is regularly monitored by time signal and any error to the nearest second applied. Chronometers are normally kept on UT but if a deck watch is used the correction from the ship's time being kept by the watch to UT must also be made.

The solution gives the zenith distance and bearing which would have been observed at the time of the observation if the observer were in the assumed latitude and longitude. Remember from Module 2.5 that the zenith distance defines a position circle centred upon the geographical position of the body observed.

On the assumption that the true position is somewhere near the assumed position then the bearing calculated can be taken to be of sufficient accuracy. The calculated zenith distance however gives a position circle at right angles to the bearing passing through the assumed position. The true zenith distance derived from the observation will show whether the observer is further away from or closer to the geographical position of the body than the assumed position. The difference between the calculated and the true zenith distances is called the intercept, and named either towards or away depending on whether the true zenith distances is less than or greater than the calculated zenith distance. The true position circle will pass through the end of the intercept. (Intercept Terminal Position or ITP.) Thus one position line is defined by the direction of the position line (at right angles to the bearing), and a position through which it passes (the ITP). Two such calculations yielding two position lines will define the vessel's position.

Calculation of the zenith distance

This is best done by the use of the spherical cosine formula if a calculator is being used. This states that in the PZX triangle:

cosine ZX = cosine PZ cosine PX + sine PZ sine PX cosine P

and

$$cosine Z = \frac{cosine PX - cosine PZ cosine ZX}{sine PZ sine ZX}$$

This can be modified by substituting complements. Thus cosine PX becomes sine declination and cosine PZ becomes sine latitude. Sine PX becomes cosine declination and sine PZ becomes cosine declination. Thus

 $\cos ZX = \sin \operatorname{lat} \sin \operatorname{dec} + \cos \operatorname{lat} \cos \operatorname{dec} \cos P$

Care should be taken if complements are substituted. By convention P is always the elevated pole and therefore PZ will always be less than 90°, but if declination is opposite to latitude PX will be over 90° and its cosine will be negative. In this case cosine PX becomes - sine declination. The equation is therefore best remembered as

 $\cos ZX = \cos \operatorname{lat} \cos \operatorname{dec} \cos P + \sin \operatorname{lat} \sin \operatorname{dec}$ (lat and dec same name)

 $\cos ZX = \cos \operatorname{lat} \cos \operatorname{dec} \cos P - \sin \operatorname{lat} \sin \operatorname{dec}$ (lat and dec opposite name)

The advantage of using the formula without substituting complements is that the calculator will itself insert the correct signs and the correct answer will result without the navigator having to remember them.

The cosine formula is very easily solved with a suitable calculator. It is however unsuitable for logarithmic solution because of the multiple changes between natural and logarithmic functions. Because of this the haversine formula was developed from the cosine formula and was in general use before the availability of hand held calculators. Logarithms are rarely used now and the haversine formula naturally has fallen into disuse. It is however given here as an alternative to the cosine formula for those who still prefer to use a logarithmic solution but all examples given use the cosine formula. The versine is $(1 - \cos ine)$ and the haversine is $\frac{1}{2}(1 - \cos ine)$.

Derived from the cosine formula the haversine formula states:

haversine ZX = (haversine P sine PZ sine PX)+ haversine (PZ \sim PX)

Procedure

1. From the chronometer reading, deduce the UT. The chronometer may need 12 hours to be added to it. This can be decided by applying the longitude in time to the approximate local time to find the approximate UT. It may be that the UT is on the following or the preceding date. The date given in any problem will, as in practice, be the date at the ship.

2. With the UT extract the GHA and declination of the body

observed.

- 3. Apply longitude to the GHA to find LHA and hence angle P in the PZX triangle. P is equal to LHA if the body is to the west of the observer and (360 – LHA) if the body is to the east of the observer.
- 4. Apply the cosine formula to solve for calculated zenith distance (CZX).
- 5. Correct the sextant altitude and obtain the true zenith distance (TZX).
- 6. Take the difference between CZX and TZX to be the intercept and name.
- 7. Calculate the bearing by ABC tables or cosine formula to give the direction of the position line.

Example 1

On 30th September at about 0900 at the ship in DR position 41° 15' N 175° 30' W, when a chronometer correct on UT showed 08h 25m 15s, the sextant altitude of the sun's lower limb was 28° 46.7'. Index error 0.4' off the arc. Height of eye 15.8 metres. Find the direction of the position line and a position through which it passes.

approximate LMT	30th 09h 00m
longitude W	11h 42m
approximate UT	2041- 201- 42
approximate O1	30th 20h 42m
UT	20h 25m 15s 30th
O I	2011 23111 138 30th
	(12 hours added to the chronometer)
	(12 hours added to the chronometer)

	(12)	nours added to the ch	ironometer)
declination 'd' declination	2° 52.5′ S 0.4′ 2° 52.9′ S	sextant altitude index error observed alt. dip	$28^{\circ} 46.7' \\ +0.4' \\ 28^{\circ} 47.1' \\ -7.0'$
GHA 20th	122° 30.1′	apparent alt.	28° 40.1′
increment	6° 18.8′	total corr	+14.3'
GHA	128° 48.9′	true alt.	28° 54.4′
	360°	true ZX	61° 05.6′
	488° 48.9′		
longitude	175° 30.0′ W		
LHA	313° 18.9′		
angle P	46° 41.1′		

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by cosine formula

cosine ZX = cosine PZ cosine PX + sine PZ sine PX cosine Pcosine $ZX = cosine 48^{\circ} 45'$ cosine $92^{\circ} 52.9' + sine 48^{\circ} 45'$ sine 92° 52.9′ cosine 46° 41.1′ =-0.03315+0.51512=0.48197

61° 11.2′ Calculated ZX 61° 05.6′ True ZX 5.6' towards intercept

A 0.827 S B 0.069 S

S 56.0° E or 124° T Azimuth C 0.896 S

From Figure 2.7.2 which shows a plot of the intercept and position line the ITP can be calculated if required. This is the position through which the position line passes which is asked for in the original question.

d'lat = 3.1' S departure = 4.6' E $d'long = 4.6 sec 41^{\circ} 15' = 6.1' E$

DR Position	41° 15.0′ N	111	175° 30.0′ W 6.1′ E
d'lat ITP	$\frac{3.1'}{41^{\circ}}$ S $\frac{11.9'}{N}$ N	d'long	175° 23.9′ W

position line runs 034°/214° through 41° 11.9′ N 175° 23.9′ W

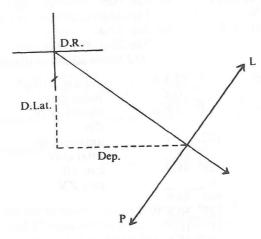


Fig. 2.7.2

Notes:

1. Intermediate steps have been shown in solving the cosine formula equations. These can be dispensed with by a navigator who is proficient with his calculator.

MODULE 2.7

2. The cosine formula to solve for zenith distance may be manipulated by using complements. Thus:

cosine ZX = cosine PZ cosine PX + sine PZ sine PX cosine P

is equivalent to:

$$\cos ZX = \cos \operatorname{lat} \cos \operatorname{dec} \cos P + \sin \operatorname{lat} \sin \operatorname{dec}$$

(if declination is opposite name to latitude then PX is over 90 and cosine $PX = -\sin \theta$ dec. It must be remembered that a negative sign is applied to sine dec in this case).

$$\cos ZX = \cos 41^{\circ} 15' \cos 2^{\circ} 52.9' \cos 46^{\circ} 41.1' - \sin 41^{\circ} 15' \sin 2^{\circ} 52.9'$$

 $\cos ZX = 0.51512 - 0.03317$
 $ZX = 61^{\circ} 11.2'$

3. The azimuth in the above example was found by using ABC tables. It could equally well be calculated by the cosine formula which states:

$$cosine Z = \frac{cosine PX - cosine PZ cosine ZX}{sine PZ sine ZX}$$

or

cosine Z =
$$\frac{\text{cosine } 92^{\circ} 52.9' - \text{cosine } 48^{\circ} 45' \text{ cosine } 61^{\circ} 05.6'}{\text{sine } 48^{\circ} 45' \text{ sine } 61^{\circ} 05.6'}$$

= -0.56068
= N 124.1°E or 124°T

EXERCISE 2.7.1

1. On 27th June at about 0900 at the ship in DR position 29° 30′ S 121° 20′ W, when a chronometer which was correct on UT showed 05h 05m 20s. The sextant altitude of the sun's lower limb was observed to be 21° 11.9′. Sextant index error 1.6′ on the

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arc. Height of eye 12.0 metres. Find the direction of the position line and a position through which it passes.

- 2. On 8th January at about 1510 at the ship in DR position 32° 15′ S 48° 16′ W, when a chronometer which was correct on UT showed 06h 21m 24s. The sextant altitude of the sun's upper limb was observed to be 48° 59.9'. Sextant index error 0.4' on the arc. Height of eye 11.0 metres. Find the direction of the position line and a position through which it passes.
- 3. On 19th September at about 1547 at the ship in DR position 00° 00′ 160° 55′ W, when a chronometer which was correct on UT showed 02h 29m 15s. The sextant altitude of the sun's lower limb was observed to be 31° 46.9'. Sextant index error 0.6' off the arc. Height of eye 12.5 metres. Find the direction of the position line and a position through which it passes.
- 4. On 18th December at about 0846 at the ship in DR position 43° 12' N 38° 25' W, when a chronometer which was 02m 21s fast on UT showed 11h 21m 52s. The sextant altitude of the sun's lower limb was observed to be 10° 23.9'. Sextant index error 1.6' off the arc. Height of eye 11.5 metres. Find the direction of the position line and a position through which it passes.
- 5. On 30th September at the ship in DR position 44° 05'N 27° 41' W, at UT 09h 26m 02s. The sextant altitude of the sun's lower limb was observed to be 16° 26.8'. Sextant index error 1.4' on the arc. Height of eye 9.0 metres. Find the direction of the position line and a position through which it passes.

Example 2

On 9th January at approximate ship's time 1940 in assumed position of 35° 10' S 127° 50' E the sextant altitude of the star Sirius was observed to be 37° 07.3'. Sextant index error 0.4' on the arc. Height of eye 15 metres. A chronometer which was correct on UT showed 11h 15m 10s. Find the direction of the position line and a position through which it passes.

approximate LMT	9th	19h	40m		
longitude W		08h	31m		
approximate UT			09m		
UT		11h	15m	10s	9th

declination	16° 43.2′ S	sextant altitude	37° 07.3′
GHA γ 11h increment GHA γ	273° 34.2′ 3° 48.1′ 277° 22.3′	index error observed alt. dip	$ \begin{array}{r} -0.4' \\ 37^{\circ} \ 06.9' \\ -6.8' \end{array} $
SHA Sirius GHA Sirius	258° 40.7′ 536° 03.0′	apparent alt. total corr true alt.	$ \begin{array}{r} 37^{\circ} \ 00.1' \\ \hline -1.3' \\ \hline 36^{\circ} \ 58.8' \end{array} $
GHA Sirius longitude LHA Sirius angle P	360° 176° 03.0' 127° 50.0' 303° 53.0' 56° 07.0'	true ZX	53° 01.2′

by cosine formula

cosine ZX = cosine PZ cosine PX + sine PZ sine PX cosine P cosine ZX = cosine 54° 50' cosine 73° 16.8' + sine 54° 50' sine 73° 16.8' cosine 56° 07' =0.16570+0.43648

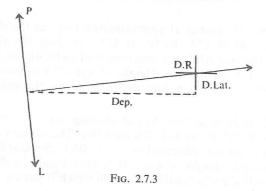
 $ZX = 52^{\circ} 58.4'$

 $\cos ZX = \cos \operatorname{lat} \cos \operatorname{dec} \cos P + \sin \operatorname{lat} \sin \operatorname{dec}$ $\cos ZX = \cos 35^{\circ} 10' \cos 16^{\circ} 43.2' \cos 56^{\circ} 07' + \sin 35^{\circ} 10'$ sin 16° 43.2′ $\cos ZX = 0.43648 + 0.16570$ $ZX = 52^{\circ} 58.4'$

Calculated ZX 52° 58.4' A 0.473 N True ZX B 0.362 S

intercept 2.8' away C 0.111 N Azimuth N 84.8° E or 085° T

From Figure 2.7.3 d'lat = 0.3' S



MODULE 2.7

departure = 2.8' W d'long = 2.8 sec 35° 10' = <math>3.4'W

DR position	35° 10.0′ S		127° 50.0′ E
d'lat	0.3' S	d'long	3.4′ W
ITP .	35° 10.3′ S		127° 46.6′ E

position line runs 355°/175° through 35° 10.3′ N 127° 46.6′ E

EXERCISE 2.7.2

1. On 19th September at approximate ship's time 1800 in DR position 24° 30′ N 145° 10′ E, at UT 08h 19m 50s. The sextant altitude of the star Arcturus was observed to be 40° 07.7′. Sextant index error 0.8′ on the arc. Height of eye 12.0 metres. Find the direction of the position line and a position through which it passes.

2. On 30th September at approximate ship's time 0600 ship in DR position 43° 05′ N 177° 16′ W, at UT 17h 01m 44s. The sextant altitude of the star Schedar was observed to be 41° 54.4′. Sextant index error 0.2′ off the arc. Height of eye 13.2 metres. Find the direction of the position line and a position through which it passes.

3. On 19th September at the ship in assumed position 17° 53.6′ N 47° 30.0′ W, when the chronometer, which was 04m 53s slow on UT, showed 08h 10m 23s. The sextant altitude of the star Alphard during morning twilight was observed to be 18° 06.5′. Sextant index error 0.5′ on the arc. Height of eye 18.6 metres. Find the direction of the position line and a position through which it passes.

4. On 18th December at approximately 0600 at the ship in DR position 42° 40′ N 172° 10′ W, at UT 17h 29m 30s the sextant altitude of the star Alphecca was observed to be 41° 46.7′. Sextant index error 1.3′ on the arc. Height of eye 17.5 metres. Find the direction of the position line and a position through which it passes.

5. On 27th June at the ship at evening stars in DR position 40° 59.5′ S 56° 57′ W, at UT 21h 26m 00s. The sextant altitude of the star Procyon was observed to be 15° 03.1′. Sextant index error 0.6′ off the arc. Height of eye 9.0 metres. Find the direction of the position line and a position through which it passes.

Example 3

On 30th September at approximate ship's time 1319 in assumed position of 14° 38′ S 54° 14′ W the sextant altitude of the moon's lower limb was observed to be 44° 37.4′. Sextant index error nil. height of eye 12 metres. A chronometer which was correct on UT showed 04h 25m 14s. Find the direction of the position line and a position through which it passes.

approximate LM longitude W approximate UT	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	chron. 04h 25n UT 16h 25n	n 14s n 14s 30th
declination	23° 22.5′ S	sextant altitude	44° 37.4′
'd'	$\pm 3.7'$	index error	_
declination	23° 26.2′ S	observed alt.	44° 37.4′
		dip	-6.1'
GHA 16th	1° 53.1′	apparent alt.	44° 31.3′
increment	6° 01.3′	main corr	+50.8'
'v'	2.3'	2nd corr	+7.1'
GHA	7° 56.7′	true altitude	45° 29.2′
longitude	54° 14.0′ W	zenith dist.	44° 30.8′
LHA 3	313° 42.7′		
angle P	46° 17.3′		

by cosine formula

cosine ZX = cosine PZ cosine PX + sine PZ sine PX cosine P cosine ZX = cosine 75° 22′ cosine 66° 33.8′ + sine 75° 22′ sine 66° 33.8′ cosine 46° 17.3′

= 0.10048 + 0.61345ZX = 44° 26.6'

or

 $\cos ZX = \cos \operatorname{lat} \cos \operatorname{dec} \cos P + \sin \operatorname{lat} \sin \operatorname{dec}$

cos ZX = cos 14° 38′ cos 23° 26.2′ cos 46° 17.3′ + sin 14° 38′ sin 23° 26.2′

 $\cos ZX = 0.61345 + 0.10048$

 $ZX = 44^{\circ} 26.6'$

Calculated ZX 44° 26.6′
True ZX 44° 30.8′
intercept 4.2′ away

A 0.250 N

B <u>0.600 S</u> C <u>0.350 S</u> Azimuth S 71.3° E or 108.7° T

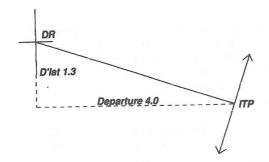


Fig. 2.7.4

From Figure 2.7.4

 $d'lat = 1.3' N departure = 4.0' W <math>d'long = 4.0 sec 14^{\circ} 38' = 4.1' W$

DR position	14° 38.0′ S		54° 14.0′ W
d'lat	1.3' N	d'long	4.1′ W
ITP	14° 36.7′ S		54° 18.1′ W

position line runs 018.7°/198.7° through 14° 36.7′ S 54° 18.1′ W

EXERCISE 2.7.3

- 1. On 28th June at approximately 0620 at a ship in assumed position 42° 50' N 41° 30' W the sextant altitude of the moon's lower limb was 31° 51.8'. A chronometer which was correct on UT showed 09h 10m 02s. Index error 2.0' off the arc. Height of eye 10 metres. Find the direction of the position line and a position through which it passes.
- 2. On 9th January at approximately 1550 hrs at a ship in assumed position 25° 30' N 175° 00' E the sextant altitude of the moon's upper limb was 55° 29.4'. A chronometer which was slow on UT by 1m 24s showed 04h 06m 41s. Index error 2.0' on the arc. Height of eye 7.2 metres. Find the direction of the position line and a position through which it passes.

Longitude by chronometer

In this method a latitude is assumed. This is used in the PZX triangle with declination and the true zenith distance to solve for angle P and hence Local Hour Angle and longitude. This longitude

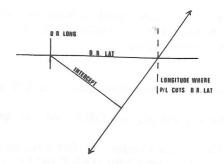


Fig. 2.7.5

will be correct only if the assumed latitude was correct and thus the assumed latitude and calculated longitude give a position through which the position line passes. The direction of the position line must be found as before.

For any one observation there obviously is only one position line regardless of the method used to reduce the observation. The intercept method and the longitude method however result in different positions through which the position line is drawn. Figure 2.7.5 shows the relationship between the information gained from the two methods.

The arguments used to solve the PZX triangle in the longitude by chronometer method are:

- 1. PZ. This is the complement of the latitude.
- 2. PX. This is the complement of the declination.
- 3. ZX. This is the zenith distance or complement of the true altitude.

By cosine formula:

$$cosine P = \frac{cosine ZX - cosine PZ cosine PX}{sine PZ sine PX}$$

or

cosine
$$P = \frac{\text{cosine } ZX - \sin \text{lat} \sin \text{dec}}{\cos \text{lat} \cos \text{dec}}$$
 (lat and dec same name)

cosine
$$P = \frac{\cos ine \ ZX + \sin lat \sin dec}{\cos lat \cos dec}$$
 (lat and dec opposite names)

sine PZ sine PX

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If complements are substituted it must be remembered that sine declination must carry a negative sign if the latitude and declination are of opposite names.

or

Procedure

- 1. From the chronometer time deduce the UT and the date at Greenwich.
- 2. Using the UT extract the GHA and the declination from the almanac.
 - 3. Correct the sextant altitude and obtain the zenith distance.
 - 4. Solve the cosine formula for angle P and hence the LHA.
 - 5. Apply GHA to LHA to obtain the longitude.
 - 6. Find the true bearing and the direction of the position line.

This method is not suitable for bodies which are close to the meridian. As a rule of thumb it may be said that the body should be at least two hours from its meridian passage. It is particularly suitable for observations of the sun in the forenoon which are going to be run up to noon and combined with a latitude by meridian altitude.

Example 4

On 30th September at about 0900 at the ship in DR position 41° 15′ N 175° 30′ W, when a chronometer correct on UT showed 08h 25m 15s, the sextant altitude of the sun's lower limb was 28° 46.7'. Index error 0.4' off the arc. Height of eye 15.8 metres. Find the direction of the position line and a position through which it passes.

approximate Ll longitude W approximate U	11h 42r	<u>n</u>	
UT	20h 25m 15s	30th	
GHA 20h increment GHA	122° 30.1′ 6° 18.8′ 128° 48.9′	sextant altitude index error observed alt. dip	$ \begin{array}{r} 28^{\circ} \ 46.7' \\ +0.4' \\ \hline 28^{\circ} \ 47.1' \\ -7.0' \\ \end{array} $
declination 'd' corr declination	$ \begin{array}{ccc} 2^{\circ} & 52.5' \text{ S} \\ & +0.4' \\ \hline 2^{\circ} & 52.9' \text{ S} \end{array} $	apparent alt. total corr true altitude zenith dist.	28° 40.1′ +14.3′ 28° 54.4′ 61° 05.6′

$$cosine P = \frac{cosine ZX + sin lat sin dec}{cos lat cos dec}$$

cosine P =
$$\frac{\text{cosine } 61^{\circ} \ 05.6' + \sin 41^{\circ} \ 15' \sin 2^{\circ} \ 52.9'}{\cos 41^{\circ} \ 15' \cos 2^{\circ} \ 52.9'}$$
$$= \frac{0.48338 + 0.03315}{0.75089}$$

$P = 46^{\circ} 3$	2.2' A 0.831S
LHA 313° 2	7.8' B 0.069 S
GHA <u>128° 4</u>	$C = \frac{0.900 \text{S}}{0.900 \text{S}}$
longitude 175° 2	.1' Azimuth S 55.9° E or 124 1° T

Position line runs 034.1°/214.1° through 41° 15′ N 175° 21.1′ W

EXERCISE 2.7.4

- 1. On 28th June at approximately 1600 at the ship in DR position 10° 25′ N 71° 00′ E, when the chronometer, which was fast on UT by 4m 27s, showed 11 h 19m 53s, the sextant altitude of the sun's lower limb was 31° 33.3'. Index error 1.2' on the arc. Height of eye 17.0 metres. Find the direction of the position line and the longitude in which it cuts the parallel of the DR latitude.
- 2. On 19th September at approximately 0730 at the ship in DR position 18° 44' N 127° 00' W when the chronometer, which was correct on UT, showed 04h 01m 42s, the sextant altitude of the sun's upper limb was 24° 34.5'. Index error 0.6' off the arc. Height of eye 18.0 metres. Find the direction of the position line and the longitude in which it cuts the parallel of the DR latitude.
- 3. On 20th December during the forenoon at the ship in DR position 35° 24' S 171° 15' E, when the chronometer, which was slow on UT by 1m 17s, showed 09h 00m 35s, the sextant altitude of the sun's lower limb was 43° 09.7'. Index error 0.4' on the arc. Height of eye 14.5 metres. Find the direction of the position line and the longitude in which it cuts the parallel of the DR latitude.
- 4. On 4th January during the forenoon at the ship in DR position 0° 30' S, 0° 04' E when the chronometer, which was correct

on UT, showed 08h 15m 35s, the sextant altitude of the sun's upper limb was 30° 27.1'. Index error 1.4' on the arc. Height of eve 19.5 metres. Find the direction of the position line and the longitude in which it cuts the parallel of the DR latitude.

5. On 30th September at approximately 0800 at the ship in DR position 44° 05' N 20° 05' W at UT 09h 11m 02s, the sextant altitude of the sun's lower limb was 18° 57.5'. Index error 1.4' on the arc. Height of eye 9.0 metres. Find the direction of the position line and the longitude in which it cuts the parallel of the DR latitude.

Noon position by longitude by chronometer and meridian altitude

A standard method of obtaining a noon position when there is only the sun available for observation is to observe the sun when it is bearing close to east in the forenoon and transfer the position line calculated by longitude by chronometer to the time of noon, that is meridian passage of the sun. The transferred position line can then be crossed with a position line obtained from a latitude by meridian altitude. The noon position can be found without any plotting.

Figure 2.7.6 represents such a morning position line which has been run up to give a noon DR position. The transferred position through this DR is shown with double arrows. The figure shows that if the noon latitude gives a latitude to the south of the DR then the ship's position must be to the west. If the noon latitude

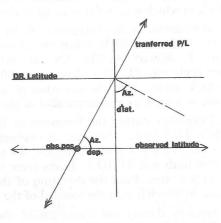


Fig. 2.7.6

is to the north of the DR then the position must be to the east. The amount by which the longitude differs from the DR longitude is given by the number of minutes the noon latitude differs from the DR latitude multiplied by the value 'C' which will have been obtained when working the azimuth at the forenoon sight.

Thus the value 'C' in this respect can be taken as the error in the longitude caused by an error of 1 minute in the latitude.

Example 5

declination

On 19th December at approximate ship's time 0810 in assumed position 25° 50' N 50° 00' \hat{W} an observation of the sun's lower limb gave a sextant altitude of 15° 47.5'. Index error was 3.0' on the arc and height of eye 13.6 metres. The chronometer showed 11h 26m 04s at the time and was slow on UT by 1m 03s. The ship then steamed 210° T for 55 miles, when a meridian altitude of the sun's lower limb was 41° 19.8' south of the observer. Find the ship's position at noon.

Approximate ship's time	0810
longitude in time	0349
approximate UT	1159 19th

arent alt. 15° 3 l corr +1 altitude 15° 5	12.9
a 1	rent alt. 15° 3 corr + altitude 15° 3

$$cosine P = \frac{cosine ZX - sin lat sin dec}{cos lat cos dec}$$

23° 24.5′ S

cosine P =
$$\frac{\text{cosine } 74^{\circ} \ 09.1' + \sin 25^{\circ} \ 50' \sin 23^{\circ} \ 24.5'}{\cos 25^{\circ} \ 50' \cos 23^{\circ} \ 24.5'}$$
$$= \frac{0.27309 + 0.17312}{0.82599}$$

on the arc and height of eye 8.0 metres. The chronometer showed 10h 05m 17s at the time and was correct on UT. The ship then steamed 045° T for 40 miles, when a meridian altitude of the sun's lower limb was 28° 39.4′ north of the observer. Find the ship's

position at noon.

1157		
1157 0322 1519 23° 24.8′	sextant altitude index error observed alt. dip apparent alt. total corr true altitude zenith dist. declination latitude DR lat. difference 'C' long error	41° 19.8′ -3.0′ 41° 16.8′ -6.5′ 41° 10.3′ +15.2′ 41° 25.5′ 48° 34.5′ 23° 24.8′ S 25° 09.7′ N 25° 02.4′ N 7.3′ N 0.826 6.0′ E
long correction	on de	50° 22.1′ W 6.0′ E 50° 16.1′ W 50° 16.1′ W
(noon DR longlong correction	index error observed alt. dip apparent alt. total corr true altitude zenith dist. declination latitude DR lat. difference 'C'

EXERCISE 2.7.5

1. On 30th September during the forenoon in assumed position 46° 17′ S 157° 20′ W an observation of the sun's lower limb gave a sextant altitude of 32° 15′. Index error was 3.0′ off the arc and height of eye 11 metres. The chronometer showed 07h 24m 51s at the time and was correct on UT. The ship then steamed 300° T for 45 miles, when a meridian altitude of the sun's lower limb was 46° 47.9′ north of the observer. Find the ship's position at noon.

MODULE 2.8

Latitude by Pole Star

The altitude of the celestial pole is equal to the observer's latitude. Unfortunately the exact position of the pole is not marked and cannot be observed. However the star Polaris has a declination in excess of 89°, so that it describes daily a circle around the pole of radius less than one degree. As it is so near the pole it is referred to as the pole star and its altitude can be observed and small adjustments made to the altitude to give an easy derivation of the latitude.

Figure 2.8.1 represents the daily path of Polaris around the pole. Its polar distance has been exaggerated. If the star is at X_1 the angular distance PX_1 , the polar distance, must be subtracted from the altitude NX_1 to obtain the altitude of the pole, or the latitude. Similarly if the star is at X_2 then the polar distance must be added to the altitude of the star to give that of the pole. At all other times the correction will be the arc PY in Figure 2.8.1 and this may be

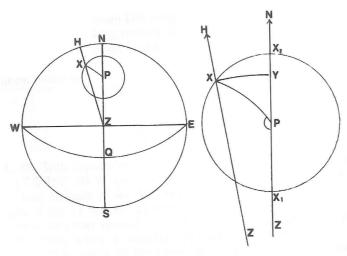


Fig. 2.8.1

positive as shown or negative. The solution of the triangle XPY for PY is tabulated in the Nautical Almanac under the title 'Pole Star Tables'. These are found in the back of the almanac.

The solution is arranged in three separate quantities a^0 , a^1 and a^2 . To each is added a constant, and the sum of the three constants is 1° , which must be subtracted at the end of the calculation. This is done to ensure that all corrections are always positive.

The correction depends upon the LHA of the star. As the SHA can be considered constant for the year it is preferable to tabulate against the argument LHA γ .

Procedure

- 1. From the UT of observation find the GHA γ and apply the DR longitude to get LHA γ .
 - 2. Correct the sextant altitude to obtain true altitude.
- 3. Using LHA γ , enter the pole star tables and find the column which is headed by the value of LHA γ . There is one column for each 10 degrees of LHA. The three corrections will be found in the same vertical column, which is divided into three sections.

The top section is tabulated against each degree of LHA within the 10° range and a^{0} can be extracted with some simple interpolation if necessary.

The middle section is tabulated against latitude and a¹ can be read against the latitude and no interpolation is necessary.

The lower section is tabulated against the month and a² can be read off against the correct month without interpolation.

- 4. The altitude of the pole is given by (true altitude of Polaris $+a^0 + a^1 + a^2 1$).
- 5. Read off the bearing of the star against the latitude from the azimuth table at the foot of the column.

Note: The pole star will not always bear due north and therefore the position line will not be exactly along a parallel. The bearing however will be so close to north that it is usually assumed that the position line does coincide with the observer's parallel. Strictly speaking the latitude derived together with the DR longitude used give a position through which the position line passes with a direction which may be up to 1.7 degrees from east/west.

Example

On 21st September in DR position 37° 58′ N 52° 30′ E at 01h 10m 24s UT an observation of Polaris gave sextant altitude 38° 40.4′. Index error 2.2′ off the arc. Height of eye 11.7m. Find the direction of the position line and a position through which it passes.

011- 10-- 24- 21-4

UT.	01h 10m 24s 21s	st	
GHA γ 01h increment GHA γ longitude E LHA γ	14° 30.0′ 2° 36.4′ 17° 06.4′ 52° 30.0′ 69° 36.4′	sextant altitude index error observed alt. dip apparent alt. total corr true altitude a ⁰ a ¹ a ²	$ \begin{array}{r} 38^{\circ} \ 40.4' \\ $
		total	38° 58.0′ 1°
		latitude	37° 58.0′ N
		bearing	359.6° T

position line runs 269.6°/089.6° through 37° 58.0′ N 52° 30′ E

EXERCISE 2.8.1

- 1. On 8th January at 19h 25m 22s UT in DR position 49° 20' N 36° 20.4' W the sextant altitude of Polaris was 50° 09.4'. The sextant index error was 1.6' off the arc and the height of eye 12.8 metres. Find the direction of the position line and a position through which it passes.
- 2. On 20th September at 21h 15m 40s UT in DR position 35° 25′ N 36° 25′ W the sextant altitude of Polaris was 35° 15.8′. The sextant index error was 0.8′ on the arc and the height of eye 11.5 metres. Find the direction of the position line and a position through which it passes.
- 3. On 27th June at 13h 26m 44s UT in DR position 47° 15′ N 158° 40′ W the sextant altitude of Polaris was 47° 42.0′. The sextant index error was 1.4′ off the arc and the height of eye 6.0 metres. Find the direction of the position line and a position through which it passes.
- 4. On 30th September at about 0520 local time in DR position 50° 40′ N 162° 10.8′ E the sextant altitude of Polaris was 51° 10.8′. The chronometer which was 02m 08s slow on UT showed 06h 13m 17s. The sextant index error was 1.2′ off the arc and the height

of eye 14.0 metres. Find the direction of the position line and a position through which it passes.

REVISION EXERCISES

Paper 1

Chart: Lands End to Falmouth

Use variation 5° W throughout

Use the deviation card in Figure Module 1.3

1. At a time 5 hours after high water Dover on spring tides a vessel was in a position with Lizard Lt. bearing 000° T distant 5 miles. Find the compass course to steer to pass 3 miles to the south of Wolf Rock Light, making allowance for any tide you may expect. Estimate the sailing time to the position off Wolf Rock. Vessel's log speed is 12 knots.

2. From a vessel to the south of Mount's Bay steering 091°C speed 8 knots Black Head was observed in transit with Lizard lighthouse bearing 051°C. After maintaining this course for one hour Lizard lt. hse. bore 309°C. If a current set 070°T at 1.5 knots in the interval find the position of the ship at the time of the second observation.

3. It is required to round Lizard point maintaining a distance off Men Hyr Rocks of 1.5 miles. What would be the vertical sextant angle to set on a sextant to observe Lizard light hse.?

4. A vessel steering 110° C speed 10 knots observed Longships Lt. bearing 345° C and Tater Du Lt. hse. bearing 035° C. 1.5 hours later Lizard Point lt. hse. was bearing 065° C while Mullion Island was bearing 029° C. Find the set and the drift of the tide in the interval.

5. Find by plane sailing the vessel's position at the end of the third course.

Initial position 49° 30′ N 8° 00′ W

1st course 261° T distance 70 miles 2nd course 210° T distance 72 miles 3rd course 166° T distance 65 miles

6. Find by plane sailing the course and distance between the following positions.

50° 15′ N 5° 25′ W 52° 10′ N 7° 05′ W

7. From the following information find the compass error and the deviation for the ship's head.

Date June 27th sun rose bearing 053°C

DR position $50^{\circ} 30' N 6^{\circ} 30' W$

Variation 8° W

Paper 2

Chart: Falmouth to Plymouth

Use 5° W variation throughout

Use the deviation card in Module 1.3

1. From a position where Eddystone Rock Lt. bears 000° T distant 3 miles find the compass course to steer to a position where Dodman Point bears 307° T distant 2.4 miles, in order to counteract a tide estimated to set 133° T at 2 knots and allowing for a 10° leeway due to a SW'ly wind. Ships speed by log 8 knots.

2. The following compass bearings were obtained from a vessel at anchor in Mevagissey Bay:

Chapel Point 238° C Black Head 001° C Gribbin Head daymark 056° C

Find the latitude and longitude of the vessel's position and the compass course to steer to arrive at a position where Rame Head chapel ruins is bearing 000° T by 3 miles.

3. A vessel steering 330° C has the buoy (FL R 10 sec) (50° 07′ N 4° 30′ W approximately) bearing 015° C distant 1.2 miles. After steaming for 40 minutes at 12 knots the vessel's position was fixed by three bearings:

Gribbin Head 003° C Chapel Point 320° C

Find the set and rate of the current, the course and speed made good.

- 4. Find the rising and dipping distance of Eddystone Light from a vessel with height of eye 12.5 metres.
- 5. Find by mercator sailing the position at the end of the run.

Initial position 55° 55′ N 7° 18′ E Course 257° C Variation 8° W Deviation 3° E Distance run 120 miles

6. From the following information find the compass error and the deviation for the ship's head.

Time at ship 1608 29th September. DR position 43° 30'N 9° 40′ W

Bearing of the sun by compass 262°. Chronometer 05h 08m 02s.

Chronometer error 2m 18s slow on UT. Variation 6° W.

Paper 3

Chart: Lands End to Falmouth

Use variation 6° W throughout

Use the deviation card in Module 3

1. At 0800 hrs in poor visibility, from a vessel steering 181° by gyro, speed 5 knots, the Longships lighthouse bore 148°G. Gyro error 1° High. The vessel continued on this course and at 0915 Wolf Rock Lt. was observed to bear 238° G. If a tide set 127° T at 2 knots throughout find the vessels position at 0915.

2. From a position with Wolf Rock Lt. bearing 350°T distance 2.4 miles, find the course and distance to a position 49° 46' N 5° 26.6' W. Find also the compass course to steer to counteract a tide setting 084° T at 3 knots and 6 degrees leeway due to a SW'ly wind, if the vessel's speed by log is 6 knots. What will be the steaming time to the position given.

3. On a vessel at anchor off Falmouth the following compass bearings were taken:

226° C Manacle Point 280° C Rosemullion Head 010° C St Anthony Head Lt.

Find the vessel's position and the error of the compass.

4. At 1000 hrs, the Runnel Stone buoy was observed in transit with Longships lighthouse bearing 318° C. At the same time Wolf Rock bore 251° C. Find the vessel's position. If the course is now set 095° C and 20 minutes later Tater Du Lt. bore 321° C and St Michael's Mount bore 014°C, estimate the set and the drift of the tide if the distance run by log in the interval was 5 miles.

5. Find the times and heights of high and low waters at Sharpness Dock on 14th January.

Paper 4

1. From the following information find the direction of the position line and a position through which it passes:

Time at ship 0825 20th September DR position 5° 58′ S 126° 03′ E Sextant altitude Saturn 50° 39.2′ Index error 1.5' off the arc Ht of eye 14.5 metres Chronometer 00h 27m 38s (correct on UT)

2. Find the GMT and LMT of meridian passage of the star Vega and the setting to put on a sextant to observe this passage:

> Date at ship 19th September DR position 13° 00′ S 138° 55′ E Index error 1.8' Off the arc Height of eye 17.0 metres

- 3. Find by Mercator sailing the course and distance from 48° 11′ S 169° 50′ E to 23° 36′ S 161° 42′ W.
- 4. From the following information find the compass error and the deviation for the ship's head:

Time at ship 1004 18th December DR position 55° 08′ N 5° 13′ E Sun bore 162° by compass Chronometer 10h 02m 17s Chronometer error 1m 40s fast on UT Variation 7° W

Paper 5

1. From the following information find the direction of the position line and a position through which it passes:

> Time at ship 1930 28th June DR position 33° 05′ N 131° 18′ W Sextant altitude Regulus 34° 54.4' Index error 1.0' on the arc Ht of eye 16.7 metres Chronometer 04h 12m 13s Chronometer error 1m 03s fast on UT

2. From the following information find the direction of the position line and a position through which it passes:

> Time at ship 1210 7th January DR position 26° 17′ N 48° 11′ W Sextant altitude Sun LL 41° 16.9' Index error 2.0' on the arc Ht of eye 13.2 metres

Chronometer 03h 18m 06s Chronometer error 7m 14s fast on UT

3. From the following observation of Polaris during evening twilight find the direction of the position line and a position through which it passes:

Date at ship 27th June
DR position 21° 03′ N 153° 16′ W
Sextant altitude 20° 15′
Index error 2.0′ on the arc
Height of eye 11.5 metres
Chronometer 05h 27m 42s
Chronometer error 1m 29s slow on UT

4. From the following sights find the position of the ship at the time of the second observation:

Assumed position 40° 12′ S 94° 30′ E
Observed longitude 94° 33′ E
Bearing 079° T
Run 3.5 hours at 16 knots
Course 352° T
Current 260° T 2 knots
Using assumed position run up intercept 3.0′ Towards
bearing 012° T

Paper 6

1. From the following information find the direction of the position line and a position through which it passes:

Time at ship 1429 29th September DR position 47° 30′ N 45° 20′ W Sextant altitude Sun LL 29° 14.3′ Index error 2.0′ on the arc Ht of eye 6.2 metres Chronometer 05h 29m 13s Chronometer error 1m 03s fast on UT

2. From the following meridian observation find the latitude and state the direction of the position line:

Date at ship 9th January DR position 51° 28′ S 136° 30′ E Sextant altitude Moon's LL 40° 15.7′ Index error nil Height of eye 16.3 metres 3. Find by Mercator sailing the arrival position:

Initial position 46° 45′ N 45° 00′ W Course 337° T distance 245 miles

4. From the following information find the error of the compass and the deviation for the ship's head:

Date at ship 29th September DR position 10° 50′ N 157° 17′ W Sun bore 273° by compass when setting Variation 4° E

Paper 7

1. From the following information find the direction of the position line and a position through which it passes:

Time at ship 1407 9th January DR position 12° 10′ N 50° 05′ W Sextant altitude Moon UL 37° 46.1′ Index error 1.0′ on the arc Ht of eye 6.2 metres Chronometer 17h 25m 01s Chronometer error 0m 48s slow on UT

2. From the following information find the direction of the position line and a position through which it passes:

Time at ship 0508 20th September DR position 38° 40′ S 138° 46′ E Sextant altitude Bellatrix 44° 50.0′ Index error 3.0′ off the arc Ht of eye 9.9 metres Chronometer 08h 12m 19s Chronometer error 2m 18s fast on UT

3. From the following meridian observation find the latitude and state the direction of the position line:

Date at ship 20th September DR position 26° 00' N 116° 30' W Sextant altitude Sun LL 64° 45.0' Index error 1.5' on the arc Height of eye 17.9 metres

4. From the following sights find the position of the ship at the time of the second observation:

Intercept 3.0' Towards Brg 287° T

Run 95 miles

Course 147° T

Time 1830

Using assumed position run up intercept 5.0 Away bearing $030^{\circ} T$

Paper 8

1. From the following information find the direction of the position line and the longitude in which it cuts the DR latitude:

> Time at ship 0840 29th September DR position 30° 40′ N 175° 18′ E Sextant altitude Sun LL 34° 35.0′ Index error 1.0' off the arc Ht of eye 10.3 metres Chronometer 09h 01m 13s Chronometer error nil

2. From the following meridian observation find the latitude and state the direction of the position line:

> Date at ship 6th January DR longitude 96° 35′ E

Sextant altitude Sun UL bearing south 41° 25.0'

Index error 2.0' on the arc Height of eye 11.5 metres

3. From the following observation of Polaris during morning twilight find the direction of the position line and a position through which it passes:

> Date at ship 27th June DR position 47° 15' N 125° 40' W Sextant altitude 47° 52' Index error 0.5' off the arc Height of eye 6.1 metres Chronometer 11h 01m 44s

Chronometer error nil

4. From the following sights worked using the DR position given, find the ship's position at 1746:

Course 071° T speed 20 knots DR position 42° 11′ S 161° 17′ E

REVISION EXERCISES

Time 1731 Intercept 5.8' Towards bearing 026° T Time 1737 Intercept 2.9' Away bearing 272° T Intercept 1.7' Towards bearing 319° T Time 1746

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ANSWERS TO EXERCISES

3. 930' S 7 5. 741' N 12 7. 995' N 37	09' W 41' W 78' W 12' W 26' W	6. 1005'	N 522' E S 300' E N 4425' E	
1. 12° 24.0′ N 3. 42° 08.2′ N	165° 34.0′ W 34° 14.4′ W	Exercise 1.1.2 2. 43° 3′ 4. 17° 4:	7.0' N 17° 46.0' 5.1' S 170° 59.5'	E E
1. 1°E 6. 12°E	2. 14° E 7. 2° W	Exercise 1.3.1 3. 5° E 8. 1° W	4. 1°W	5. 17° W
1. 217.5° T 6. 333° T	2. 004° T 7. 353° T	Exercise 1.3.2 3. 004° T 8. 093.5° T	4. 264.5° T	5. 042.5° T
1. 240° C 6. 325.5° C	2. 008° C 7. 079° C	Exercise 1.3.3 3. 355.5° C 8. 246.5° C	4. 260° C	5. 033.5° C
1. 351.5° T 6. 059° T	2. 347.5° T 7. 085° T	Exercise 1.3.4 3. 160.5° T 8. 200° T	4. 253° T	5. 234° T
		Exercise 1.4.1		
1. 057°	2. 125°	3. 247°	4. 322°	5. 113°
6. 091°	7. 000°	8. 194°	9. 240°	10. 269°
1. 152°T 19.6 4. 343°T		Exercise 1.4.2 2. 296°T 13.3 kr 5. 177°T 14.3 kr	1010	92°T 2.8 knots
		77 - 1 - 1 - 1		
4 0 7 1		Exercise 1.5.1	7.05 miles	
1. 9.7 miles	ror 2º E Bassins	g 057° T 4.	49° 54.2′ N 5° 46	5.7′ W •
5. Compass er	FOR 3 E. Dearing	6	49° 50.0′ N 5° 43	.8' W

Exercise 1.6.1

1.	41° 2	4.6' N	or	S		2	. 70)°	31.7′1	N 01	· S	
3.	9° 22′					4	. 34	18	.5 mile	es		
5.	57° 2	4.6' N	or	59°	04.6' S	6	. 31	0	42' N	23°	07.8' W	
7.	50° 20	$0.1'\mathrm{N}$	or	S		8	. 6°	1	15.1'			
9.	48° 1	1.3′ N	or	S		10	. 39)°	00'N	50°	19.4′ W	

Exercise 1.6.2

1. 11° 08.	9'	2.	49.8 miles
3. 51° 19.	1′ N 28° 57.2′ N	4.	574.5 knots
5. 6° 02.2′		6.	594.9 miles
7 20- 22	6-		

7. 20m 23.6s

10. 894.5 miles

Exercise 1.6.3

1.	Course N 63.9' W distance 259 miles	2. 39° 31.5′ N 166° 11.3′ W
3.	Course S 59° 465' E distance 2620.2 miles	4. 35° 04.7′ S 176° 04.5′ W

Exercis	e 1.6.4	
1. a. 848.9 b. 1862.0 c. 2244.1	d. 3962.7	
2. Course S 30.3° W distance 2212.0 mile	es	
3. Course S 14.2° W distance 1851.2 mile	es	
4. Course S 60.6° E distance 6000.0 miles	3	
5. 18° 40.5′ N 155° 30.7′ E		
6. 11° 24.3' N distance 1355.5 miles		
7. 28° 51.4′ S 00° 35.5′ E		
8. 33° 13.8′ N 150° 07.2′ W		
9. Course S 47° 28' E distance 2633.1 mi	les	

and the same of th

1. Initial course S 5	0° 39.5′ E d	istance 5038.	6 miles		
positions	45° 10.7′ S	90° W	course	S 55.9° E	
	51° 52.4′ S	110° W		S 71.0° E	
	54° 14.1′ S	130° W		N 87.0° E	
	53° 09.9′ S	150° W		N 76.8° E	
	48° 15.5′ S	170° W		N 61.2° E	

2. Distance 4638.8 miles. Initial course S 33° 29.7′ W. Position of Vertex 68° 33.0′ N 58° 28.0′ E

Exercise 1.6.5

- 3. Initial course N 77° 37.7′ W. Final course S 33° 29.7′ W. Distance 1732.3 miles
- 4. Initial course S 67° 30.3′ E. Vertex 40° 44.8′ S 20° 17′ W. Distance 3599 miles
- 5. Great circle distance 5190.4. Mercator distance 5594.1. Saving 403.7 miles

6.	Initial course	N 61° 50	.5' W. Ve	rtex 54° 10.	4' N 160° 19.7'	W. Distar	nce 4076.7	miles
	positions	52°	24.4' N	140° W	course	N 73°	38.4' W	
		54°	10.3' N	160° W		N 89°	44.0' W	
		52°	31.4' N	180°		S 74°	09.7' W	
		46°	50.1' N	160° E		S 58°	49.7' W	

5. 49° 57.0′ N 5° 45.5′ W

7. 49° 58.5′ N 7° 35.7′ W. PL 035°/215°

6. 49° 50.0′ N 5° 43.8′ W

Exercise 1.6.6

- 1. Initial course S 54° 46.3' E. Distance 5484.6 miles. Vertices 70° 54.9' E and 116° 05.2′ E
- 2. Initial course S 73° 56.6' E. Distance 3613.4 miles
- 3. Initial course S 52° 00.4′ E. Distance 5279.6 miles
- 4. Initial course S 69° 23.8′ W. Distance 4804.0 miles
- 5. Distance 6630.6. Course at equator S 48° E

Exercise 1.6.7 (Numerical answers only are given)

- 2. Vertices 42° N 40° E and 42° S 140° W Conv. 42° 1. 090° or 270°
- 4. GC Dist 3539.8m Dep 3856.7m Difference 316.9
- 5. Approx 085°

Exercise 1.7.1

- 1. LW 0135 1.2 metres, HW 0709 13.7 metres, LW 1407 0.9 metres, HW 1938 13.8 metres
- 2. HW 2122 14.1 metres, interval -0407, 3.05 metres
- 3. HW 0837 14.1 metres, interval +0247, 4.2 metres
- 4. 9.9 metres will not dry
- 5. Ht of tide 6.0 metres, interval -0330, 0822 hrs
- 6. Ht of tide 9.0 metres, interval -0132, 1434 hrs
- 7. Interval +0241 Ht of tide 8.0 metres, 53.2 metres above water

Exercise 1.7.2

- 1. LW 0447 0.6 metres, HW 0810 9.5 metres, LW 1715 0.6 metres, HW 2037 9.5 metres
- 2. HW 1931 8.2 metres, 10.7 metres
- 3. HW 0624 12.2 metres, LW 1231 0.4 metres, interval +0406, 2.0 metres
- 4. HW 0914 12.8 metres, LW 1523 0.6 metres, interval + 0246, 8.3 metres
- 5. Ht of tide 8.0 metres, HW 1108 10.8 metres, LW 0521 1.8 metres, interval $-0220,0848\,\mathrm{hrs}$
- 6. Ht of tide 5.5 metres, HW 2001 11.2 metres, LW 0152 1.4 metres, interval +0320, 2321 hrs
- 7. HW 0823 11.3 metres, LW 1609 1.2 metres, interval +0637, 1.2 metres

Exercise 2.1.1

- 1. GHA 333° 28.2' Declination 22° 23.8' S
- 2. GHA 49° 02.2' Declination 1° 29.0' N
- 3. GHA 350° 23.0' Declination 23° 24.5' S
- 4. GHA 81° 20.3' Declination 23° 16.5' N
- 5. GHA 246° 23.6' Declination 2° 37.2' S

Exercise 2.1.2

- 1. GHA 144° 13.9' Declination 8° 30.0' S
- 2. GHA 30° 37.1' Declination 26° 43.3' N
- 3. GHA 335° 49.3' Declination 9° 34.4' S
- 4. GHA 341° 54.5' Declination 0° 44.0' S
- 5. GHA 346° 20.4' Declination 16° 17.8' S
- 6. GHA 271° 57.0' Declination 16° 45.6' N

Exercise 2.1.3

1. LHA 72° 20.2′	2. LHA 68° 59.6′	3. LHA 267° 05.4′
4. LHA 342° 14.7′	5. LHA 143° 07.3′	6. LHA 294° 22.9′
7. LHA 199° 59.2′	8. LHA 63° 39.6′	

Exercise 2.3.1

1. LHA 3	05° 26.1′	Angle P 54° 33.9′ 7	T. Brg S 65.3° E	Error 9.3° W Dev 3.3° W
2. LHA 2	5° 09.5′	Angle P 25° 09.5′ 7	T. Brg N 46.7° W	Error 2.3° E Dev 5.3° E
3. LHA 3	19° 24.0′	Angle P 40° 36.0′ T	. Brg S 37.3° E	Error 15.3° W Dev 19.3° W
4. LHA 3	02° 54.2′	Angle P 57° 05.8' 7	. Brg N 51.2° E	Error 7.8° W Dev 5.8° W
5. LHA 5	1° 35.0′	Angle P 51° 35.0′ T	T. Brg S 77.2° W	Error 5.3° W

Exercise 2.3.2

1. LHA 69° 32.4′	Angle P 69° 32.4′ T. Brg S 69.4° W	Error 19.4° E Dev 23.4° E
2. LHA 51° 23.7′	Angle P 51° 23.7′ T. Brg S 74.8° W	Error 7.8° E Dev 1.3° E
3. LHA 332° 14.5′	Angle P 27° 45.5′ T. Brg S 42.1° E	Error 2.9° E Dev 3.9° E
	Angle P 66° 02′ T. Brg N 50.6° W	Error 6.6° W Dev 0.4° E
	Angle P 105° 44.9′ T. Brg S 33.9° W	Error 6.1° W Dev 2.1° W

Exercise 2.3.3

- 1. Amplitude E 3° 00.4' S. Compass error 4° E
- 2. Amplitude E 2° 12.3' N. Compass error 2.8° E. Deviation 2.2° W
- 3. Amplitude W 31.3° N. Compass error 0.3° E. Deviation 6.3° E
- 4. Amplitude E 30.5° S. Compass error 5.5° W
- 5. Amplitude W 35.9° S. Compass error 0.9° High
- 6. Amplitude E 32.4° N. Compass error 2.4° High

Exercise 2.4.1

1. True attitude 52° 39.6°	2. True altitude 33° 20.1'	3. True altitude 71° 33.2′
4. True altitude 27° 24.1′	5. True altitude 62° 47.1′	6. True altitude 55° 33.6′

Exercise 2.4.2

1. True altitude 47° 21.8′	2. True altitude 32° 17.0′	3. True altitude 21° 05.5′
4. True altitude 47° 06.6'	5. True altitude 37° 02.3'	5. True altitude 12° 08.0'
7. True altitude 53° 14.0′	8. True altitude 23° 08.1'	9. True altitude 51° 47.5'
10. True altitude 14° 26 2'		

Exercise 2.4.3

1. True altitude 63° 52.0′	2. True altitude 35° 10.9'	3. True altitude 58° 23.3'
4. True altitude 77° 43.0′	5. True altitude 22° 32.5′	6. True altitude 39° 15.0'
7. True altitude 51° 27.6′	8. True altitude 44° 08.0'	

Exercise 2.4.4

1. True altitude 52° 39.4′	2. True altitude 33° 20.2'	3. True altitude 71° 33.3′
4. True altitude 27° 24.2′	5. True altitude 62° 46.9'	6. True altitude 55° 33.5'

Exercise 2.4.5

1. True altitude 47° 21.8′	2. True altitude 32° 17.1′	3. True altitude 21° 05.5′
4. True altitude 47° 06.6'	5. True altitude 37° 02.2′	6. True altitude 12° 08.0′

7. True altitude 53° 14.2′ 8. True altitude 23° 08.1′ 9. True altitude 51° 47.6′

10. True altitude 14° 26.3'

Exercise 2.4.6

1.	True altitude 63°	52.0'	2.	True altitude 35°	10.8'	3.	True altitude 58°	22.9'
.4	Tena altituda 77º	12 5'	5	True altitude 220	32 6'	6	True altitude 30°	156

7. True altitude 51° 27.1′ 8. True altitude 44° 07.9′

Exercise 2.5.1

1.	46°	55.2' N	6°	45.6' W	2.	36°	10.1'S	122°	33.6' E	
3.	9°	27.3' N	177°	47.5' E	4.	52°	11.7' N	164°	15.2' W	
5.	34°	14.6' N	40°	28.3' W	6.	10°	14.9' S	25°	46.2' W	
7.	15°	13.8' S	159°	17.5' W	8.	36°	48.6' N	147°	08.1'E	
9.	23°	45.3' N	51°	57.4' W	10.	7°	00.6' S	41°	55.0' W	
11.	41°	23.4' S	114°	36.0' E	12.	19°	34.7' N	161°	10.8' W	
13.	52°	37.5' N	135°	56.8' W	14.	52°	12.6' N	164°	33.5' W	
15.	50°	21.8' N	23°	45.4' W	16.	5°	55.8' N	88°	52.9' E	
17.	30°	30.0' N	46°	13.6' W	18.	32°	06.2' S	115°	27.3' E	

Exercise 2.6.1

- 1. TZX 18° 42.8' Latitude 35° 13.9' N 2. TZX 62° 03.1' Latitude 0° 19.5' S
- 3. TZX 61° 52.7′ Latitude 49° 55.5′ S 4. TZX 18° 44.6′ Latitude 26° 56.2′ S
- 5. TZX 56° 02.2' Latitude 0° 05.4' S

Exercise 2.6.2

- 1. TZX 23° 41.4' Latitude 0° 17.6' N 2. TZX 48° 20.8' Latitude 25° 04.3' S
- 3. TZX 28° 59.0' Latitude 51° 27.7' S 4. TZX 39° 38.0' Latitude 37° 04.1' N
- 5. TZX 53° 12.4' Latitude 51° 31.1'S

Exercise 2.6.3

- 1. Decl. 20° 13.8' S T. Alt. 41° 11.8' Latitude 28° 34.4' N
- 2. Decl. 26° 52.1′ N T. Alt. 30° 54.3′ Latitude 32° 13.6′ S
- 3. Decl. 7° 40.9′ S T. Alt. 70° 28.1′ Latitude 27° 12.8′ S
- 4. Decl. 23° 21.4' S T. Alt. 68° 51.5' Latitude 2° 12.9' S

Exercise 2.6.4

- 1. True altitude 22° 08.6' Latitude 50° 25.0' N
- 2. True altitude 12° 14.9′ Latitude 52° 57.5′ N
- 3. True altitude 21° 40.0′ Latitude 55° 06.6′ N
- 4. True altitude 19° 24.3' Latitude 49° 53.4' S
- 5. True altitude 12° 48.6' Latitude 45° 35.7' S

Exercise 2.7.1

1. LHA 314° 14.9′ Angle P 45° 45.1′ Decl. 23° 19.2′ N T. Alt. 21° 17.8′ CZX 68° 43.8′ Int. 1.6 T. Brg. N 44.9° E ITP 29° 28.9′ S 121° 18.7′ W P/L 134.9°/314.9°

- 2. LHA 45° 24.6′ Angle P 45° 24.6′ Decl. 22° 13.4′ S T. Alt. 48° 36.8′ CZX 41° 17.1′ Int. 6.1 A. Brg. N 87.7° W ITP 32° 15.2′ S 48° 08.8′ W P/L 002.3°/182.3°
- 3. LHA 57° 58.5′ Angle P 57° 58.5′ Decl. 1° 18.1′ N T. Alt. 31° 55.8′ CZX 57° 59.1′ Int. 5.1 A. Brg. N 88.5° W ITP 00° 00.1′ S 160° 49.9′ W P/L 001.5°/181.5°
- 4. LHA 312° 21.9′ Angle P 47° 38.1′ Decl. 23° 23.0′ S T. Alt. 10° 30.6′ CZX 79° 40.6′ Int. 11.2 T. Brg. S 43.6° E ITP 43° 03.9′ N 38° 14.4′ W P/L 046.4°/226.4°
- 5. LHA 296° 17.3′ Angle P 63° 42.7′ Decl. 2° 42.2′ S T. Alt. 16° 32.9′ CZX 73° 26.5′ Int. 0.6 A. Brg. S 69.1° E ITP 44° 05.2′ N 27° 41.8′ W P/L 020.9°/200.9°

Exercise 2.7.2

- 1. LHA 54° 00.3′ Angle P 54° 00.3′ Decl. 19° 10.0′ N T. Alt. 39° 59.6′ CZX 50° 06.6′ Int. 6.2 T. Brg. N 84.9° W ITP 24° 30.6′ N 145° 03.2′ E P/L 005.1°/185.1°
- 2. LHA 77° 00.8' Angle P 77° 00.8' Decl. 56° 33.5' N T. Alt. 41° 47.1' CZX 48° 40.0' Int. 27.1 T. Brg. N 45.7° W ITP 43° 23.9' N 177° 42.6' W P/L 224.3°/044.3°
- 3. LHA 292° 12.5′ Angle P 67° 47.5′ Decl. 8° 40.2′ S T. Alt. 17° 55.4′ CZX 71° 59.1′ Int. 5.5 A. Brg. S 74.3° E ITP 17° 55.1′ N 47° 35.6′ W P/L 015.7°/195.7°
- 4. LHA 303° 25.0′ Angle P 56° 35.0′ Decl. 26° 42.0′ N T. Alt. 41° 36.9′ CZX 48° 13.1′ Int. 10.0 A. Brg. S 89.8° E ITP 42° 40.0′ N 172° 23.6′ W P/L 000.2°/180.2°
- 5. LHA 65° 15.7′ Angle P 65° 15.7′ Decl. 5° 13.1′ N T. Alt. 14° 54.8′ CZX 75° 13.9′ Int. 8.7 T. Brg. N 69.3° W ITP 40° 56.4′ S 57° 07.8′ W P/L 200.7°/020.7°

Exercise 2.7.3

- 1. LHA 292° 34.2′ Angle P 67° 25.8′ Decl. 24° 59.2′ N T. Alt. 32° 48.1′ CZX 57° 09.6′ Int. 2.3 A. Brg. N 85° E ITP 42° 49.8′ N 41° 33.1′ W P/L 355°/175°
- 2. LHA 340° 17.2′ Angle P 19° 42.8′ Decl. 2° 54.8′ S T. Alt. 55° 38.3′ CZX 34° 14.2′ Int. 7.5 A. Brg. S 36.8° E ITP 25° 36.0′ N 174° 55.0′ E P/L 053°/233°

Exercise 2.7.4

- GHA 348° 04.1′ TZX 58° 20.8′ LHA 59° 53.0′ Longitude 71° 48.9′ E Brg N 69° W PL 201°/011°
- GHA 61° 58.0′ TZX 65° 50.3′ LHA 295° 03.9′ Longitude 126° 54.1′W Brg S 82.9° E PL 007°/187°
- 3. GHA 136° 11.6′ TZX 46° 42.2′ LHA 307° 31.3′ Longitude 171° 19.7′ E Brg N 90° E PL 000°/180°
- 4. GHA 302° 42.6′ TZX 59° 59.8′ LHA 302° 35.3′ Longitude 0° 07.3′W Brg S 63.8° E PL 026.2°/206.2°
- 5. GHA 320° 13.3′ TZX 70° 56.0′ LHA 300° 03.7′ Longitude 20° 09.6′W Brg S 66.2° E PL 023.8°/203.8°

Exercise 2.7.5

- GHA 113° 42.7′ TZX 57° 33.3′ LHA 314° 27.7′ Forenoon longitude 157° 15.0′ W Brg N 54.6° E PL 144.6°/324.6°. Noon DR 45° 54.5′ S 158° 11.2′. Longitude correction 0.2′ E. Noon position 45° 54.7′ S 158° 11.0′ W
- GHA 150° 33.6′ TZX 72° 34.9′ LHA 319° 00.0′ Forenoon longitude 168° 26.4′ W Brg N 39.1° E PL 129.1°/309.1°. Noon DR 37° 46.7′ S 169° 02.3′. Longitude correction 11.3′ E. Noon position 37° 53.9′ S 169° 13.6′ E

Exercise 2.8.1

- 1. LHA γ 2° 55.9′ Position 49° 29.1′ N 36° 20.4′ W PL 090.6°/270.6°
- 2. LHA γ 281° 50.8′ Position 35° 27.6′ N 36° 25′ W PL 090.9°/270.9°
- 3. LHA Y 318° 15.7′ Position 47° 31.1′ N 158° 40′ W PL 091.1°/271.1°
- 4. LHA Y 84° 07.7' Position 50° 34.1' N 162° 10.8' W PL 089.2°/269.2°

Paper 1

- 1. 281°C, 1h 42m
- 2. 49° 53.7′ N 5° 05.7′ W
- 3. 1° 27′
- 4. Second position 49° 54.6' N 5° 20.4' W, tide 330° 1.7 knots
- 5. 47° 03.5′ N 10° 14.3′ W
- 6. Course N 281/2° W, distance 131.0 miles
- 7. Compass error 1.5° W, deviation 6.5° E

Paper 2

- 1. 282½°
- 2. 50° 16.3′ N 4° 44.6′ W, 094½° C
- 3. Tide 221° 1.5 knots, course and speed made good 315° 11.8 knots
- 4. 20.65 miles
- 5. 55° 17.9′ N 3° 56.1′ E
- 6. Compass error 71/2° W, deviation 11/2° W

Paper 3

- 1. 49° 58.5′ N 5° 44.0′ W
- 2. Course and distance 121° T 16.2 miles. 134½°. Steaming time 1h 58m
- 3. 50° 07.1′ N 5° 00.5′ W, 20° W
- 4. 49° 59.6′ N 5° 37.9′ W, tide 349° 2.1 knots
- 5. LW 0500 0.6m, HW 0824 8.7m, LW 1720 0.6m, HW 2046 8.5m

Paper 4

- 1. LHA 28° 24.2′, CZX 39° 33.0′, TZX 39° 26.8′, intercept 6.2′ towards, brg N 43.8° W ITP 5° 53.5′ S 125° 58.7′ E 226.2°/046.2°
- 2. UT 0929, LMT 1841 19th. 38° 19.3'
- 3. Course N 42° 50.3′ E, distance 2011.5 miles
- 4. LHA 336° 16.7′ Error 4° W, Deviation 3° E

Paper 5

- 1. LHA 56° 11.7′, CZX 55° 18.7′, TZX 55° 15.2′, intercept 3.5′ towards, brg 261½° ITP 33° 04.5′ N 131° 22.1′ W, PL 171½°/351½°
- 2. LHA 357° 58.9′, CZX 48° 41.5′, TZX 48° 36.3′, intercept 5.2′ towards, brg 177½°, ITP 26° 11.8′ N 48° 10.7′ W, PL 267½°/087½°
- 3. LHA γ 204° 56.0′, latitude 20° 46.8′ N, PL 269.8°/089.8°
- 4. 39° 15.1′ S 94° 13.2′ E

ANSWERS TO EXERCISES

Paper 6

- LHA 39° 07.0′, CZX 60° 30.8′, TZX 60° 37.8′, intercept 7.0′ away, brg S 46.4° W ITP 47° 34.8′ N 45° 12.5′ W, PL 136½°/316½°
- 2. Declination 1° 59.7′ S, latitude 51° 25.7′ N
- 3. 50° 30.5′ N 47° 24.5′ W
- 4. Declination 2° 38.0′ S, error 6° W, deviation 10° W

Paper 7

- LHA 309° 13.6', CZX 51° 48.9', TZX 51° 52.4', intercept 3.5' away, brg 099.8°, ITP 12° 10.6' N 50° 08.5' W, PL 189.8°/009.8°
- 2. LHA 358° 15.5′, CZX 45° 03.1′, TZX 45° 13.5′, intercept 10.4′ away, brg N 2½° E ITP 38° 50.4′ S 138° 45.4′ E, PL 272½°/092½°
- 3. Declination 1° 01.4′ N, latitude 26° 09.8′ N, PL 090°/270°
- 4. 22° 33.9′ N 91° 15.1′ W

Paper 8

- 1. LHA 312° 56.7′, CZX 55° 28.3′, TZX 55° 15.0′, intercept 13.3′ towards, brg S 62.6° E, ITP 30° 33.9′ N 175° 31.7′ E, PL 207½°/027½°
- 2. Declination 22° 32.5′ S, latitude 26° 27.6′ N, PL 090°/270°
- 3. LHA Υ 314° 54.8′, latitude 47° 42.7′ N, PL 091.1°/271.1°
- 4. 42° 03.5′ S 161° 25.0′ E

Extracts from the Nautical Almanac 2003

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A2ALTITUDE CORRECTION TABLES 10°-90°—SUN, STARS, PLANETS

App. Alt. = Apparent altitude = Sextant altitude corrected for index error and dip.

					CTARC
UT ARIES	VENUS -4.5	MARS +1.5	JUPITER -2.5	SATURN -0.4	STARS
GHA	GHA Dec	GHA Dec	GHA Dec	GHA Dec	Name SHA Dec
d h 0 / 400 103 11.4 01 118 13.9 02 133 16.4 03 148 18.8 04 163 21.3	228 06.3 S15 53.9 243 06.3 S4.4 258 06.3 55.0 273 06.3 55.5 288 06.4 56.0	233 55.9 S17 30.1 248 56.8 30.5 263 57.6 30.9 278 58.4 . 31.4 293 59.3 31.8 309 00.1 32.3	323 52.3 N16 36.0 338 55.0 36.1 353 57.7 36.2 9 00.4 . 36.3 24 03.1 36.3 39 05.8 36.4	19 25.9 N22 02.2 34 28.6 02.2 49 31.2 02.2 64 33.9 . 02.2 79 36.6 02.2 94 39.2 02.2	Acamar 315 24.3 S40 17.8 Achernar 335 32.6 S57 13.7 Acrux 173 18.7 S63 06.6 Adhara 255 18.6 S28 58.5 Aldebaran 290 58.6 N16 30.9
05 178 23.7 06 193 26.2 07 208 28.7 08 223 31.1 09 238 33.6 10 253 36.1	303 06.4 56.6 318 06.4 \$15 57.1 333 06.4 57.7 348 06.4 58.2 3 06.5 58.8 18 06.5 59.3	324 01.0 S17 32.7 339 01.8 33.1 354 02.6 33.6 9 03.5 . 34.0 24 04.3 34.4	54 08.4 N16 36.5 69 11.1 36.6 84 13.8 36.7 99 16.5 . 36.7 114 19.2 36.8	109 41.9 N22 02.2 124 44.6 02.2 139 47.2 02.2 154 49.9 . 02.2 169 52.6 02.2	Alioth 166 27.7 N55 56.4 Alkaid 153 05.4 N49 17.7 Al Na'ir 27 54.2 S46 57.7 Alnilam 275 54.4 S 1 12.0 Alphard 218 03.9 S 8 40.2
11 268 38.5 12 283 41.0 13 298 43.5 14 313 45.9 15 328 48.4 16 343 50.9	93 06.5 02.0	39 05.1 34.9 54 06.0 S17 35.3 69 06.8 35.8 84 07.7 36.2 99 08.5 36.6 114 09.3 37.1	174 30.0 37.1 189 32.7 . 37.2 204 35.4 37.3	199 57.9 N22 02.2 215 00.6 02.2 230 03.2 02.2 245 05.9 . 02.2 260 08.6 02.2	Alphecca 126 18.2 N26 42. Alpheratz 357 52.2 N29 06. Altair 62 16.6 N 8 52. Ankaa 353 23.7 \$42 17. Antares 112 36.7 \$26 26.
17 358 53.3 18 13 55.8 19 28 58.2 20 44 00.7 21 59 03.2 22 74 05.6	123 06.5 03.1 138 06.5 \$16 03.6 153 06.6 04.2 168 06.6 04.7 183 06.6 05.3 198 06.6 05.8	129 10.2 37.5 144 11.0 \$17 37.5 159 11.8 38.4 174 12.7 38.6 189 13.5 . 39.0 204 14.3 39.0	234 40.8 N16 37.5 249 43.5 37.5 264 46.2 37.6 2 279 48.9 37.7 7 294 51.6 37.8	275 11.2 02.2 290 13.9 N22 02.2 305 16.6 02.2 320 19.2 02.2 335 21.9 . 02.2 350 24.6 02.2 5 27.2 02.2	Arcturus 146 03.3 N19 09. Atria 107 46.5 S69 01. Avior 234 20.9 S59 31. Bellatrix 278 40.5 N 6 21. Betelgeuse 271 09.9 N 7 24.
23 89 08.3 500 104 10.4 01 119 13.4 02 134 15.3 03 149 18.4 04 164 20.4	213 06.6 06.3 6 228 06.6 \$16 06.9 0 243 06.6 07.4 5 258 06.6 08.0 0 273 06.6 08.5	234 16.0 S17 40. 249 16.8 41. 264 17.7 41. 279 18.5 . 41. 294 19.3 42.	5 324 57.0 N16 37.9 0 339 59.7 38.0 4 355 02.4 38.1 8 10 05.1 38.2 3 25 07.8 38.3	20 29.9 N22 02.2 35 32.6 02.2 50 35.2 02.2 65 37.9 . 02.2 80 40.5 02.2 95 43.2 02.2	Canopus 263 59.3 S52 41. Capella 280 46.2 N46 00. Deneb 49 37.6 N45 17. Denebola 182 41.9 N14 33. Diphda 349 04.1 S17 58
05 179 22. 06 194 25. 07 209 27. 08 224 30. S 09 239 32. U 10 254 35.	9 303 06.6 09.6 4 318 06.5 \$16 10.3 8 333 06.5 10.3 3 348 06.5 11.3 7 3 06.5 . 11.3 2 18 06.5 12.3	324 21.0 S17 43. 7 339 21.8 43. 2 354 22.7 44. 7 9 23.5 44. 3 24 24.3 44.	1 55 13.2 N16 38.4 6 70 15.9 38.5 0 85 18.6 38.6 4 100 21.3 38.7 9 115 24.0 38.8	110 45.9 N22 02.2 125 48.5 02.2 140 51.2 02.2 155 53.9 . 02.2 170 56.5 02.2	Elnath 278 22.7 N28 36 Eltanin 90 50.5 N51 29 Enif 33 55.5 N 9 53 Fomalhaut 15 33.2 S29 36
N 11 269 37. D 12 284 40. A 13 299 42. Y 14 314 45. 15 329 47. 16 344 50. 17 359 52	1 48 06.5 \$16 13.4 6 63 06.5 13.1 1 78 06.5 14.5 5 93 06.4 15.0 0 108 06.4 15.	4 54 26.0 S17 45. 9 69 26.8 46. 4 84 27.7 46 0 99 28.5 47 5 114 29.3 47	7 145 29.4 N16 38.9 1 160 32.1 39.0 6 175 34.8 39.1 0 190 37.6 39.0 4 205 40.3 39.3	201 01.9 N22 02.2 0 216 04.5 02.2 1 231 07.2 02.2 2 246 09.9 . 02.2 2 261 12.5 02.2 3 276 15.2 02.2	Gacrux 172 10.3 S57 07 Gienah 176 00.8 S17 33 Hadar 149 00.0 S60 22 Hamal 328 10.0 N23 26 Kaus Aust. 83 55.1 S34 23
17 359 52 18 14 54 19 29 57 20 44 59 21 60 02 22 75 04 23 90 07	9 138 06.4 S16 16. 4 153 06.4 17. 9 168 06.4 17. 3 183 06.3 . 18. 8 198 06.3 18.	6 144 31.0 S17 48 1 159 31.8 48 7 174 32.7 49 2 189 33.5 . 49 7 204 34.3 50	.7 250 48.4 39.1 .2 265 51.1 39.1 .6 280 53.8 . 39.1 .0 295 56.5 39.1 .4 310 59.2 39.1	5 306 20.5 02.2 6 321 23.2 02.2 6 336 25.8 . 02.1 7 351 28.5 02.1 8 6 31.2 02.1	2 Markab 13 46.7 N15 1: Menkar 314 23.5 N 4 0: 1 Menkent 148 17.5 S36 2: Miaplacidus 221 40.9 S69 4:
600 105 09 01 120 12 02 135 14 03 150 17 04 165 19	.7 228 06.3 S16 19 .2 243 06.2 20 .6 258 06.2 20 .1 273 06.2 . 21 .6 288 06.2 22	8 234 36.0 \$17 50 4 249 36.8 51 .9 264 37.7 51 .4 279 38.5 52 .0 294 39.3 52	.3 341 04.6 40.	0 36 36.5 02. 1 51 39.2 02. 1 66 41.8 02. 2 81 44.5 02.	1 Nunki 76 08.9 S26 1 1 Peacock 53 32.6 S56 4 1 Pollux 243 37.4 N28 0 1 Procyon 245 08.0 N 5 1
M 09 240 33 O 10 255 3	318 06.1 \$16 23 7.0 333 06.1 23 9.4 348 06.0 24 1.9 3 06.0 24 1.8 18 06.0 25	.0 324 41.0 S17 53 .6 339 41.8 53 .1 354 42.6 54 .7 9 43.5 56 .2 24 44.3 55	3.4 56 18.1 N16 40. 3.9 71 20.9 40. 4.3 86 23.6 40. 4.7 101 26.3 40. 5.1 116 29.0 40. 5.6 131 31.7 40.	.5 126 52.5 02. .6 141 55.1 02. .6 156 57.8 . 02. .7 172 00.5 02.	1 Regulus 207 52.0 N11 5 1 Rigel 281 19.7 S 8 1 1 Rigil Kent. 140 03.6 S60 5 1 Sabik 102 22.3 S15 4
N 11 270 34 D 12 285 3 A 13 300 4 Y 14 315 4 Y 15 330 4 16 345 4	9.3 48 05.9 \$16 26 1.7 63 05.9 26 4.2 78 05.8 27 6.7 93 05.8	5.3 54 46.0 \$17 5 5.8 69 46.8 5 7.3 84 47.6 5 7.9 99 48.5 5 3.4 114 49.3 5	146 34.4 N16 40 6.4 161 37.1 41 6.8 176 39.8 41 7.3 191 42.5 . 41 7.7 206 45.2 41 8.1 221 48.0 41	.0 217 08.4 02 .1 232 11.1 02 .1 247 13.8 . 02 .2 262 16.4 02 .3 277 19.1 02	1. Shaula 96 33.5 537 (1) 1. Sirius 258 40.7 \$16 4 (1) 1. Spica 158 40.0 \$11 1 1. Suhail 222 58.2 \$43.3
18 15 5 19 30 5 20 45 5 21 61 0	4.1 138 05.6 S16 24 6.5 153 05.6 30 9.0 168 05.6 30 1.5 183 05.5 3 3.9 198 05.5 3	9.5 144 50.9 \$17 5 0.0 159 51.8 5	8.5 236 50.7 N16 41 9.0 251 53.4 41 9.4 266 56.1 41 9.8 281 58.8 . 41 0.2 297 01.5 41	.4 292 21.8 N22 02 .5 307 24.4 02 .5 322 27.1 02 .6 337 29.7 02 .7 352 32.4 02 .8 7 35.1 02	1.1 Zuben'ubi 137 14.7 \$16 0 1.1 SHA Mer.P 1.1 Venus 123 56.0 8

	T		T					Ť	Tw	ilight	1	T,	Mo	onrise	
UT	SU	N		N	MOON			Lat.	Naut.	Civil	Sunrise	4	5	6	7
	GHA	Dec	GHA	v	Dec	d	HP	N 72	h m	h m	h m	h m	h m	h m	h
400	178 51.1 9	S22 47.1	162 27.9	6.8	S24 28.3	5.0	57.7	N 70	08 02	09 43			14 12	13 24	
01	195 50.8	46.9 46.6	176 53.7 191 19.5	6.8				68	07 47	09 13	11 32		12 51	12 19	12 0
03		. 46.4	205 45.5	7.0	24 18.1 24 12.8			66	07 35 07 25	08 50 08 32	10 21	12 43 11 48	12 12 11 45	11 58	
04	200.0	46.1	220 11.5	7.2	24 07.4	5.6	57.6	62	07 16	08 17	09 20	11 15	11 24	11 28	
05		45.9	234 37.7	7.2	24 01.8			60	07 08	08 04	09 00	10 51	11 07	11 16	11 2
07	268 49.4 S	45.4	249 03.9 263 30.2	7.3	S23 56.2 23 50.3	5.9		N 58 56	07 01 06 55	07 53 07 44	08 44 08 30	10 31 10 15	10 52	11 06	
9 08		45.1	277 56.7	7.5	23 44.4	6.1	57.5	54	06 49	07 35	08 18	10 15	10 29	10 57	11 0
A 09		. 44.8 44.6	292 23.2 306 49.8	7.6 7.7	23 38.3			52 50	06 44	07 27	08 07	09 49	10 19	10 42	10 5
, îî	343 48.0	44.3	321 16.5	7.7	23 25.7			45	06 39 06 28	07 20 07 05	07 58 07 38	09 38 09 16	10 11 09 52	10 35	10 5
12		22 44.1	335 43.3	7.9	\$23 19.2	6.6		N 40	06 18	06 52	07 22	08 57	09 37	10 10	10 3
13	13 47.4 28 47.1	43.8 43.5	350 10.2 4 37.2	8.0	23 12.6 23 05.8			35 30	06 09	06 41	07 09	08 42	09 24	10 00	10 3
15	43 46.8 .	. 43.3	19 04.3	8.2	22 59.0			20	06 01 05 45	06 30 06 12	06 57 06 36	08 29	09 13 08 54	09 51 09 36	10 2
16	58 46.6	43.0	33 31.5	8.3	22 52.0	7.1	57.2	N 10	05 29	05 56	06 18	07 46	08 37	09 23	10 0
17	73 46.3 88 46.0 S	42.7	47 58.8	8.3	22 44.9			0	05 13	05 39	06 02	07 28	08 21	09 11	09 5
19	103 45.7	42.2	62 26.1 76 53.6	8.5	S22 37.6 22 30.3			S 10 20	04 55 04 33	05 22 05 02	05 45 05 26	07 09 06 49	08 05 07 48	08 58	09 4
20		42.0	91 21.2	8.7	22 22.8	7.6	57.1	30	04 05	04 38	05 05	06 26	07 29	08 29	09 2
21 22	133 45.1 . 148 44.9	. 41.7 41.4	105 48.9 120 16.7	9.0	22 15.2 22 07.5			35 40	03 47	04 23	04 53	06 13	07 17	08 20	09 2
23	163 44.6	41.1	134 44.7	9.0	21 59.7			45	03 25 02 55	04 06 03 44	04 38 04 21	05 57 05 38	07 04 06 48	08 10 07 58	09 1
500	178 44.3 S	22 40.9	149 12.7	9.1	\$21 51.8	8.0		S 50	02 13	03 16	03 59	05 15	06 29	07 43	08 5
01	193 44.0 208 43.7	40.6 40.3	163 40.8 178 09.0	9.2	21 43.8 21 35.6		56.9 56.9	52 54	01 48 01 11	03 01 02 45	03 49	05 04	06 20	07 37	08 5
03	223 43.4 .	. 40.1	192 37.3	9.4	21 27.4			56	////	02 45	03 37 03 24	04 51 04 36	06 10 05 58	07 29	08 4
04 05	238 43.2 253 42.9	39.8 39.5	207 05.7 221 34.3	9.6	21 19.0			58	1111	01 57	03 08	04 19	05 44	07 11	08 3
06	268 42.6 S		236 02.9	9.6 9.7	21 10.6 S21 02.0			S 60	////	01 18	02 49	03 57	05 28	06 59	08 2
07	283 42.3	39.0	250 31.6	9.9	20 53.3		56.8	Lat.	Sunset	Twil	ight		Mod	onset	
08	298 42.0 313 41.7 .	38.7 . 38.4	265 00.5 279 29.4	9.9	20 44.6	8.9	56.7			Civil	Naut.	4	5	6	7
10	328 41.5	38.1	293 58.4		20 26.8	8.9 9.1	56.7 56.7	0	h m	h m	h m	h m	h m	h m	h
11	343 41.2	37.9	308 27.6	10.2	20 17.7	9.1	56.6	N 72		13 40	15 51			17 41	20 0
12 13	358 40.9 S 13 40.6	37.6	322 56.8 337 26.2		S20 08.6 19 59.3	9.3	56.6 56.6	N 70 68	12 39	14 28 14 58	16 09 16 24		15 11 16 31	18 17 18 43	20 2
14	28 40.3	37.0	351 55.7	10.5	19 50.0	9.4	56.6	66	13 50	15 21	16 36	14 49	17 09	19 02	20 4
15 16	43 40.1 . 58 39.8	. 36.7 36.5	6 25.2 20 54.9		19 40.6 19 31.0	9.6	56.5 56.5	64 62	14 26 14 51	15 39 15 54	16 46 16 55	15 43 16 15	17 35	19 18	20 5
17	73 39.5	36.2	35 24.6	10.9	19 21.4	9.6	56.5	60	15 11	16 07	17 03	16 15	17 55 18 11	19 30	21 0
18	88 39.2 S		49 54.5		S19 11.8	9.8	56.4	N 58	15 27	16 18	17 10	16 58	18 25	19 51	21 1
19	103 38.9	35.6 35.3	64 24.5 1 78 54.5		19 02.0 18 52.1	9.9	56.4 56.4	56 54	15 41	16 27	17 16	17 14	18 37	19 59	21 1
21	133 38.4 .	. 35.0	93 24.7		18 42.2		56.3	52	15 53 16 03	16 36 16 44	17 22 17 27	17 27 17 39	18 47 18 56	20 06 20 12	21 2
	148 38.1 163 37.8	34.8	107 55.0		18 32.2	10.1	56.3	50	16 13	16 51	17 32	17 50	19 05	20 18	21 2
	178 37.6 Si	34.5	122 25.4		18 22.1		56.3	45	16 33	17 06	17 43	18 11	19 22	20 31	21 3
OT	193 37.3		136 55.8 1 151 26.4 1	11.6	\$18 11.9 18 01.6		56.3 56.2	N 40 35	16 49 17 02	17 19 17 30	17 53 18 02	18 29 18 44	19 36 19 48	20 41 20 50	21 4
02	208 37.0 223 36.7	33.6	165 57.0	11.8	17 51.3	10.4	56.2	30	17 14	17 40	18 10	18 56	19 58	20 58	21 5
	223 36.7 . 238 36.4		180 27.8 1 194 58.7 1		17 40.9 17 30.4		56.2 56.1	20 N 10	17 34 17 52	17 58 18 15	18 26 18 41	19 18 19 36	20 16 20 31	21 11	22 0
05	253 36.2		209 29.6		17 19.9		56.1	0	18 09	18 31	18 57	19 54	20 45	21 22 21 33	22 1
06	268 35.9 S2		224 00.7		\$17 09.3		56.1	S 10	18 26	18 49	19 16	20 11	21 00	21 43	22 2
	283 35.6 298 35.3		238 31.8 1 253 03.0 1		16 58.6 16 47.8	10.8	56.1 56.0	20 30	18 44 19 05	19 09 19 33	19 37	20 29 20 50	21 15 21 32	21 55 22 07	22 3
09	313 35.1 .	. 31.6	267 34.4 1	12.4	16 37.0	10.9	56.0	35	19 18	19 47	20 23	21 03	21 42	22 15	22 3
	328 34.8 343 34.5		282 05.8 1 296 37.3 1		16 26.1 16 15.2		56.0 55.9	40 45	19 32 19 49	20 05	20 45	21 17	21 53	22 23	22 4
1000	358 34.2 S2	-	311 08.9 1		\$16 04.2		55.9	S 50	19 49	20 26	21 14	21 33 21 54	22 06 22 22	22 32 22 44	22 5
13	13 33.9	30.4	325 40.6 1	12.8	15 53.1	11.2	55.9	52	20 21	21 08	22 21	22 03	22 22	22 44	23 0
14	28 33.7 43 33.4 .		340 12.4 1 354 44.3 1		15 41.9 15 30.7		55.9 55.8	54 56	20 33 20 46	21 25	22 57	22 14	22 38	22 55	23 0
16	58 33.1	29.5	9 16.3 1	13.0	15 19.5	11.3	55.8	58	20 46	21 45 22 12	1111	22 26 22 41	22 47 22 58	23 02 23 09	23 1
17	73 32.8	29.2	23 48.3 1		15 08.2		55.8	S 60	21 20	22 50	1111	22 57	23 10	23 17	23 2
18 19	88 32.6 S2 103 32.3	28.9	38 20.4 1 52 52.7 1		\$14 56.8 14 45.4		55.7 55.7			SUN	4		МО	ON	
20	118 32.0	28.3	67 25.0 1		14 33.9		55.7	Day	Eqn. of		Mer.	Mer.	Pass.	Age F	hase
	133 31.7 .	. 28.0	81 57.4 1		14 22.4		55.7		00 ^h	12 ^h	Pass.	Upper	Lower		
	148 31.5	27.6	96 29.9 1 111 02.4 1		14 10.8 \$13 59.2		55.6 55.6	d 4	m s 04 35	m s 04 49	h m 12 05	h m 13 41	h m 01 13	d %	
	163 31.2	27.3													
23		d 0.3		15.6	15.4		15.2	5	05 02 05 29	05 16 05 43	12 05 12 06	14 33 15 22	02 08 02 58	03 8 04 15	

24		200	0 0/1	TOATT	٠,	0, 0 (1		.,	,				_
UT	ARIES	VENUS	-4.5	MARS	+1.5	JUPITER -	-2.5	SATUR	N -0	0.4	S	TARS	11
	GHA	GHA	Dec	GHA	Dec		ec	GHA	Dec		Name	SHA	Dec
01 02 03 04	106 08.8 121 11.3 136 13.8 151 16.2 166 18.7	243 05.3 258 05.3 273 05.2 . 288 05.2	0 / 16 32.7 33.2 33.8 . 34.3 34.8 35.4	234 55.9 249 56.7 264 57.6 279 58.4 294 59.2 310 00.1	S18 01.1 01.5 01.9 02.3 02.8 03.2	327 06.9 N16 342 09.7 357 12.4 12 15.1 27 17.8 42 20.5	41.9 42.0 42.1 42.1 42.2 42.3	22 37.7 37 40.4 52 43.0 67 45.7 82 48.4 97 51.0	0	2.1 2.1 2.1 2.1 2.1 2.1	Acrux Adhara	315 24.3 335 32.6 173 18.7 255 18.6 290 58.6	S63 06.
06 07 08 09 09	181 21.2 196 23.6 211 26.1 226 28.6 241 31.0 256 33.5 271 36.0	303 05.1 318 05.1 S 333 05.0 348 04.9 3 04.9 . 18 04.8 33 04.8		325 00.9 340 01.7 355 02.5 10 03.4 25 04.2 40 05.0	5,000	57 23.2 N16 72 25.9 87 28.6 102 31.4 117 34.1 132 36.8		112 53.7 127 56.3 142 59.0 158 01.7 173 04.3 188 07.0	N22 0		Al Na'ir Alnilam Alphard	166 27.7 153 05.3 27 54.2 275 54.4 218 03.9	N49 17. S46 57. S 1 12. S 8 40.
S 12 D 13 A 14	286 38.4 301 40.9 316 43.3 331 45.8 346 48.3 1 50.7		39.1 39.6 40.2 . 40.7 41.2 41.8	55 05.9 70 06.7 85 07.5 100 08.3 115 09.2 130 10.0	\$18 06.1 06.6 07.0 07.4 07.8 08.2	147 39.5 N16 162 42.2 177 44.9 192 47.7 207 50.4 222 53.1	42.9 43.0 43.1 43.1 43.2 43.3	203 09.6 218 12.3 233 15.0 248 17.6 263 20.3 278 22.9	0)2.1)2.1)2.1)2.1)2.1)2.1	Altair Ankaa	112 36.7	N29 06 N 8 52 S42 17 S26 26
18 19 20 21 22 23	16 53.2 31 55.7 46 58.1 62 00.6 77 03.1 92 05.5		42.8 42.8 43.3 43.9 44.4 44.9	145 10.8 160 11.6 175 12.5 190 13.3 205 14.1 220 14.9	\$18 08.7 09.1 09.5 09.9 10.3 10.7	237 55.8 N16 252 58.5 268 01.2 283 04.0 298 06.7 313 09.4	43.4 43.5 43.6 43.7 43.7 43.8	293 25.6 308 28.3 323 30.9 338 33.6 353 36.2 8 38.9	()2.1)2.1)2.1)2.1)2.1)2.1	Arcturus Atria Avior Bellatrix Betelgeuse	146 03.3 107 46.5 234 20.9 278 40.5 271 09.9	S69 01 S59 31 N 6 21 N 7 24
800 01 02 03 04 05	107 08.0 122 10.4 137 12.9 152 15.4 167 17.8 182 20.3		616 45.5 46.0 46.5 . 47.1 47.6 48.1	235 15.8 250 16.6 265 17.4 280 18.2 295 19.1 310 19.9	\$18 11.2 11.6 12.0 12.4 12.8 13.2	328 12.1 N16 343 14.8 358 17.5 13 20.3 28 23.0 43 25.7	43.9 44.0 44.1 44.2 44.3	23 41.5 38 44.2 53 46.9 68 49.5 83 52.2 98 54.8	: (: (02.1 02.1 02.1 02.1 02.1 02.1	Canopus Capella Deneb Denebola Diphda	182 41.9 349 04.1	N46 00 N45 17 N14 33 S17 58
06 W 07 E 08 D 09 N 11	197 22.8 212 25.2 227 27.7 242 30.2 257 32.6 272 35.1	318 03.5 5 333 03.4 348 03.3 3 03.2 18 03.1 33 03.0	516 48.6 49.2 49.7 50.2 50.8 51.3	325 20.7 340 21.5 355 22.4 10 23.2 25 24.0 40 24.8	\$18 13.7 14.1 14.5 14.9 15.3 15.7	58 28.4 N16 73 31.1 88 33.9 103 36.6 118 39.3 133 42.0	44.4 44.5 44.6 44.7 44.8 44.9	113 57.5 129 00.1 144 02.8 159 05.5 174 08.1	i !	02.1 02.1 02.1 02.0 02.0	Dubhe Elnath Eltanin Enif Fomalhaut	33 55.5 15 33.2	N28 36 N51 29 N 9 53 S29 36
E 12 S 13 D 14 A 15 Y 16 Y 17	287 37.6 302 40.0 317 42.5 332 44.9 347 47.4 2 49.9	48 03.0 5 63 02.9 78 02.8 93 02.7 108 02.6 123 02.5	516 51.8 52.3 52.9 53.4 53.9 54.4	55 25.7 70 26.5 85 27.3 100 28.1 115 29.0 130 29.8	\$18 16.1 16.6 17.0 17.4 17.8 18.2	148 44.8 N16 163 47.5 178 50.2 193 52.9 208 55.6 223 58.4	45.0 45.1 45.2 45.3 45.4	204 13.4 219 16.1 234 18.1 249 21.4 264 24.1 279 26.1	1 1 1 1	02.0 02.0 02.0 02.0 02.0	Gacrux Gienah Hadar Hamal Kaus Aust.	328 10.0 83 55.1	S17 3: S60 2: N23 2: S34 2:
18 19 20 21 22 23	17 52.3 32 54.8 47 57.3 62 59.7 78 02.2 93 04.7	138 02.4 3 153 02.3 168 02.3 183 02.2 198 02.1 213 02.0	\$16 55.0 55.5 56.0 56.6 57.1 57.6	145 30.6 160 31.4 175 32.3 190 33.1 205 33.9 220 34.7	\$18 18.6 19.0 19.5 19.9 20.3 20.7	239 01.1 N16 254 03.8 269 06.5 284 09.3 299 12.0 314 14.7	45.5 45.6 45.7 45.8 45.9	294 29.4 309 32.1 324 34. 339 37.1 354 40.1 9 42.1	0 7 3 0 7	02.0 02.0 02.0 02.0 02.0	Kochab Markab Menkar Menkent Miaplacidus	314 23.5 148 17.5 221 40.8	N15 1: N 4 06 S 36 2: S 569 4:
900 01 02 03 04 05	123 09.6 138 12.1 153 14.5	228 01.9 243 01.8 258 01.7 273 01.6 288 01.5 303 01.4	\$16 58.1 58.7 59.2 16 59.7 17 00.2 00.7	235 35.5 250 36.4 265 37.2 280 38.0 295 38.8 310 39.7	21.5 21.9 22.3	329 17.4 N16 344 20.1 359 22.9 14 25.6 29 28.3 44 31.0	46.0 46.1 46.1 46.2 46.3 46.4	39 48.	6 3 9	02.0 02.0 02.0 02.0 02.0 02.0	Mirfak Nunki Peacock Pollux Procyon	53 32.6	S26 17 S56 43 N28 0
06 07 T 08 H 09 U 10 R 11	198 21.9 213 24.4 228 26.8 243 29.3	318 01.3 333 01.2 348 01.1 3 01.0 18 00.9 33 00.8		325 40.5 340 41.3 355 42.1 10 42.9 25 43.8 40 44.6	24.4 24.8 25.2	89 39.2 104 42.0 119 44.7	6 46.5 46.6 46.7 46.8 46.8 46.9	130 03. 145 06. 160 09. 175 11.	9 5 2	02.0 02.0 02.0 02.0 02.0 02.0	Rasalhague Regulus Rigel Rigil Kent. Sabik	207 52.0 281 19.1 140 03.1 102 22.1	7 S 8 1: 5 S60 5: 3 S15 4:
S 12 D 13 A 14 A 15 Y 16	288 36.7 303 39.2 318 41.6 333 44.1		\$17 04.4 04.9 05.5 06.0 06.5 07.0	55 45.4 70 46.2 85 47.0 100 47.9 115 48.7 130 49.5	\$18 26.0 26.4 26.8 3 27.3 27.7	149 50.1 N1 164 52.9 179 55.6 194 58.3 210 01.0 225 03.8	47.1 47.2 47.3 47.4 47.5	220 19. 235 22. 250 25. 265 27. 280 30.	8 5 1 8 4	02.0 02.0 02.0 02.0 02.0	Sirius Spica Suhail	258 40. 158 40. 222 58.	5 S37 0 7 S16 4 0 S11 1 2 S43 2
18 19 20 21 22 23	18 51.5 33 53.9 48 56.4 63 58.9 79 01.3	152 59.9 167 59.8 182 59.6 197 59.5	\$17 07.5 08.1 08.6 09.1 09.6 10.1	145 50.3 160 51.1 175 52.0 190 52.8	3 \$18 28.5 28.9 29.3 3 29.7 3 30.1	255 09.2 270 12.0 285 14.7	47.6 47.6 47.7 47.8 47.9 48.0	310 35, 325 38, 340 41, 355 43,	4 0 7	02.0 02.0 02.0 02.0 02.0 02.0	Zuben'ubi Venus Mars	80 45. 137 14. SHA 120 55. 128 07. 221 04.	Mer.Pa 9 8 4 8 8 1
Mer Pa	h m	v -0.1	d 0.5	υ 0.8	3 d 0.4	v 2.7	d 0.3	v 2	.7 d	0.0	Jupiter Saturn	276 33.	

UT	SUN MOON					Lat.	Twilight			I	Moonrise				
	GHA	Dec	GHA	υ	Dec	d	HP	Lat.	Naut.	Civil	Sunrise	7	8	9	10
d d	h	0 /	0 /	,	0 /	,	,	N 72	08 16	h m 10 20	h m	h m 12 33	h m 12 02	h m	h m 11 12
700	1 193 30.7	26.7	140 07.	8 13.8	13 35.8	11.8	55.6	N 70 68	07 58 07 44	09 37 09 08	11 11	12 15 12 00	11 53 11 46	11 35 11 33	11 17 11 21
Ö	3 223 30.1	26.1	154 40.0 169 13.4 183 46.4	4 14.0	13 12.2	11.9	55.5	66	07 33 07 23	08 46 08 29	10 14 09 41	11 48 11 38	11 40 11 34	11 32 11 31	
0.0	5 253 29.6	25.5 25.5 S22 25.2	198 19.	4 14.1	13 00.3 12 48.4	11.9	55.5	62 60	07 14 07 07	08 15 08 02	09 16 08 57	11 29 11 22	11 30 11 26	11 30 11 29	11 30 11 32
T 0	7 283 29.0	24.9 24.6	212 52.5	7 14.3	12 24.5	12.0	55.4	N 58 56	07 00 06 54	07 52 07 42	08 42 08 28	11 15 11 09	11 22 11 19	11 28 11 27	11 34 11 36
U 0	9 313 28.5	24.2	241 59.0 256 32.3 271 05.3	3 14.4	12 12.5 12 00.4 11 48.3	12.1	55.4	54 52 50	06 48 06 43	07 34 07 26	08 16 08 06	11 04 10 59	11 16 11 13	11 27 11 26	11 37 11 39
S 1	1 343 27.9	23.6 S22 23.3		2 14.5	11 36.1	12.1	55.3	45	06 38 06 28	07 19 07 04	07 57 07 38	10 55 10 45	11 11 11 06	11 26 11 25	11 40 11 43
D 1:	3 13 27.4	23.0	314 46.3 329 20.0	14.7	S11 24.0 11 11.7 10 59.5	12.2	55.3	N 40 35 30	06 18 06 09	06 52 06 41	07 22 07 09	10 37 10 30	11 01 10 58	11 24 11 23	11 46 11 48
Y 1	5 43 26.9 5 58 26.6	22.3	343 53.8 358 27.6	14.8	10 47.2 10 34.9	12.3	55.2	20 N 10	06 01 05 46 05 31	06 31 06 13 05 57	06 57 06 37 06 19	10 24 10 14 10 05	10 54 10 48 10 43	11 22 11 21	11 50 11 53
17		21.7 S22 21.4	13 01.4	15.0 15.0	10 22.5 \$10 10.1	12,4	55.2	0 S 10	05 15 04 57	05 41	06 03	09 56	10 38	11 20 11 19	11 56 11 59
19	9 103 25.8 0 118 25.5	21.1	42 09.4 56 43.4	15.0	9 57.7 9 45.3	12.4	55.1	20	04 37 04 35 04 07	05 04 05 04 04 40	05 46 05 28 05 07	09 47 09 38 09 27	10 34	11 18 11 17	12 02 12 05
22	148 25.0	20.4	71 17.5 85 51.7	15.2	9 32.8 9 20.3	12.5	55.1 55.1	35 40	03 50 03 28	04 26	04 55	09 21 09 14	10 22 10 19 10 15	11 16 11 15 11 14	12 08 12 11 12 13
800		19.8 S22 19.4	100 26.0	15.3	9 07.8 S 8 55.2	12.6	55.0 55.0	45 S 50	03 00 02 18	03 47	04 24	09 06 08 56	10 11	11 13	12 16
02	2 208 23.9	19.1 18.8	144 09.0		8 42.7 8 30.1	12.6	55.0 55.0	52 54	01 55 01 21	03 06	03 53 03 41	08 51 08 46	10 03	11 12	12 19 12 20 12 22
03 04 05	238 23.4	18.1	158 43.5 173 18.0	15.6	8 17.4 8 04.8	12.7	55.0 54.9	56 58	1111	02 30 02 05	03 28 03 13	08 40 08 34	09 57 09 53	11 11 11 11 10	12 24 12 26
06	268 22.8		187 52.6 202 27.2	15.6		12.7	54.9 54.9	S 60	////	01 28	02 55 ight	08 26	09 49	11 09	12 28
W 07	298 22.3	17.1 16.8	217 01.8 231 36.5	15.8	7 26.7 7 14.0	12.7	54.9 54.9	Lat.	Sunset	Civil	Naut.	7	8	onset 9	10
N 10	328 21.8	16.5 16.2 15.8	246 11.3 260 46.1 275 21.0	15.9	7 01.3 6 48.5 6 35.7	12.8	54.8 54.8	N 72	h m	h m	h m	h m	h m	h m	h m
E 12 S 13	358 21.2 13 21.0			16.0	S 6 22.9 6 10.1	12.8	54.8 54.8	N 70 68	13 02	13 53 14 37	15 58 16 15	20 04	22 03 22 09	23 55 23 53	25 46 25 36
D 14	28 20.7 43 20.4	14.8	319 05.8 333 40.8	16.0	5 57.3 5 44.4	12.9	54.8 54.7	66 64	14 00 14 33	15 05 15 27 15 45	16 29 16 41 16 51	20 33 20 44 20 53	22 14 22 19 22 22	23 51 23 50 23 49	25 28 25 21 25 15
Y 16	58 20.2 73 19.9	14.1 13.8	348 15.8	16.1 16.2	5 31.6 5 18.7	12.9	54.7 54.7	62 60	14 57 15 16	15 59 16 11	16 59 17 07	21 00	22 25 22 28	23 48	25 10 25 06
18 19	103 19.4	S22 13.5 13.1	17 26.1 32 01.2	16.1 16.3	S 5 05.8 4 53.0	12.8 12.9	54.7 54.7	N 58 56	15 32 15 45	16 22 16 31	17 13 17 20	21 12 21 17	22 30 22 33	23 47 23 46	25 02 24 59
20 21	133 18.8	12.8	46 36.5 61 11.7	16.3	4 40.1 4 27.2	13.0	54.7 54.6	54 52	15 57 16 07	16 40 16 47	17 25 17 30	21 22 21 26	22 34 22 36	23 45	24 56 24 53
22 23	148 18.6 163 18.3	12.1 11.8	75 47.0 90 22.3	16.3	4 14.2 4 01.3	12.9	54.6 54.6	50 45	16 16 16 36	16 54 17 09	17 35 17 46	21 29 21 37	22 38 22 41	23 44 23 43	24 51 24 46
900 01 02	178-18.1 193-17.8 208-17.5	S22 11.4 11.1 10.7	104 57.6 119 33.0	16.4	S 3 48.4 3 35.4	12.9	54.6 54.6	N 40 35	16 51 17 05	17 22 17 33	17 55 18 04	21 44 21 49	22 44 22 46	23 43 23 42	24 41 24 37
03 04	223 17.3 238 17.0	10.4	134 08.4 148 43.8 163 19.2	16.4	3 22.5 3 09.6 2 56.6	13.0	54.6 54.5 54.5	30 20 N 10	17 16 17 36 17 54	17 42 18 00	18 12 18 27	21 54 22 02	22 48 22 52	23 41 23 40	24 34 24 28
05 06	253 16.7 268 16.5	09.7	177 54.7 192 30.2	16.5	2 43.6	12.9	54.5	0	18 10	18 16 18 33	18 43 18 59	22 10 22 17	22 55 22 58	23 39 23 38	24 23 24 18
T 07	283 16.2 298 16.0	09.0	207 05.7 221 41.3	16.6	S 2 30.7 2 17.7 2 04.8	12.9	54.5 54.5 54.5	S 10 20 30	18 27 18 45 19 06	18 50 19 09 19 33	19 17 19 38 20 05	22 23 22 31 22 39	23 01 23 04	23 37 23 36	24 13 24 08
H 09	313 15.7 328 15.4	08.3	236 16.8 250 52.4	16.6	1 51.8	13.0	54.5 54.5	35 40	19 18 19 32	19 47 20 04	20 23 20 45	22 43 22 49	23 08 23 10 23 12	23 35 23 34 23 34	24 03 23 59
R 11 S 12	343 15.2 358 14.9	07.6	265 28.0 280 03.6	16.6	1 25.9	13.0	54.4	45 S 50	19 49	20 25 20 53	21 13	22 55	23 14	23 33	23 56 23 51
D 13	13 14.7 28 14.4	06.9	294 39.3 309 14.9	16.6	0 59.9 0 47.0	12.9	54.4 54.4	52 54	20 20 20 20 31	21 06 21 22	22 17 22 49	23 02 23 05 23 09	23 17 23 19 23 20	23 32 23 31	23 46 23 44
Y 16	43 14.1 58 13.9	06.2	323 50.6 338 26.3	16.7	0 34.0 :	12.9	54.4 54.4	56 58	20 44 20 59	21 42 22 07	1111	23 13 23 17	23 22 23 24	23 31 23 30 23 30	23 41 23 39 23 35
17 18	73 13.6 88 13.4		353 01.9 7 37.6	16.7 S			54.4 54.4	S 60	21 17	22 42 SUN	1111	23 22	23 26 MO	23 29	23 32
19 20	103 13.1 118 12.9	04.7 04.4	22 13.4 36 49.1	16.7	0 17.8 3	12.9	54.4 54.4	Day	Eqn. of	Time	Mer.	Mer. F	Page I		hase
21 22	133 12.6 148 12.3	04.0 03.7	51 24.8 66 00.5	16.8	0 43.7 1 0 56.6 1	12.9	54.3 54.3	d	00 ^h	12 ^h m s	Pass.	Upper h m	Lower h m	d %	
23	163 12.1 SD 16.3	03.3 d 0.3			1 1 09.5		54.3	7 8	05 56 06 22	06 09 06 35	12 06 12 07	16 06 16 48	03 44 04 28	05 22 06 31	
	00 10.5	a 0.3	30	15.1	14.9		14.8	9	06 47	07 00	12 07	17 29	05 09	07 40	

78		2003 N	ARCH 29,	30, 31 (SA	1., 3014., 14101	
UT	ARIES	VENUS -4.0	MARS +0.5	JUPITER -2.3	SATURN +0.1	STARS
	GHA	GHA Dec	GHA Dec	GHA Dec	GHA Dec	Name SHA Dec
2900 01 02 03 04	0 / 185 59.1 201 01.6 216 04.0 231 06.5 246 08.9	227 12.9 34.9 242 12.5 34.0 257 12.1 . 33.0 272 11.6 32.0	259 22.3 \$23 07.7 274 23.0 07.6 289 23.8 07.5 304 24.6 . 07.4 319 25.3 07.2 334 26.1 07.1	55 12.3 N19 05.0 70 14.8 05.1 85 17.4 05.1 100 19.9 . 05.1 115 22.4 05.1 130 24.9 05.1	103 17.7 N22 16.1 118 20.0 16.1 133 22.3 16.1 148 24.6 . 16.1 163 26.9 16.2 178 29.2 16.2	Acamar 315 24.7 S40 17,7 Achemar 335 33.1 S57 13,4 Acrux 173 18.0 S63 07,0 Adhara 255 18.9 S28 58,8 Aldebaran 290 58.8 N16 30,9
05 06 07 S 08 A 09 T 10	261 11.4 276 13.9 291 16.3 306 18.8 321 21.3 336 23.7 351 26.2	207 11.2	349 26.9 \$23 07.0 4 27.7 06.9 19 28.4 06.8 34 29.2 . 06.6 49 30.0 06.5 64 30.7 06.4	145 27.4 N19 05.1 160 29.9 05.1 175 32.4 05.1 190 34.9 . 05.1 205 37.5 05.1 220 40.0 05.2	193 31.5 N22 16.2 208 33.8 16.2 223 36.1 16.2 238 38.4 . 16.2 253 40.7 16.3 268 43.0 16.3	Alioth 166 27.0 N55 56.5 Alkaid 153 04.6 N49 17.7 Al Na'ir 27 54.0 S46 56.8 Alnilam 275 54.6 S 1 12.1 Alphard 218 03.8 S 8 40.4 Alphecca 126 17.5 N26 42.0
U 11 R 12 D 13 A 14 Y 16	6 28.7 21 31.1 36 33.6 51 36.0 66 38.5	32 08.1 S11 24.4 47 07.7 23.4 62 07.3 22.4 77 06.8 . 21.5 92 06.4 20.5 107 06.0 19.5	79 31.5 \$23 06.3 94 32.3 06.1 109 33.0 06.0 124 33.8 05.9 139 34.6 05.8 154 35.3 05.6	235 42.5 N19 05.2 250 45.0 05.2 265 47.5 05.2 280 50.0 05.2 295 52.5 05.2 310 55.0 05.2	283 45.3 N22 16.3 298 47.6 16.3 313 49.9 16.3 328 52.2 . 16.3 343 54.5 16.3 358 56.8 16.4	Alpheratz 17.5 N26 42.0 Alpheratz 357 52.3 N29 06.3 Altair 62 16.2 N 8 52.3 Ankaa 353 23.9 S42 17.5 Antares 112 36.0 S26 26.4 Arcturus 146 02.7 N19 09.8
18 19 20 21 22 22	96 43.4 111 45.9 126 48.4 1 141 50.8 2 156 53.3	122 05.5 S11 18.6 137 05.1 17.6 152 04.7 16.6 167 04.2 . 15.7 182 03.8 14.7 197 03.4 13.7	169 36.1 \$23 05.5 184 36.9 05.4 199 37.6 05.3 214 38.4 . 05.1 229 39.2 05.0 244 40.0 04.9	325 57.5 N19 05.2 341 00.0 05.2 356 02.6 05.2 11 05.1 05.2 26 07.6 05.3 41 10.1 05.3		Atria 107 45.0 S69 01.8 Avior 234 21.2 S59 31.4 Bellatrix 278 40.8 N 6 21.1 Betelgeuse 271 10.1 N 7 24.4 Canopus 263 59.8 S52 42.1
3000	0 186 58.2 1 202 00.7 2 217 03.2 3 232 05.6 4 247 08.1	272 01.2 08.9	259 40.7 \$23 04.8 274 41.5 04.6 289 42.3 04.5 304 43.0 04.4 319 43.8 04.3 334 44.6 04.1	71 15.1 05.3 86 17.6 05.3 101 20.1 . 05.3 116 22.6 05.3 131 25.1 05.3	119 15.1 16.5 134 17.4 16.5 149 19.7 . 16.5 164 22.0 16.5 179 24.3 16.6	Capella 280 46.6 N46 00.2 Deneb 49 37.3 N45 17.1 Denebola 182 41.5 N14 33.2 Diphda 349 04.2 S17 58.3
0 0 S	6 277 13.0 7 292 15.5 8 307 17.9 9 322 20.4 0 337 22.9	302 00.3 \$11 06.9 316 59.9 06.0 331 59.5 05.0 346 59.0 . 04.0 1 58.6 03.0	349 45.3 \$23 04.0 4 46.1 03.5 19 46.9 03.7 34 47.7 . 03.6 49 48.4 03.5 64 49.2 03.6	7 176 32.6 05.2 6 191 35.1 . 05.2 6 206 37.6 05.4 1 221 40.1 05.4	3 209 28.9 16.6 3 224 31.2 16.6 3 239 33.5 . 16.6 4 254 35.8 16.6 4 269 38.0 16.6	Elnath 278 22.9 N28 36.7 Eltanin 90 49.8 N51 28.9 Enif 33 55.3 N 9 53.1 Fomalhaut 15 33.1 S29 36.5
D 1 A 1 Y 1	2 7 27.8 13 22 30.3 14 37 32.7 15 52 35.2 16 67 37.3 17 82 40.3	3 31 57.8 \$11 01.1 3 46 57.3 11 00.1 7 61 56.9 10 59.1 2 76 56.5 58.2 7 91 56.0 57.2	79 50.0 S23 03.1 94 50.7 03.1 109 51.5 03.1 124 52.3 . 02.1 139 53.1 02. 154 53.8 02.	1 251 45.1 05.4 0 266 47.6 05.8 8 281 50.1 . 05.7 7 296 52.6 05. 6 311 55.1 05.	4 299 42.6 16.7 4 314 44.9 16.7 4 329 47.2 . 16.7 4 344 49.5 16.7 4 359 51.8 16.7	Gienah 176 00.3 S17 33.6 Hadar 148 59.0 S60 23.2 Hamal 328 10.2 N23 28.5 Kaus Aust. 83 54.5 S34 23.0
	18 97 42.4 19 112 45. 20 127 47. 21 142 50. 22 157 52. 23 172 54.	0 136 54.8 54.2 5 151 54.3 53.3 0 166 53.9 52.3 4 181 53.5 51.3	169 54.6 \$23 02. 184 55.4 02. 199 56.1 02. 214 56.9 . 02. 229 57.7 01. 244 58.5 01.	3 342 00.1 05. 2 357 02.6 05. 0 12 05.1 . 05. 9 27 07.6 05. 8 42 10.1 05.	4 29 56.4 16.8 4 44 58.7 16.8 4 60 01.0 . 16.8 4 75 03.3 16.8 4 90 05.5 16.8	Markab 13 46.7 N15 13.1 B Menkar 314 23.8 N 4 06.0 Menkent 148 16.8 S36 23.1 Miaplacidus 221 41.1 S69 44.0
	00 187 57. 01 202 59. 02 218 02. 03 233 04. 04 248 07. 05 263 09.	8 226 52.2 48.3 3 241 51.8 47.4 8 256 51.4 . 46.4 2 271 50.9 45.4	320 02.3 01	5 72 15.1 05 .4 87 17.6 05 .2 102 20.1 . 05 .1 117 22.6 05 .0 132 25.1 05	.5 120 10.1 16. .5 135 12.4 16. .5 150 14.7 . 16. .5 165 17.0 16. .5 180 19.3 16.	9 Nunki 76 08.3 S26 17.6 Peacock 53 32.0 S56 43.4 Pollux 243 37.4 N28 01.2 Procyon 245 08.1 N 5 13.0
M	06 278 12 07 293 14 08 308 17 09 323 19 10 338 22	1 301 50.1 \$10 43.4 6 316 49.7 42.4 1 331 49.2 41.5 346 48.8 40.5 0 1 48.4 39.5	5 04.7 00 6 20 05.4 00 6 35 06.2 00 6 50 07.0 00	.7 162 30.1 05 .6 177 32.6 05 .4 192 35.1 05	.5 210 23.9 17. .5 225 26.1 17. .5 240 28.4 . 17. .5 255 30.7 17. .5 270 33.0 17.	0 Regulus 207 51.8 N11 57.1 Rigel 281 19.9 S 8 12.0 Rigil Kent. 140 02.5 S60 50.8 Sabik 102 21.7 S15 43.8
N D A Y	11 353 24 12 8 26 13 23 29 14 38 31 15 53 34 16 68 36 17 83 39	.9 31 47.6 S10 37.4 4 46 47.1 36.4 .9 61 46.7 35.4 3 76 46.3 34. 88 91 45.9 33. 106 45.5 32.	5 80 08.5 \$23 00 5 95 09.3 22 55 5 110 10.1 55 5 125 10.9 56 5 140 11.6 55 5 155 12.4 55	9.9 252 45.1 05 9.8 267 47.6 05 9.6 282 50.1 05 9.5 297 52.6 05 9.3 312 55.1 05	5.5 300 37.6 17 5.5 315 39.9 17 5.5 330 42.2 . 17 5.5 345 44.5 17 5.5 0 46.7 17	1. Shaula 96 32.8 537 06.3 1. Sirius 258 40.9 \$16 43.3 1. Spica 158 39.5 \$11 10.7 1. Suhail 222 58.2 \$43 26.9
	18 98 41 19 113 44 20 128 46 21 143 49 22 158 51 23 173 56	1.7 121 45.0 S10 31. 1.2 136 44.6 30. 1.6 151 44.2 29. 1.1 166 43.8 . 28. 1.6 181 43.4 27.	6 185 14.0 56 6 200 14.7 56 6 215 15.5 5 6 230 16.3 5	9.1 343 00.1 0 8.9 358 02.5 0 8.8 13 05.0 0 8.7 28 07.5 0	5.6 30 51.3 17 5.6 45 53.6 17 5.6 60 55.9 . 17 5.6 75 58.2 17	2. Zuben'ubi 137 14.1 \$16 03.4 2. SHA Mer.Pass. 2. / h m 7.2 Venus 25 04.7 9 52 7.2 Wars 72 42.5 6 41 3 Jupiter 229 14.4 20 12
Me		m , .	.0 v 0.8 d	0.1 v 2.5 d	0.0 v 2.3 d	0.0 Saturn 277 14.6 17 01

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UT	SUN	MOON	Lat.	Twil Naut.	ight Civil	Sunrise	29	Mod 30	nrise 31	1
	GHA Dec	GHA v Dec d HP		h m	h m	h m	h m	h m	h m	h m
29 00 01 02 03 04 05	193 44.7 08.8 208 44.9 09.7 223 45.0 . 10.7 238 45.2 11.7 253 45.4 12.7	216 50.3 12.5 S17 56.0 10.5 55.6 231 21.8 12.6 17 45.5 10.6 55.6 245 53.4 12.7 17 34.9 10.6 55.6 260 25.1 12.8 17 24.3 10.7 55.5 274 56.9 12.9 17 13.6 10.8 55.5 289 28.8 12.9 17 02.8 10.8 55.5	N 72 N 70 68 66 64 62 60	02 05 02 40 03 04 03 22 03 36 03 48 03 58	03 56 04 10 04 22 04 31 04 38 04 45 04 50	05 09 05 15 05 20 05 24 05 27 05 30 05 33	08 13 07 29 06 59 06 37 06 19 06 04 05 52	07 14 06 54 06 38 06 25 06 14 06 05 05 56	06 40 06 30 06 22 06 15 06 09 06 04 06 00	06 12 06 10 06 08 06 06 06 05 06 03 06 02
06 07 S 08 A 09 T 10 U 11 R 12 D 13 A 14 Y 16	283 45.8 14.6 298 46.0 15.6 313 46.2 . 16.6 328 46.4 17.5 343 46.6 18.5 358 46.7 N 3 19.5 13 46.9 20.5	304 00.7 13.0 \$16 52.0 11.0 55.5 333 04.8 13.1 16 41.0 10.9 55.5 333 04.8 13.1 16 30.1 11.1 55.4 347 36.9 13.3 16 19.0 11.1 55.4 16 16.1 16.1 16.1 16.1 16.1 16.1 16.1	N 58 56 54 52 50 45 N 40 35 30 20 N 10	04 06 04 14 04 20 04 26 04 31 04 41 04 49 04 55 05 00 05 08 05 13	04 55 04 59 05 03 05 07 05 10 05 16 05 21 05 25 05 28 05 34 05 38	05 35 05 37 05 39 05 41 05 42 05 45 05 48 05 50 05 52 05 56 05 59	05 41 05 31 05 23 05 15 05 09 04 54 04 42 04 32 04 23 04 07 03 53	05 49 05 43 05 37 05 32 05 28 05 17 05 09 05 02 04 55 04 44 04 34	05 56 05 52 05 49 05 46 05 43 05 38 05 33 05 29 05 25 05 19 05 13	06 01 06 00 05 59 05 59 05 58 05 56 05 55 05 54 05 53 05 51 05 50
17 18 19 20 21 22 23	73 47.7 24.4 88 47.9 N 3 25.3 103 48.1 26.3 118 48.2 27.3 133 48.4 28.2 148 48.6 29.2 163 48.8 30.2	103 56.9 13.8 14 48.4 11.6 55.3 118 29.7 13.9 \$14 36.8 11.7 55.2 133 02.6 14.0 14 25.1 11.7 55.2 147 35.6 14.0 14 13.4 11.7 55.2 162 08.6 14.1 14 01.7 11.9 55.2 176 41.7 14.2 13 49.8 11.8 55.2 191 14.9 14.2 13 38.0 11.9 55.2	0 S 10 20 30 35 40 45	05 17 05 18 05 19 05 18 05 16 05 14 05 11	05 41 05 43 05 44 05 45 05 45 05 45 05 45	06 01 06 04 06 06 06 09 06 11 06 12 06 14	03 40 03 27 03 13 02 57 02 48 02 37 02 24	04 25 04 16 04 06 03 54 03 48 03 40 03 31	05 07 05 02 04 56 04 50 04 46 04 42 04 37	05 48 05 47 05 45 05 44 05 43 05 42 05 40
30 00 01 02 03 04 05	193 49.2 32.1 208 49.4 33.1 223 49.6 34.1 238 49.7 35.1 253 49.9 36.0	205 48.1 14.3 513 26.1 12.0 55.1 220 21.4 14.3 13 14.1 12.0 55.1 234 54.7 14.5 13 02.1 12.1 55.1 249 28.2 14.4 12 50.0 12.1 55.1 264 01.6 14.6 12 37.9 12.1 55.1 278 35.2 14.6 12 25.8 12.2 55.0	\$ 50 52 54 56 58 \$ 60	05 07 05 05 05 03 05 00 04 57 04 53	05 45 05 44 05 44 05 43 05 42 05 42	06 17 06 18 06 19 06 20 06 22 06 23	02 09 02 02 01 54 01 44 01 34 01 22	03 21 03 16 03 10 03 04 02 57 02 49	04 31 04 28 04 25 04 21 04 18 04 13	05 39 05 38 05 37 05 37 05 36 05 35
06 07 08 S 09	268 50.1 N 3 37.0 283 50.3 38.0 298 50.5 39.0 313 50.7 39.9	293 08.8 14.7 \$12 13.6 12.3 55.0 307 42.5 14.7 12 01.3 12.3 55.0 322 16.2 14.8 11 49.0 12.3 55.0 336 50.0 14.8 11 36.7 12.4 55.0	Lat.	Sunset	Twili	ight Naut.	29	Моо 30	nset 31	1
U 10 N 11 D 12 A 13 Y 14 15 16	328 50.9 40.9 343 51.1 41.9 358 51.2 N 3 42.8 13 51.4 43.8 28 51.6 44.8 43 51.8 . 45.8 58 52.0 46.7	351 23.8 14.9 11 24.3 12.4 55.0 5 57.7 15.0 11 11.9 12.4 54.9 20 31.7 15.0 S10 59.5 12.5 54.9 35 05.7 15.0 10 47.0 12.5 54.9 49 39.7 15.1 10 34.5 12.6 54.9 64 13.8 15.2 10 21.9 12.6 54.9 78 48.0 15.2 10 09.9 12.6 54.9	N 72 N 70 68 66 64 62	h m 19 03 18 57 18 52 18 47 18 44 18 41	h m 20 17 20 02 19 50 19 41 19 33 19 26	h m 22 13 21 35 21 10 20 51 20 36 20 24	h m 11 50 12 33 13 01 13 22 13 39 13 53	h m 14 21 14 40 14 54 15 05 15 15 15 23	h m 16 23 16 31 16 37 16 42 16 46 16 49	h m 18 17 18 16 18 15 18 15 18 14 18 14
17 18 19 20 21 22 23	73 52.2 47.7 88 52.4 N 3 48.7 103 52.6 49.6 118 52.7 50.6 133 52.9 51.6 148 53.1 52.6 163 53.3 53.5	93 22.2 15.3	60 N 58 56 54 52 50 45	18 38 18 35 18 33 18 31 18 30 18 28 18 25	19 20 19 16 19 11 19 07 19 04 19 01 18 54	20 13 20 05 19 57 19 51 19 45 19 40 19 29	14 04 14 14 14 23 14 31 14 37 14 44 14 57	15 30 15 36 15 42 15 46 15 51 15 55 16 03	16 53 16 55 16 58 17 00 17 02 17 04 17 08	18 13 18 13 18 12 18 12 18 12 18 11 18 11
31 00 01 02 03 04 05	178 53.5 N 3 54.5 193 53.7 55.5 208 53.9 56.4 223 54.1 57.4 238 54.2 58.4 253 54.4 3 59.3	195 23.1 15.6 S 8 27.4 12.9 54.8 209 57.7 15.6 S 8 145.12.9 54.7 224 32.3 15.7 8 01.6 12.9 54.7 239 07.0 15.8 7 48.7 12.9 54.7 253 41.8 15.7 7 35.8 13.0 54.7 268 16.5 15.8 7 22.8 13.0 54.7	N 40 35 30 20 N 10 0	18 22 18 19 18 17 18 14 18 11 18 08	18 49 18 45 18 41 18 36 18 32 18 29	19 21 19 15 19 09 19 01 18 56 18 53	15 08 15 17 15 25 15 39 15 51 16 02	16 10 16 16 16 21 16 30 16 38 16 46	17 11 17 14 17 16 17 20 17 24 17 27	18 10 18 10 18 09 18 09 18 08 18 08
06 07 08 M 09 O 10 N 11 D 12	268 54.6 N 4 00.3 283 54.8 01.3 298 55.0 02.3 313 55.2 . 03.2 328 55.4 04.2 343 55.5 05.2	282 51.3 15.9 \$ 7 09.8 13.0 54.7 297 262.2 15.8 6 56.8 13.1 54.7 312 01.0 16.0 6 43.7 13.0 54.6 326 36.0 15.9 6 30.7 13.1 54.6 355 45.9 16.0 6 04.5 13.1 54.6	S 10 20 30 35 40 45	18 05 18 03 18 00 17 58 17 56 17 54	18 26 18 25 18 23 18 23 18 23 18 23	18 51 18 50 18 51 18 52 18 54 18 57	16 13 16 25 16 38 16 46 16 55 17 05	16 53 17 01 17 09 17 15 17 20 17 27	17 31 17 34 17 38 17 41 17 43 17 46	18 07 18 06 18 06 18 05 18 05 18 04
A 13 Y 14 Y 15 16 17	358 55.7 N 4 06.1 13 55.9 07.1 28 56.1 08.1 43 56.3 09.0 58 56.5 10.0 73 56.7 11.0	10 20.9 16.1 \$ 5 51.4 13.1 54.6 24 56.0 16.1 5 38.3 13.2 54.6 39 31.1 16.1 5 25.1 13.1 54.6 54 06.2 16.2 5 12.0 13.2 54.5 68 41.4 16.1 4 58.8 13.2 54.5 83 16.5 16.3 4 45.6 13.2 54.5	\$ 50 52 54 56 58 \$ 60	17 52 17 50 17 49 17 48 17 46 17 45	18 24 18 24 18 24 18 25 18 25 18 26	19 01 19 03 19 05 19 08 19 11 19 15	17 17 17 23 17 29 17 36 17 44 17 52	17 35 17 38 17 42 17 46 17 51 17 57	17 50 17 51 17 53 17 55 17 57 17 59	18 04 18 03 18 03 18 03 18 02 18 02
18 19 20 21	88 56.8 N 4 11.9 103 57.0 12.9 118 57.2 13.9 133 57.4 14.8	97 51.8 16.2 S 4 32.4 13.2 54.5 112 27.0 16.3 4 19.2 13.2 54.5 127 02.3 16.2 4 06.0 13.3 54.5 141 37.5 16.4 3 52.7 13.2 54.5	Day	Eqn. of	12 ^h	Mer. Pass.	Mer. I	Lower	Age Pl	nase
22 23	148 57.6 15.8 163 57.8 16.8 SD 16.0 <i>d</i> 1.0	156 12.9 16.3 3 39.5 13.3 54.5 170 48.2 16.4 \$ 3 26.2 13.2 54.5 SD 15.1 15.0 14.9	29 30 31	m s 05 02 04 44 04 26	m s 04 53 04 35 04 17	h m 12 05 12 05 12 04	h m 09 51 10 35 11 17	h m 22 14 22 57 23 38	d % 26 10 27 5 28 2	

						OTIDO
UT	ARIES	VENUS -3.9	MARS -1.4	JUPITER -1.8	SATURN +0.0	STARS
- 1	GHA	GHA Dec	GHA Dec	GHA Dec	GHA Dec	Name SHA Dec
27 00 01 02 03 04	289 44.1 304 46.5 319 49.0 334 51.5	194 56.9 N22 40.8 209 56.1 41.1 224 55.3 41.4 239 54.5 41.7 254 53.6 42.0 269 52.8 42.4	297 23.7 S13 53.3 312 25.3 53.1 327 26.8 52.9 342 28.4 52.7 357 29.9 52.5 12 31.5 52.3	134 48.5 N16 26.8 149 50.5 26.7 164 52.5 26.6 179 54.5 . 26.4 194 56.5 26.3 209 58.5 26.1	181 29.3 N22 36.5 196 31.4 36.5 211 33.5 36.5 226 35.6 . 36.5 241 37.7 36.5 256 39.8 36.5	Acamar 315 24.5 S40 17.3 Achemar 335 32.6 S57 12.9 Acrux 173 18.4 S63 07.3 Adhara 255 19.1 S28 58.5 Aldebaran 290 58.7 N16 31.0
05 06 07 08 F 09 R 10	349 53.9 4 56.4 19 58.8 35 01.3 50 03.8 65 06.2 80 08.7	284 52.0 N22 42.7 299 51.1 43.0 314 50.3 43.3 329 49.5 . 43.6 344 48.6 43.9 359 47.8 44.2	27 33.1 \$13 52.1 42 34.6 51.9 57 36.2 51.7 72 37.8 . 51.5 87 39.3 51.4 102 40.9 51.2	225 00.5 N16 26.0 240 02.5 25.8 255 04.5 25.7 270 06.5 . 25.6 285 08.5 25.4 300 10.5 25.3 315 12.5 N16 25.1	271 41.9 N22 36.5 286 44.1 36.5 301 46.2 36.5 316 48.3 . 36.5 331 50.4 36.5 346 52.5 36.5 1 54.6 N22 36.5	Alioth 166 27.3 N55 56.8 Alkaid 153 04.7 N49 18.1 Al Na'ir 27 53.1 S46 56.5 Alnilam 275 54.7 S 1 11.9 Alphard 218 04.1 S 8 40.3 Alphecca 126 17.3 N26 42.3
D 12 A 13 Y 14 Y 15 16 17	170 23.5	14 47.0 N22 44.5 29 46.1 44.8 44 45.3 45.1 59 44.5 . 45.4 74 43.6 45.7 89 42.8 46.0 104 42.0 N22 46.3	117 42.5 S13 51.0 132 44.1 50.8 147 45.6 50.6 162 47.2 . 50.4 177 48.8 50.2 192 50.3 50.0 207 51.9 S13 49.9	330 14.5 25.0 345 16.5 24.8 0 18.5 24.7 15 20.5 24.6 30 22.5 24.4 45 24.5 N16 24.3	16 56.7 36.5 31 58.8 36.5 47 00.9 . 36.5 62 03.1 36.5 77 05.2 36.5 92 07.3 N22 36.5	Alpheratz 357 51.7 N29 06.3 Altair 62 15.6 N 8 52.6 Ankaa 353 23.3 S42 17.1 Antares 112 35.6 S26 26.5 Arcturus 146 02.7 N19 10 0
18 19 20 21 22 23	200 28.4 215 30.9 230 33.3 245 35.8 3 260 38.3	104 42.0 N22 46.3 119 41.1 46.6 134 40.3 46.9 149 39.5 . 47.2 164 38.6 47.5 179 37.8 47.8	222 53.5 49.7 237 55.1 49.5 252 56.7 49.3 267 58.2 49.1 282 59.8 48.9	60 26.4 24.1 75 28.4 24.0 90 30.4 23.8 105 32.4 23.7 120 34.4 23.5		Atria 107 44.1 S69 02.2 Avior 234 22.0 S59 31.3 Bellatrix 278 40.8 N 6 21.2 Betelgeuse 271 10.2 N 7 24.5 Canopus 264 00.2 S52 41.8 Capella 280 46.6 N46 00.1
2800 02 02 04 05	2 305 45.7 3 320 48.1 4 335 50.6 5 350 53.1	209 36.1 48.4 224 35.3 48.7 239 34.5 . 48.9 254 33.6 49.2 269 32.8 49.5 284 31.9 N22 49.8	313 03.0 48.6 328 04.6 48.6 343 06.1 . 48.2 358 07.7 48.0 13 09.3 47.8	150 38.4 23.3 165 40.4 23.1 180 42.4 . 23.0 195 44.4 22.8 210 46.4 22.7 225 48.4 N16 22.5	212 24.2 36.4 227 26.3 36.4 242 28.4 36.4 257 30.5 36.4 5 272 32.6 N22 36.4	Deneb 49 36.5 N45 17.3 Denebola 182 41.7 N14 33.3 Diphda 349 03.8 S17 58.0 Dubhe 194 01.3 N61 44.3
S 00 A 00 T 1 U 1	7 20 58.0 8 36 00.4 9 51 02.9 0 66 05.4 1 81 07.8	299 31.1 50.1 314 30.3 50.4 329 29.4 . 50.4 344 28.6 50.1 359 27.8 51.1	43 12.5 47.5 4 58 14.1 47.5 5 73 15.6 . 47. 9 88 17.2 46.5 2 103 18.8 46.	5 240 50.4 22.4 3 255 52.4 22.3 1 270 54.4	2 302 36.8 36.4 1 317 39.0 . 36.4 0 332 41.1 36.4 8 347 43.2 36.4 7 2 45.3 N22 36.4	Eltanin 90 49.3 N51 29.3 Enif 33 54.6 N 9 53.3 Formalhaut 15 32.4 S29 36.2 Gacrux 172 09.9 S57 08.2
A 1 Y 1	3 111 12.8 4 126 15.2 15 141 17.7 16 156 20.2 17 171 22.6	29 26.1 51. 2 44 25.2 52. 3 59 24.4 52. 4 23.6 52. 6 89 22.7 52.	8 133 22.0 46. 0 148 23.6 46. 3 163 25.2 . 46. 6 178 26.8 45. 8 193 28.4 45.	4 331 02.4 21. 2 346 04.4 21. 0 1 06.4 . 21. 8 16 08.4 21. 7 31 10.4 20.	5 17 47.4 36.4 4 32 49.5 36.4 77 51.6 36.4 1 62 53.7 36.4 9 77 55.9 36.4 8 92 58.0 N22 36.4	Hadar 148 59.0 S60 23.6 Hamal 328 09.9 N23 28.6 Kaus Aust. 83 53.8 S34 23.0 Kochab 137 18.6 N74 08.8
2	18 186 25.1 19 201 27.6 20 216 30.0 21 231 32.5 22 246 34.9 23 261 37.4	5 119 21.0 53. 134 20.2 53. 149 19.4 53. 164 18.5 54	4 223 31.6 45 7 238 33.2 45 9 253 34.8 45 .2 268 36.4 44 .5 283 38.0 44	3 61 14.4 20. 1 76 16.4 20. 0 91 18.4 20. 8 106 20.4 20. 6 121 22.3 20	7 108 00.1 36. 5 123 02.2 36. 4 138 04.3 36. 2 153 06.4 36. 1 168 08.5 36.	3 Markab 13 46.1 N15 13.3 Menkar 314 23.5 N 4 06.2 Menkent 148 16.8 S36 23.3 Miaplacidus 221 42.4 S69 44.0
29	00 276 39.9 01 291 42.0 02 306 44.0 03 321 47.0 04 336 49.	9 194 16.8 N22 54 3 209 16.0 55 8 224 15.1 55 3 239 14.3 55 7 254 13.5 55	.0 313 41.2 44 .2 328 42.8 44 .5 343 44.4 43 .8 358 46.0 43	.3 151 26.3 19 .1 166 28.3 19 .9 181 30.3 . 19 .7 196 32.3 19	.8 198 12.8 36. .6 213 14.9 36. .5 228 17.0 . 36. .3 243 19.1 36. .2 258 21.2 36	3 Nunki 76 07.7 S26 17.6 9 Peacock 53 30.9 S56 43.4 Pollux 243 37.7 N28 01.2 Procyon 245 08.3 N 5 13.1
S	05 351 52. 06 6 54. 07 21 57. 08 36 59. 09 52 02. 10 67 04.	7 284 11.8 N22 56 1 299 10.9 56 6 314 10.1 56 1 329 09.2 5 344 08.4 5	28 49.2 \$13 43 5.5 43 50.8 43 6.8 58 52.4 43 7.0 73 54.0 44 7.3 88 55.6 44	3.2 241 38.3 18 3.0 256 40.3 18 2.9 271 42.3 18 2.7 286 44.3 18	3.9 288 25.4 36 3.8 303 27.5 36	3. Regulus 207 52.0 N11 57.2 3. Rigel 281 19.9 S 8 11.8 Rigil Kent. 140 02.4 S60 51.2 3. Sabik 102 21.2 S15 43.8
	11 82 07 12 97 09 13 112 11 14 127 14 15 142 16 16 157 19 17 172 21	.4 14 06.7 N22 5 .9 29 05.9 5 .4 44 05.0 5 .8 59 04.2 5 .3 74 03.3 5	7.8 118 58.8 \$13 4 3.0 134 00.4 4 3.3 149 02.0 4 8.5 164 03.7 4 8.8 179 05.3 4	2.2 316 48.3 N16 18 2.2 331 50.3 18 2.0 346 52.3 1 1.8 1 54.3 . 1 1.7 16 56.2 1 1.5 31 58.2 1	3.2 3 36.0 N22 36 3.0 18 38.1 36 7.9 33 40.2 36 7.7 48 42.3 . 36 7.6 63 44.4 36 7.5 78 46.6 36	3.3 Shaula 96 32.2 537 06. 3.3 Sirius 258 41.0 S16 43. 3.5 Spica 158 39.5 S11 10. 3.2 Suhail 222 58.7 S43 26. 5.2
	18 187 24 19 202 26 20 217 29 21 232 31 22 247 34	1.2 104 01.6 N22 5 1.7 119 00.8 5 1.2 133 59.9 22 5 1.6 148 59.1 23 0 1.1 163 58.3	9.3 209 08.5 \$13 4 9.5 224 10.1 4 9.7 239 11.7 4 0.0 254 13.4 4 0.2 269 15.0 4	1.1 62 02.2 1 1.0 77 04.2 1 0.8 92 06.2 1 0.6 107 08.2 1	7.2 108 50.8 30 7.0 123 52.9 30 6.9 138 55.0 30 6.7 153 57.1 3	5.2 Zuben'ubi 137 14.0 S16 03. 6.2 6.2 SHA Mer.Pas 6.2 Venus 278 56.2 11 02 6.2 Mars 22 20.7 4 07 Lipiter 219 55.7 14 56
Me		m .	0.3 v 1.6 d	0.2 v 2.0 d	0.1 v 2.1 d	0.0 Saturn 266 39.2 11 49

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UT	S	UN		N	MOON			Lat.	Naut.	Civil	Sunrise	27	28	29	30
	GHA	Dec	GHA	v	Dec	d	HP	N 72	h m	h m	l a	h m	h m	h m	h m
27 00 27 01	179 17.2	N23 20.8	212 55.2	12.5	N21 20.5	8.2	54.3	N 70							
01	194 17.0		227 26.7		21 28.7 21 36.8	8.1	54.4 54.4	68 66				22 47			
03	224 16.8	20.5	256 29.6	12.3	21 44.9	7.9	54.4	64	1111	1111	01 36	00 17	{ 90 10 }		
04 05	239 16.6 254 16.5		271 00.9 285 32.2		21 52.8 22 00.7	7.9 7.7	54.4 54.4	62 60	1111	//// 00 56	02 13 02 39	00 40 00 59	00 47 01 13	01 03 01 39	01 46 02 25
06 07	269 16.4 284 16.2	N23 20.3 20.2	300 03.4 314 34.5		N22 08.4 22 16.1	7.7 7.5	54.4 54.4	N 58 56	1111	01 44	02 59 03 16	01 15	01 34 01 51	02 05	02 53
08	299 16.1	20.1	329 05.5	12.0	22 23.6	7.5	54.4	54	00 51	02 36	03 30	01 40	02 06	02 42	03 32
F 09	314 16.0 329 15.8		343 36.5 358 07.4		22 31.1 22 38.5	7.4	54.4 54.5	52 50	01 36 02 03	02 53 03 08	03 42 03 53	01 51 02 00	02 19 02 30	02 57 03 09	03 47 04 00
11	344 15.7 359 15.6	19.8 N23 19.7	12 38.2		22 45.7 N22 52.9	7.2	54.5 54.5	45 N 40	02 48 03 19	03 38	04 15 04 33	02 20 02 36	02 53	03 36 03 56	04 27 04 48
A 13	14 15.5	19.6	41 39.7	11.6	23 00.0	6.9	54.5	35	03 42	04 19	04 48	02 49	03 28	04 14	05 06
Y 15	29 15.3 44 15.2	19.4	56 10.3 70 40.8	11.5	23 06.9 23 13.8	6.9	54.5 54.5	30 20	04 00 04 29	04 34 04 59	05 01 05 23	03 01 03 22	03 42 04 06	04 29 04 54	05 21 05 47
16 17	59 15.1 74 14.9		85 11.3 99 41.7		23 20.5 23 27.2	6.7	54.5 54.5	N 10	04 52 05 11	05 19 05 37	05 42 05 59	03 39	04 26 04 45	05 16 05 37	06 10 06 30
18	89 14.8	N23 19.1	114 12.0	11.3		6.4	54.5	S 10	05 28	05 54	06 17	04 13	05 04	05 58	06 51
20	104 14.7 119 14.5	18.9	128 42.3 143 12.5	11.1	23 40.1 23 46.4	6.3	54.6 54.6	20 30	05 44 06 00	06 11 06 30	06 35 06 56	04 31 04 52	05 25 05 49	06 20 06 45	07 13 07 39
21 22	134 14.4 149 14.3		157 42.6 172 12.6		23 52.7 23 58.8	6.1	54.6 54.6	35 40	06 09 06 18	06 41 06 52	07 09 07 23	05 04 05 18	06 03 06 20	07 01 07 18	07 55 08 12
23	164 14.2		186 42.6		24 04.8	5.8	54.6	45 S 50	06 28	07 06	07 39	05 35	06 39	07 40 08 07	08 34
2800	179 14.0 194 13.9	18.4	201 12.5 215 42.4		N24 10.6 24 16.4	5.8 5.7	54.6 54.6	52	06 40 06 45	07 22 07 29	08 00 08 10	05 56 06 06	07 04 07 16	08 20	09 14
02 03	209 13.8 224 13.6		230 12.1		24 22.1 24 27.6	5.5 5.4	54.7 54.7	54 56	06 51 06 57	07 37 07 46	08 21 08 33	06 18 06 31	07 30 07 46	08 35 08 53	09 29 09 46
04 05	239 13.5 254 13.4		259 11.5 273 41.1	10.6	24 33.0 24 38.3	5.3 5.2	54.7 54.7	58 S 60	07 04 07 11	07 56 08 08	08 48 09 05	06 46 07 04	08 05 08 28	09 14 09 42	10 08 10 35
06	269 13.2	N23 17.8	288 10.6	10.5	N24 43.5	5.1	54.7				light			nset	
s 07	284 13.1 299 13.0		302 40.1 317 09.5		24 48.6 24 53.6	5.0 4.8	54.7 54.7	Lat.	Sunset	Civil	Naut.	27	28	29	30
A 09 T 10	314 12.9		331 38.8 346 08.0		24 58.4	4.7	54.8 54.8		h m	h m	h m	h m	h m	h m	h m
U 11	344 12.6	17.3	0 37.2	10.2	25 07.7	4.5	54.8	N 72 N 70							
R 12 D 13	14 12.3		29 35.5	10.0	N25 12.2 25 16.6	4.4	54.8 54.8	68							
A 14	29 12.2 44 12.1		44 04.5 58 33.5		25 20.8 25 24.9	4.1	54.8 54.8	66	22 30			22 09 20 47	22 50		
Y 16	59 11.9 74 11.8		73 02.4 87 31.2		25 28.9 25 32.7	3.8	54.9 54.9	62 60	21 53 21 27	23 09	1111	20 10 19 44	21 39 21 04	22 48 22 08	23 22 22 49
18	89 11.7	N23 16.4	102 00.0	9.7	N25 36.5	3.6	54.9	N 58	21 07	22 21	1111	19 23	20 38	21 40	22 24
19 20	104 11.6 119 11.4	16.2	116 28.7 130 57.4	9.7	25 40.1 25 43.5	3.4 3.4	54.9 54.9	56 54	20 50 20 36	21 52 21 30	23 14	19 07 18 52	20 18 20 01	21 19 21 01	22 05 21 48
21 22	134 11.3 149 11.3		145 26.1 159 54.6		25 46.9 25 50.1	3.2	54.9 55.0	52 50	20 24 20 13	21 13 20 58	22 30 22 03	18 40 18 29	19 47 19 34	20 46 20 33	21 34 21 22
23	164 11.0	15.8	174 23.2	9.4	25 53.2	3.0	55.0	45 N 40	19 51	20 28	21 18	18 06 17 48	19 09	20 06	20 56
29 00	179 10.9 194 10.8	3 15.6	188 51.6 203 20.1	9.4	N25 56.2 25 59.0	2.8	55.0 55.0	35	19 33 19 18	20 06 19 48	20 24	17 33	18 31	19 27	20 18
02 03	209 10.7		217 48.5		26 01.7 26 04.3	2.6	55.0 55.0	30 20	19 05 18 43	19 32 19 08	20 06 19 37	17 19 16 57	18 16 17 51	19 12 18 46	20 04 19 38
04	239 10.4 254 10.3	15.2	246 45.1	9.2	26 06.7 26 09.0	2.3	55.1 55.1	N 10 0	18 24 18 07	18 47 18 29	19 14 18 56	16 38 16 19	17 30 17 10	18 23 18 02	19 17 18 56
06	269 10.2	N23 15.0	275 41.5	9.2	N26 11.2	2.0	55.1	S 10	17 50	18 12	18 39	16 01	16 50	17 42	18 36
07 08	284 10.0 299 09.9		290 09.7 304 37.8		26 13.2 26 15.1	1.9	55.1 55.1	20 30	17 31 17 10	17 55 17 36	18 23 18 06	15 42 15 20	16 28 16 04	17 19 16 53	18 14 17 48
S 09	314 09.8 329 09.6		319 05.9 333 33.9		26 16.9 26 18.5	1.6	55.1 55.2	35 40	16 58 16 44	17 26 17 14	17 58 17 48	15 07 14 52	15 49 15 32	16 38 16 20	17 33 17 16
N 11	344 09.5	14.3	348 01.9	9.0	26 20.0	1.3	55.2	45	16 27	17 01	17 38	14 34	15 12	15 59	16 55
D 12 A 13	359 09.4 14 09.3	N23 14.2 14.0	2 29.9 16 57.8		N26 21.3 26 22.5	1.2	55.2 55.2	S 50 52	16 06 15 57	16 45 16 37	17 26 17 21	14 13 14 02	14 47 14 34	15 31 15 18	16 28 16 15
Y 14	29 09.3 44 09.0	13.9	31 25.7 45 53.6	8.9	26 23.6 26 24.6	1.0	55.2 55.2	54 56	15 46 15 33	16 29 16 20	17 15 17 09	13 50 13 37	14 20 14 04	15 03 14 45	16 00 15 43
16	59 08.9	13.6	60 21.4	8.8	26 25.4	0.6	55.3	58 S 60	15 18	16 10	17 03 16 55	13 21 13 03	13 45 13 21	14 23 13 55	15 21 14 54
17 18		N23 13.4	74 49.2 89 17.0	8.7		0.4	55.3 55.3	3 00	15 01	15 59 SUN	10 33			ON	1 24 34
19 20	104 08.5 119 08.4		103 44.7 118 12.5		26 26.9 26 27.2	0.3	55.3 55.3	Day	Eqn. o	of Time	Mer.	Mer.	Pass.	Age F	Phase
21	134 08.2	2 13.0	132 40.2	8.6	26 27.3	0.1	55.4		00 ^h	12 ^h	Pass.	Upper	Lower		10
22	149 08.1 164 08.0		147 07.8 161 35.5		26 27.2 N26 27.0	0.2	55.4 55.4	27	m s 02 51	m s 02 57	h m 12 03	h m 10 08	h m 22 32	d %	
	SD 15.8		SD	14.8	14.9		15.0	28 29	03 04 03 16	03 10 03 22	12 03 12 03	10 57 11 50	23 23 24 16	28 2 29 0	
							-								

194		200	J JL	I I LIVIDLI	10, 20, 21	(1 111., 07 11., 0			
UT	ARIES	VENUS	-3.9	MARS -2.4	JUPITER -1.7	SATURN +0.1	S	TARS	1
	GHA	GHA	Dec	GHA Dec	GHA Dec	GHA Dec	Name	SHA	Dec
1900 01 02 03 04 05	357 29.3 12 31.7 27 34.2 42 36.7 57 39.1 72 41.6	173 11.2 S 188 10.8 203 10.4 218 10.1 . 233 09.7 248 09.3	0 29.6 30.9 32.2 . 33.5 34.7 36.0	22 49.4 S16 24.3 37 52.2 24.2 52 55.0 24.1 67 57.8 24.1 83 00.6 24.0 98 03.4 23.9	200 27.7 N10 31.7 215 29.7 31.5 230 31.6 31.3 245 33.6 . 31.1 260 35.6 30.9 275 37.5 30.7	254 30.6 N22 09.6 269 32.9 09.6 284 35.2 09.6 299 37.5 . 09.6 314 39.8 09.6 329 42.1 09.6	Achernar Acrux Adhara Aldebaran	173 18.9 255 18.7 290 58.1	
06 07 08 7 09 10 11	87 44.1 102 46.5 117 49.0 132 51.4 147 53.9 162 56.4	263 08.9 S 278 08.6 293 08.2 308 07.8 323 07.5 338 07.1		113 06.2 \$16 23.8 128 08.9 23.8 143 11.7 23.7 158 14.5 23.6 173 17.3 23.5 188 20.1 23.4	290 39.5 N10 30.5 305 41.5 30.3 320 43.4 30.2 335 45.4 30.0 350 47.4 29.8 5 49.3 29.6	344 44.4 N22 09.6 359 46.6 09.5 14 48.9 09.5 29 51.2 . 09.5 44 53.5 09.5 59 55.8 09.5	Al Na'ir Alnilam Alphard	218 03.9	S46 56. S 1 11. S 8 40.
12 13 14 15 16 17	177 58.8 193 01.3 208 03.8 223 06.2 238 08.7 253 11.2		0 44.9 46.2 47.5 . 48.8 50.0 51.3	203 22.9 \$16 23.4 218 25.6 23.3 28.4 23.2 248 31.2 23.1 263 34.0 23.0 278 36.8 23.0	20 51.3 N10 29.4 35 53.2 29.2 50 55.2 29.0 65 57.2 . 28.8 80 59.1 28.6 96 01.1 28.5	74 58.1 N22 09.5 90 00.4 09.5 105 02.7 09.4 120 05.0 09.4 135 07.3 09.4 150 09.6 09.4	Altair Ankaa Antares	126 17.7 357 51.2 62 15.6 353 22.7 112 35.9	N 29 06. N 8 52. S42 17. S26 26.
18 19 20 21 22 23	268 13.6 283 16.1 298 18.6 313 21.0 328 23.5 343 25.9	83 04.5 S 98 04.1 113 03.8 128 03.4 . 143 03.0 158 02.7	0 52.6 53.9 55.1 . 56.4 57.7 0 59.0	293 39.5 \$16 22.9 308 42.3 22.8 323 45.1 22.7 338 47.9 22.6 353 50.6 22.5 8 53.4 22.4	126 05.0 28.1 141 07.0 27.9 156 09.0 . 27.7 171 10.9 27.5	165 11.9 N22 09.4 180 14.2 09.4 195 16.5 09.4 210 18.8 . 09.3 225 21.0 09.3 240 23.3 09.3	Avior Bellatrix Betelgeuse	278 40.2 271 09.6	S69 02 S59 30 N 6 21 N 7 24
20 00 01 02 03 04 05	358 28.4 13 30.9 28 33.3 43 35.8 58 38.3 73 40.7	173 02.3 \$ 188 01.9 203 01.6 218 01.2 . 233 00.8 248 00.4	1 00.2 01.5 02.8 . 04.1 05.3 06.6	23 56.2 \$16 22.4 38 58.9 22.3 54 01.7 22.3 69 04.5 22.3 84 07.2 22.0 99 10.0 21.5	216 16.8 26.9 231 18.8 26.8 246 20.8 26.6 261 22.7 26.4	255 25.6 N22 09.3 270 27.9 09.3 285 30.2 09.3 300 32.5 . 09.3 315 34.8 09.3 330 37.1 09.2	Canopus Capella Deneb Denebola Diphda	182 41.8 349 03.2	N46 00 N45 17 N14 33 S17 57
06 07 S 08 A 09 T 10 U 11	88 43.2 103 45.7 118 48.1 133 50.6 148 53.0 163 55.5	263 00.1 S 277 59.7 292 59.3 307 59.0 . 322 58.6 337 58.2	09.2 10.4 . 11.7 13.0 14.3	114 12.7 \$16 21.8 129 15.5 21.1 144 18.3 21.6 159 21.0 21.8 174 23.8 21.6 189 26.5 21.6	7 306 28.6 25.8 321 30.6 25.6 336 32.6 25.4 351 34.5 25.3 4 6 36.5 25.1	15 44.0 09.2 30 46.3 09.2 45 48.6 09.2 60 50.9 09.2	Dubhe Elnath Eltanin Enif Fomalhaut	33 54.4 15 32.0	N28 36 N51 29 N 9 53 S29 36
R 12 D 13 A 14 A 15 Y 16 17	178 58.0 194 00.4 209 02.9 224 05.4 239 07.8 254 10.3	352 57.8 S 7 57.5 22 57.1 37 56.7 . 52 56.4 67 56.0	16.8 18.1 . 19.4 20.6 21.9	204 29.3 \$16 21 219 32.0 21 234 34.8 21 249 37.5 . 21 264 40.3 20 279 43.0 20	2 36 40.4 24.7 51 42.4 24.5 0 66 44.4 24.3 0 81 46.3 24.1 3 96 48.3 23.9	90 55.5 09.1 105 57.8 09.1 121 00.1 09.1 136 02.4 09.1 151 04.7 09.1	Gacrux Gienah Hadar Hamal Kaus Aust.	172 10.3 176 00.6 148 59.6 328 09.2 83 53.9	S17 33 S60 23 N23 28 S34 23
18 19 20 21 22 23	269 12.8 284 15.2 299 17.7 314 20.2 329 22.6 344 25.1	82 55.6 S 97 55.3 112 54.9 127 54.5 . 142 54.1 157 53.8	1 23.2 24.5 25.7 . 27.0 28.3 29.6	294 45.8 \$16 20. 309 48.5 20. 324 51.3 20. 339 54.0 20. 354 56.7 20. 9 59.5 20.	5 126 52.2 23.6 5 141 54.2 23.4 4 156 56.2 . 23.2 3 171 58.1 23.0 2 187 00.1 22.6	181 09.3 09.1 196 11.6 09.0 211 13.9 09.0 226 16.2 09.0 3 241 18.5 09.0	Kochab Markab Menkar Menkent Miaplacidus	148 17.1 221 42.4	N15 1: N 4 00 S36 2: S69 4:
21 00 01 02 03 04 05	14 20.0	172 53.4 \$ 187 53.0 202 52.7 217 52.3 232 51.9 247 51.5	1 30.8 32.1 33.4 34.7 35.9 37.2	25 02.2 \$16 20. 40 05.0 20. 55 07.7 19. 70 10.4 . 19. 85 13.2 19. 100 15.9 19.	0 217 04.0 22.6 9 232 06.0 22.2 8 247 08.0	271 23.1 09.0 2 286 25.4 09.0 301 27.7 08.9 9 316 30.0 08.9 7 331 32.3 08.9	Procyon	308 51.2 76 07.7 53 30.8 243 37.3 245 07.9	S26 1 S56 4 N28 0 N 5 1
06 07 08 S 09 U 10 N 11	134 49.7 149 52.2	262 51.2 S 277 50.8 292 50.4 307 50.1 . 322 49.7 337 49.3	1 38.5 39.8 41.0 . 42.3 43.6 44.9	115 18.6 S16 19. 130 21.4 19. 145 24.1 19. 160 26.8 19. 175 29.5 19. 190 32.3 18.	4 307 15.8 21.3 3 322 17.8 21.3 2 337 19.8 20.9 0 352 21.8 20.	3 1 36.9 08.9 1 16 39.2 08.9 9 31 41.5 . 08.9 7 46 43.8 08.9 6 61 46.1 08.8	Regulus Rigel Rigil Kent. Sabik	96 13.6 207 51.9 281 19.4 140 03.1 102 21.4	N11 5 S 8 1 L S60 5 S S15 4
D 12 A 13 Y 14 Y 15 16 17	179 57.1 194 59.6 210 02.0 225 04.5 240 07.0	52 47.5	47.4 47.4 48.7 . 50.0 51.2 52.5	205 35.0 S16 18. 220 37.7 18. 235 40.4 18. 250 43.1 18. 265 45.9 18. 280 48.6 18.	7 37 27.7 20.1 6 52 29.6 20.1 5 67 31.6 19.1 4 82 33.6 19.1 3 97 35.5 19.	2 91 50.7 08.8 0 106 53.0 08.8 8 121 55.3 . 08.8 6 136 57.6 08.8 4 151 59.9 08.8	Shaula Sirius Spica Suhail	258 40.6 158 39.7 222 58.5	4 S37 0 5 S16 4 7 S11 1 5 S43 2
18 19 20 21 22 23	9 285 14.4 300 16.8 315 19.3 2 330 21.8 3 345 24.2	97 46.3 112 46.0 127 45.6 142 45.2	55.1 56.3 . 57.6 1 58.9	295 51.3 S16 18. 310 54.0 18. 325 56.7 18. 340 59.4 17. 356 02.1 17. 11 04.9 17.	1 127 39.5 19. 0 142 41.4 18. 8 157 43.4 . 18. 7 172 45.4 18.	1 182 04.5 08.7 9 197 06.8 08.7 7 212 09.1 . 08.7 5 227 11.4 08.7	Zuben'ubi Venus	80 44.1 137 14.1 SHA 174 33.1 25 27.1 202 46.	Mer. Pa
Mer. Pa	h m	v -0.4	d 1.3	v 2.8 d 0	1 v 2.0 d 0.	2 v 2.3 d 0.0		256 57.	

	21	003 5	FLIFMR	ER 19	, 20,	21	(FKI.,	SAI.,	SUN	-)		195
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03	226 29.6 40.8 241 29.8 39.9	313 14.5 327 43.3	9.8 26 33.0 9.7 26 35.2	2.2 54.8	64	03 48 03 58	04 48 04 52	05 36	19 56	21 10	22 12 22 49	24 14 24 35
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T 10 U 11 R 12 D 13 A 14 Y 15 Y 16 17 18 19 20 21 21 22 23 21 00 01	331 36.5 09.8 1 08.8 16 37.1 07.9 8 13 13 7.3 06.9 46 37.6 05.9 16 13 7.8 04.9 76 38.0 04.9 13 82.2 N 1 03.0 106 38.5 02.0 121 38.7 01.1 136 38.9 1 00.1 136 39.9 1 00.1 166 39.3 58.1 181 39.6 N 0 57.2 181 39.6 N 0 56.2	41 49.7 56 17.5 70 45.3 85 13.0 99 40.8 114 08.6 128 36.3 143 04.1 157 31.8 171 59.5 186 27.2 200 54.9 215 22.6 229 50.3 244 18.0 258 45.8	8.8 26 38.7 8.7 N26 34.5 8.8 26 32.1 8.8 26 22.7 8.7 26 27.0 8.8 26 22.3 8.7 26 21.4 8.7 N26 18.3 8.7 26 15.2 8.7 26 08.4 8.7 26 08.4 8.7 26 01.0 8.8 N25 57.1 8.8 725 53.0	2.0 55.5 2.2 55.6 2.4 55.6 2.7 55.6 2.7 55.7 2.9 55.7 3.1 55.8 3.4 55.8 3.4 55.8 3.7 55.9 3.9 55.9 4.1 55.9	N 70 68 66 64 62 60 N 58 56 54 52 50 45 N 40 35	18 17 18 15 18 13 18 11 18 10 18 08 18 07 18 06 18 06 18 05 18 04 18 04	19 26 19 17 19 09 19 03 18 57 18 53 18 49 18 46 18 43 18 40 18 38 18 36	21 00 20 37 20 21 20 07 19 56 19 47 19 40 19 33 19 27 19 22 19 18 19 14	17 23 16 39 16 10 15 47 15 29 15 13 15 00	18 01 17 23 16 56 16 35 16 17 16 02 15 49	20 21 18 51 18 13 17 46 17 25 17 08 16 53 16 40 16 29	19 53 19 09 18 40 18 17 17 59 17 44 17 31 17 19 17 09 17 00
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T 10 U 11 R 12 D 13 A 14 F 15 Y 16 17 18 19 200 21 22 23 21 00 03 04 05 06	331 36.5 10.8 1 36.9 N 1 08.8 16 37.1 07.9 13 37.3 06.9 46 37.6 05.9 16 37.8 04.9 76 38.0 04.9 19 38.2 N 1 03.0 106 38.5 02.0 121 38.7 01.1 136 38.9 1 00.1 136 39.3 58.1 181 39.6 N 0 57.2 11 40.0 55.2 211 40.0 55.2 226 40.2 . 54.3	41 49.7 56 17.5 70 45.3 85 13.0 99 40.8 114 08.6 128 36.3 143 04.1 157 31.8 171 59.5 186 27.2 200 54.9 215 22.6 229 50.3 244 18.0 258 45.8 273 13.5 287 41.2	8.8 26 38.7 8.7 N26 34.5 8.8 26 32.1 8.8 26 22.1 8.8 26 22.1 8.7 26 27.0 8.8 26 24.3 8.7 26 21.4 8.7 N26 18.3 8.7 26 15.2 8.7 26 11.8 8.7 26 004.7 8.7 26 004.7 8.7 26 004.7 8.7 25 40.8 8.7 25 40.8 8.7 25 40.8 8.7 25 40.8 8.7 25 40.8 8.7 25 40.8 8.7 25 44.5	2.0 55.5 5.6 2.7 55.6 2.7 55.6 2.7 55.6 2.7 55.7 3.1 55.8 3.4 55.8 3.7 55.8 3.7 55.9 4.1 55.9 4.1 55.9 4.2 56.0 4.3 56.0 4.3 56.0 4.5 56.0	N 70 68 66 64 62 60 N 58 56 52 50 45 N 40 35 30 20	18 17 18 15 18 13 18 11 18 10 18 08 18 07 18 06 18 06 18 06 18 04 18 04 18 02 18 01 18 00 17 59	19 26 19 17 19 09 19 03 18 57 18 53 18 49 18 46 18 43 18 36 18 32 18 32 18 28 18 28 18 24 18 24	21 00 20 37 20 21 20 07 19 56 19 47 19 40 19 33 19 27 19 12 19 18 19 10 19 00 18 55 18 51 18 46	17 23 16 39 16 10 15 47 15 29 15 13 15 00 14 32 14 10 13 37 13 10	18 01 17 23 16 56 16 35 16 17 16 02 15 49 15 23 15 01 14 44 14 29 14 03	20 21 18 51 18 13 17 46 17 25 17 08 16 53 16 40 16 29 16 05 15 46 15 30 15 17 14 53	19 53 19 09 18 40 18 17 17 59 17 44 17 31 17 19 17 00 16 41 16 25 16 12 16 10 15 40
T 10 U 11 R 12 D 13 A 14 Y 16 17 18 19 20 21 22 22 23 21 00 01 02 03 04 05	331 36.5	41 49.7 56 17.5 70 45.3 85 13.0 99 10.8 114 00.6 128 36.3 143 04.1 157 31.8 171 59.5 186 27.2 200 54.9 215 22.6 229 50.3 244 18.0 258 45.8 273 13.5 287 41.2 302 08.9 316 36.6 331 04.3 345 32.0	8.8 26 38.7 8.7 N26 34.5 8.8 26 32.1 8.8 26 29.7 8.7 26 27.0 8.7 26 27.0 8.7 26 15.2 8.7 26 15.2 8.7 26 15.2 8.7 26 01.4 8.7 26 01.4 8.7 26 01.4 8.7 26 01.4 8.7 26 01.4 8.7 25 40.0 8.8 N25 57.1 8.7 25 48.8 8.7 25 44.0 8.7 25 35.4 8.7 25 34.8 8.7 25 44.0 8.7 25 35.4 8.7 25 35.4 8.7 25 35.4	2.0 55.5 2.2 55.6 2.4 55.6 2.4 55.6 2.7 55.7 3.1 55.7 3.1 55.8 3.4 55.8 3.7 55.9 3.9 55.9 4.1 55.9 4.2 56.0 4.3 56.0 4.3 56.0 4.3 56.0 4.5 56.1 4.7 56.1 4.9 56.1 4.9 56.1	N 70 68 664 62 60 N 58 56 54 52 50 45 N 40 35 30 20 N 10 0 0 0 0	18 17 18 15 18 13 18 11 18 10 18 08 18 06 18 06 18 06 18 04 18 04 18 01 18 00 18 00 17 59 17 58 17 57	19 26 19 17 19 03 18 57 18 53 18 49 18 46 18 38 18 36 18 36 18 28 18 26 18 21 18 17 18 17	21 00 20 37 20 21 20 07 19 56 19 47 19 40 19 33 19 27 19 18 19 14 19 00 18 55 18 51 18 43 18 41 18 41	17 23 16 39 16 10 15 47 15 13 15 00 14 32 13 37 13 10 12 48 12 26 11 42	18 01 17 23 16 56 16 35 16 17 16 02 15 29 15 01 14 44 14 29 14 03 13 19 12 58 12 36	20 21 18 51 17 46 17 25 17 08 16 53 16 40 16 29 16 05 15 46 15 30 15 17 14 53 14 32 14 13 13 53 13 33	19 53 19 09 18 40 18 17 59 17 44 17 31 17 19 17 00 16 41 16 25 16 00 15 40 15 22 15 06 14 43
T 10 U 11 R 12 D 13 A 14 Y 16 17 18 19 9 20 21 22 22 23 21 00 03 04 05 06 07 8 8 9 9	331 36.5	41 49.7 56 17.5 70 45.3 85 13.0 99 40.8 114 08.6 128 36.3 143 04.1 157 31.8 171 59.5 186 27.2 200 54.9 215 22.6 229 50.3 244 18.0 258 45.8 273 13.5 287 41.2 302 08.9 316 36.6 331 04.3 345 32.0 359 59.7 14 27.5	8.8 26 38.7 8.7 N26 34.5 8.8 26 32.1 8.8 26 29.7 8.7 26 27.0 8.7 26 27.0 8.7 26 11.4 8.7 N26 18.3 8.7 26 11.4 8.7 N26 18.3 8.7 26 11.8 8.7 26 01.0 8.8 N25 57.1 8.7 25 48.8 8.7 25 44.0 8.7 25 35.4 8.7 25 25.8 8.8 25 20.7 8.8 25 25.8 8.8 25 25.7	2.0 55.5 2.4 55.6 2.4 55.6 2.7 55.6 2.7 55.6 2.7 55.7 3.1 55.7 3.1 55.8 3.4 55.8 3.7 55.9 3.9 55.9 3.9 55.9 4.1 55.9 4.2 56.0 4.3 56.0 4.3 56.0 4.5 56.1 4.7 56.1 4.7 56.1 4.7 56.1 5.2 56.2 5.3 56.2	N 70 68 664 662 60 N 58 550 45 30 20 N 10 20 35	18 17 18 15 18 13 18 11 18 10 18 06 18 06 18 06 18 04 18 04 18 02 18 01 18 00 17 59 17 55 17 55 17 55 17 55 17 55	19 26 19 17 19 03 18 57 18 53 18 49 18 46 18 43 18 38 18 36 18 32 18 26 18 24 18 19 18 17 18 17 18 17 18 17 18 17 18 17 18 17 18 17 18 17	21 00 20 37 20 27 20 27 19 46 19 47 19 40 19 37 19 27 19 12 19 18 19 10 18 55 18 51 18 43 18 41 18 43 18 43 18 47	17 23 16 39 16 10 15 47 15 13 15 00 14 10 13 37 13 10 12 48 12 05 11 42 11 10 00	18 01 17 23 16 56 16 35 16 17 16 02 15 49 15 23 15 01 14 44 14 29 14 03 13 19 12 58 12 36 12 10	20 21 18 51 17 46 17 25 17 08 16 29 16 05 15 46 15 30 15 17 14 53 14 32 14 13 13 53 13 33 13 38 12 54	19 53 19 09 18 40 18 17 17 59 17 44 17 31 17 19 17 00 16 41 16 25 16 10 15 40 15 22 15 06 14 49 14 31 14 11 13 58
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T 100 111 R 122 17 16 17 17 18 19 12 17 17 18 18 19 12 17 17 18 18 19 12 17 17 18 18 19 12 17 17 18 18 19 12 17 18 18 19 19 19 19 19 19 19 19 19 19 19 19 19	331 36.5	41, 49.7 70 45.3 85 13.0 99 40.8 114 08.6 128 36.3 143 04.1 157 31.8 171 59.5 186 27.2 200 54.9 215 22.6 229 50.3 244 18.0 258 45.8 273 13.5 287 41.2 302 08.9 316 36.6 331 04.3 345 32.0 359 59.7 14 27.5 28 55.2 43 22.9 57 50.7	8.8 26 38.7 8.7 N26 34.5 8.8 26 32.1 8.7 N26 34.5 8.8 26 29.7 8.7 26 27.0 8.7 26 27.0 8.7 26 11.8 8.7 26 11.8 8.7 26 10.0 8.8 N25 57.1 8.7 26 01.0 8.8 N25 57.1 8.7 25 40.5 8.7 25 40.5 8.7 25 40.5 8.7 25 35.4 8.7 25 40.5 8.7 25 40.5 8.7 25 40.5 8.7 25 53.0 8.7 25 53.0 8.7 25 53.0 8.7 25 54.5 8.7 25 54.5 8.7 25 55.0 8.7 25 55.0 8.7 25 55.0 8.7 25 25.0 8.7 25 15.5 8.8 25 25.0 8.7 25 15.5 8.8 25 25.0 8.8 25 20.7 8.8 25 50.7	2.0 55.5 2.4 55.6 2.4 55.6 2.7 55.6 2.7 55.7 3.1 55.7 3.1 55.8 3.4 55.8 3.7 55.9 3.9 55.9 4.1 55.9 4.2 56.0 4.3 56.0 4.3 56.0 4.5 56.1 4.9 56.1 4.9 56.1 5.1 56.1 5.1 56.2 5.1 56.2 5.1 56.3 5.1 56.3	N 70 688 664 660 670 N 588 554 552 505 320 N 10 0 S 200 335 405 50 S 50	18 17 18 15 18 13 18 11 18 10 18 07 18 06 18 06 18 05 18 04 18 02 18 01 18 00 18 00 17 59 17 58 17 55 17 55 17 55 17 54 17 54	19 26 19 17 19 09 19 03 18 57 18 49 18 48 18 40 18 38 18 26 18 22 18 28 18 26 18 21 18 17 18 17 18 17 18 17 18 12 18 23 18 23 18 24 18 23 18 24 18 25 18 26 18 21 18 27 18 17 18 17 18 17 18 17 18 17 18 18 17 18 18 18 18 18 18 18 18 18 18 18 18 18 1	21 00 20 37 20 27 20 27 19 56 19 47 19 47 19 33 19 27 19 18 19 14 19 16 19 06 19 00 18 55 18 51 18 43 18 43 18 44 18 43 18 53 18 53 18 53 18 59	17 23 16 39 16 10 15 47 15 29 15 13 15 00 14 32 13 37 10 12 48 12 26 11 14 10 10 10 42 11 10 00 10 9 53	18 01 17 23 16 56 16 35 16 17 16 02 15 49 15 23 15 01 14 44 14 29 12 58 12 36 12 10 11 36 11 14 11 36 11 14	20 21 18 51 18 13 17 46 17 25 17 016 29 16 05 15 46 29 14 13 33 13 33 13 38 12 54 12 37 11 52	19 53 19 09 18 40 18 17 17 59 17 09 17 00 15 16 41 16 25 16 12 22 15 06 14 49 11 23 28 13 44 13 28 13 07
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T 100 U 11 11 11 11 11 11 11 11 11 11 11 11 1	331 36.5 10.8 346 36.7 09.8 1 36.9 N 1 08.8 16 37.1 07.9 06.9 46 37.6 0.5 06.9 06	41 49.7 56 17.5 70 45.3 85 13.0 99 40.8 114 08.6 128 36.3 143 04.1 157 31.8 171 59.5 186 27.2 200 54.9 215 22.6 229 50.3 244 18.0 258 45.8 273 13.5 287 41.2 302 08.9 316 36.6 331 04.3 345 32.0 359 59.7 72 18.5 86 46.3 101 14.0 114.0 115 41.9	8.8 26 38.7 8.7 N26 34.5 8.8 26 32.1 8.7 N26 34.5 8.8 26 29.7 8.7 26 27.0 8.7 26 27.0 8.7 26 11.8 8.7 26 11.8 8.7 26 01.0 8.8 N25 57.1 8.7 26 01.0 8.8 N25 57.1 8.7 25 40.5 8.7 25 40.5 8.7 25 30.7 8.7 25 30.7 8.7 25 30.7 8.7 25 10.2 8.8 N25 30.7 8.7 25 51.0 8.7 25 40.5 8.7 25 40.5 8.7 25 10.2 8.8 N25 30.7 8.7 25 10.2 8.8 25 20.7 8.7 25 10.2 8.8 25 20.7 8.8 25 25 01.7 8.8 25 25 01.7 8.7 25 10.2 8.8 24 53.4 8.8 24 53.4 8.9 24 43.4 8.9 24 43.4	2.0 55.5 2.4 55.6 2.4 55.6 2.7 55.7 2.7 55.7 3.1 55.8 3.4 55.8 3.7 55.9 3.9 55.9 3.9 55.9 4.1 55.9 4.2 56.0 4.3 56.0 4.5 56.1 4.5 56.1 4.5 56.1 5.1 56.1 5.1 56.2 5.1 56.2 5.1 56.2 5.1 56.3 5.1 56.4 6.1 56.4 6.1 56.4 6.1 56.4 6.1 56.4	N 708 686 642 660 8 586 554 550 45 502 300 305 445 502 554 658 658	18 17 18 13 18 11 18 10 18 08 18 06 18 06 18 06 18 06 18 00 18 00 17 59 17 55 17 55 17 55 17 54 17 54 17 53 17 53 17 53 17 53	19 26 19 17 19 09 19 03 18 57 18 46 18 48 18 38 18 38 18 32 18 28 18 28 18 24 18 11 18 17 18 17 18 17 18 17 18 12 18 23 18 24 18 21 18 23 18 26 18 21 18 23 18 23 18 23 18 23 18 24 18 21 18 21 18 23 18 23 18 23 18 23 18 24 18 21 18 23 18 24 18 21 18 23 18 23 18 23 18 24 18 23 18 24 18 23 18 24 18 23 18 24 18 23 18 24 18 24 18 25 18 25 18 26 18 27 18 27	21 00 20 37 20 21 20 07 19 56 19 47 19 48 19 19 22 19 18 19 10 6 19 00 18 55 18 51 18 43 18 44 18 43 18 49 18 53 18 53 18 53 19 10 19 10 19 10 19 10 19 10 19 10 19 10 19 11 19 14	17 23 16 39 16 10 15 47 15 29 15 13 15 10 14 32 14 10 12 26 11 10 10 20 10 42 10 10 10 42 10 10 10 10 10 10 10 10 10 10 10 10 10	18 01 17 23 16 56 16 35 16 16 17 16 02 15 49 11 14 42 11 13 14 11 13 14 11 10 47 10 33 10 18 10 19 59 70 99 37	20 21 18 13 17 46 16 25 17 08 16 53 16 40 16 25 15 17 14 53 14 32 13 33 13 08 12 54 12 37 12 17 11 52 11 40 10 51	19 53 19 05 18 40 18 17 59 17 44 17 17 19 17 00 16 41 16 25 16 10 15 40 15 40 15 20 15 06 14 49 14 31 14 11 13 18 13 28 13 3 48 13 27 12 28 12 38
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18 19 20 21 22 23 2900	92 19.7 \$ 2 03.9 107 20.0 04.9 122 20.2 05.9 137 20.4 . 06.8 152 20.6 07.8 167 20.8 08.8 182 21.0 \$ 2 09.7	58 06.0 8.4 \$14 18.3 14.4 60.4 72 33.4 8.3 14 32.7 14.4 60.4 87 00.7 8.2 14 47.1 14.2 60.4 101 27.9 8.2 15 01.3 14.2 60.4 115 55.1 8.1 15 15.5 14.1 60.4 130 22.2 8.0 15 29.6 13.9 60.4 144 49.2 8.0 \$15 43.5 13.9 60.4	\$ 10 20 30 35 40 45 \$ 50	04 56 0 04 50 0 04 45 0 04 40 0 04 33 0	05 25 05 22 05 18 05 15 05 15 05 07	05 46 05 44 05 41 05 40 05 39 05 37	07 38 07 28 07 18 07 12 07 05 06 58 06 48	08 27 08 13 07 57 07 48 07 37 07 25	09 21 09 02 08 41 08 29 08 15 07 59 07 38	10 18 09 56 09 32 09 17 09 00 08 40 08 15
02 03 04 05	197 21.2 10.7 212 21.4 11.7 227 21.6 12.7 242 21.8 13.6 257 22.0 14.6	159 16.2 7.9 15 57.4 13.7 60.4 173 43.1 7.8 16 11.1 13.7 60.4 188 09.9 7.8 16 24.8 13.6 60.3 202 36.7 7.7 16 38.4 13.4 60.3 217 03.4 7.6 16 51.8 13.3 60.3	52 54 56 58 \$ 60	04 19 0 04 14 0 04 09 0 04 02 0	05 00 04 57 04 54 04 50 04 46	05 34 05 32 05 31 05 30 05 28	06 44 06 39 06 34 06 29 06 22	07 03 06 56 06 47 06 38 06 27	07 29 07 18 07 06 06 52 06 36	08 03 07 50 07 34 07 15 06 52
06 07 08 M 09	272 22.2 S 2 15.6 287 22.5 16.6 302 22.7 17.5 317 22.9 18.5	231 30.0 7.5 \$17 05.1 13.3 60.3 245 56.5 7.5 17 18.4 13.1 60.3 260 23.0 7.4 17 31.5 13.0 60.3 274 49.4 7.3 17 44.5 12.9 60.3	Lat.	Sunset	Twili Civil	ght Naut.	28	Moo 29	nset 30	1
O 10 N 11	332 23.1 19.5 347 23.3 20.4	289 15.7 7.3 17 57.4 12.8 60.3 303 42.0 7.1 18 10.2 12.6 60.3	N 72	17 31 1	h m 8 38	h m 20 01	h m 16 41	h m	h m	h m
D 12 A 13 Y 14 Y 15 16 17	2 23.5 \$ 2 21.4 17 23.7 22.4 32 23.9 23.4 47 24.1 24.3 62 24.3 25.3 77 24.5 26.3	318 08.1 7.2 \$18 22.8 12.5 60.3 323 34.3 7.0 18 35.3 12.4 60.2 347 00.3 7.0 18 47.7 12.3 60.2 1 26.3 6.9 19 00.0 12.2 60.2 15 52.2 6.8 19 12.2 12.0 60.2 30 18.0 6.7 19 24.2 11.9 60.2	N 70 68 66 64 62 60	17 35 1 17 37 1 17 38 1 17 39 1 17 40 1	.8 34 .8 30 .8 27 .8 25 .8 23 .8 21	19 48 19 37 19 28 19 21 19 15 19 10	17 08 17 29 17 46 18 00 18 11 18 21	15 57 16 53 17 26 17 51 18 11 18 27	16 37 17 38 18 13 18 38	18 22 19 01
18 19 20 21 22 23	92 24.7 \$ 2 27.3 107 24.9 28.2 122 25.1 29.2 137 25.4 30.2 152 25.6 31.1 167 25.8 32.1	44 43.7 6.7 \$19 36.1 11.8 60.2 59 09.4 6.6 19 47.9 11.7 60.2 73 35.0 6.6 19 59.6 11.5 60.2 88 00.6 6.4 20 11.1 11.3 60.1 102 26.0 6.4 20 22.4 11.3 60.1 116 51.4 6.4 20 33.7 11.1 60.1	N 58 56 54 52 50 45	17 42 1 17 43 1 17 43 1 17 44 1	8 20 8 19 8 18 8 17 8 16 8 14	19 06 19 02 18 59 18 56 18 54 18 49	18 30 18 38 18 45 18 51 18 57 19 09	18 41 18 53 19 03 19 13 19 21 19 39	18 58 19 15 19 29 19 42 19 53 20 16	19 28 19 50 20 07 20 23 20 36 21 03
30 00 01 02 03 04 05	182 26.0 \$ 2 33.1 197 26.2 34.1 212 26.4 35.0 227 26.6 . 36.0 242 26.8 37.0 257 27.0 37.9	131 16.8 6.2 \$20 44.8 10.9 60.1	N 40 35 30 20 N 10 0	17 48 1 17 49 1 17 50 1 17 52 1	.8 13 .8 13 .8 12 .8 12 .8 13 .8 14	18 45 18 42 18 40 18 38 18 37 18 38	19 19 19 28 19 35 19 49 20 01 20 12	19 53 20 06 20 17 20 36 20 52 21 08	20 35 20 50 21 04 21 27 21 47 22 06	21 24 21 42 21 58 22 24 22 46 23 07
06 07 T 08 U 09 E 11	272 27.2 \$ 2 38.9 287 27.4 39.9 302 27.6 40.9 317 27.8 41.8 332 28.0 42.8 347 28.2 43.8	217 47.3 5.9 \$21 48.4 10.1 60.0 232 12.2 5.8 21 58.5 10.0 60.0 246 37.0 5.7 22 08.5 9.8 60.0 261 01.7 5.7 22 18.3 9.6 59.9 275 26.4 5.6 22 27.9 9.5 59.9 289 51.0 5.5 22 37.4 9.3 59.9	\$ 10 20 30 35 40 45	17 57 1 18 00 1 18 01 1 18 03 1	8 16 8 20 8 24 8 27 8 30 8 34	18 41 18 45 18 52 18 56 19 02 19 09	20 23 20 35 20 48 20 56 21 06 21 16	21 23 21 40 21 59 22 10 22 23 22 38	22 25 22 46 23 09 23 23 23 39 23 59	23 28 23 51 24 17 24 32 24 50 25 12
S 12 D 13 A 14 Y 15 16 17	2 28.4 \$ 2 44.7 17 28.6 45.7 32 28.8 46.7 47 29.0 47.7 62 29.3 48.6 77 29.5 49.6	304 15.5 5.5 \$22 46.7 9.2 59.9 318 40.0 5.4 22 55.9 9.1 59.9 333 04.4 5.4 23 05.0 8.8 59.9 347 28.8 5.3 23 13.8 8.7 59.8 1 53.1 5.3 23 22.5 8.6 59.8 16 17.4 5.2 23 31.1 8.4 59.8	\$ 50 52 54 56 58 \$ 60	18 08 1 18 10 1 18 11 1 18 12 1	8 40 8 42 8 45 8 48 8 52 8 56	19 19 19 23 19 28 19 34 19 40 19 48	21 29 21 35 21 42 21 50 21 58 22 08	22 57 23 06 23 17 23 28 23 41 23 57	24 23 24 34 24 48 25 03 25 21 25 44	00 23 00 34 00 48 01 03 01 21 01 44
18 19	92 29.7 S 2 50.6 107 29.9 51.5	30 41.6 5.1 \$23 39.5 8.2 59.8 45 05.7 5.1 23 47.7 8.0 59.8			SUN	-		00000	ON	
20	122 30.1 52.5	59 29.8 5.1 23 55.7 7.9 59.7	Day	Eqn. of T	ime 12 ^h	Mer.	Mer.		Age P	hase
21 22 23	137 30.3 53.5 152 30.5 54.5 167 30.7 55.4	73 53.9 5.0 24 03.6 7.8 59.7 88 17.9 4.9 24 11.4 7.5 59.7 102 41.8 4.9 S24 18.9 7.4 59.7	28 29	m s 1	m s 09 14 09 34	Pass. h m 11 51 11 50	h m 13 59 14 54	h m 01 32 02 26	d % 02 8 03 15	
13/3	SD 16.0 d 1.0	SD 16.5 16.4 16.3	30		9 53	11 50	15 52	03 23	04 25	

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UT ARIE	S VENUS -3.9	MARS -1.2	JUPITER -1.8	SATURN -0.1	STARS	
GHA		GHA Dec	GHA Dec	GHA Dec	Name SHA	Dec
31 00 38 53 01 53 55 02 68 58 03 84 00 04 99 02 05 114 05	5.6 179 50.4 31.8 3.0 194 49.6 32.7 0.5 209 48.9 33.5 2.9 224 48.2 34.3	59 19.1 S11 11.9 74 20.7 11.4 89 22.3 10.9 104 24.0 10.4 119 25.6 09.9 134 27.3 09.4	234 15.7 N 7 35.8 249 17.8 35.7 264 19.8 35.5 279 21.9 . 35.4 294 24.0 35.2 309 26.1 35.1	294 36.3 N22 03.4 309 38.8 03.4 324 41.2 03.4 339 43.7 . 03.4 354 46.2 03.4 9 48.7 03.4	Acrux 173 18. Adhara 255 18. Aldebaran 290 57.	6 S40 17. 6 S57 13. 8 S63 06. 4 S28 58. 8 N16 31.
06 129 07 07 144 10 08 159 12	7.9 254 46.8 S19 36.0 3.3 269 46.0 36.8 2.8 284 45.3 37.6 3.3 299 44.6 . 38.5 7.7 314 43.9 39.3	149 28.9 \$11 08.9 164 30.6 08.4 179 32.2 08.0 194 33.8 . 07.5 209 35.5 07.0 224 37.1 06.5	324 28.1 N 7 34.9 339 30.2 34.8 354 32.3 34.6 9 34.4 . 34.5 24 36.4 34.3 39 38.5 34.2	24 51.2 N22 03.4 39 53.7 03.4 54 56.2 03.4 69 58.7 . 03.4 85 01.2 03.4 100 03.7 03.4	Al Na'ir 27 52, Alnilam 275 53, Alphard 218 03.	9 S 1 11 6 S 8 40
12 219 22 13 234 25 14 249 27 15 264 30	5.1 359 41.7 41.8 7.6 14 41.0 42.6 0.1 29 40.3 . 43.4 2.5 44 39.5 44.2	239 38.8 \$11 06.0 254 40.4 05.5 269 42.0 05.0 284 43.7 . 04.5 299 45.3 04.0 314 46.9 03.5	54 40.6 N 7 34.0 69 42.7 33.9 84 44.8 33.7 99 46.8 . 33.6 114 48.9 33.4 129 51.0 33.3	115 06.2 N22 03.4 130 08.6 03.4 145 11.1 03.5 160 13.6 . 03.5 175 16.1 03.5 190 18.6 03.5	Altair 62 15. Ankaa 353 22.	8 N26 42 2 N29 06 7 N 8 52 7 S42 17 0 S26 26
19 324 39 20 339 42 21 354 44 22 9 47 23 24 49	2.4 104 36.6 47.5	14 53.5 01.6 29 55.1 01.1	144 53.1 N 7 33.1 159 55.2 33.0 174 57.2 32.8 189 59.3 . 32.7 205 01.4 32.5 220 03.5 32.4	205 21.1 N22 03.5 220 23.6 03.5 235 26.1 03.5 250 28.6 . 03.5 265 31.1 03.5 280 33.6 03.5	Atria 107 45.	0 N19 09 2 S69 02 2 S59 30 9 N 6 21 3 N 7 24
100 39 52 01 54 54 02 69 53 03 84 56 04 100 03 05 115 04	7.2 194 32.3 52.3 9.6 209 31.5 53.1 2.1 224 30.8 53.9	90 01.6 59.1 105 03.2 58.6	235 05.5 N 7 32.2 250 07.6 32.1 265 09.7 31.9 280 11.8 . 31.8 295 13.9 31.6 310 15.9 31.5	295 36.1 N22 03.5 310 38.6 03.5 325 41.1 03.5 340 43.6 . 03.5 355 46.0 03.5 10 48.5 03.5	Deneb 49 36. Denebola 182 41.	2 S52 41 4 N46 00 8 N45 17 6 N14 33 2 S17 58
06 130 07 07 145 09 8 08 160 13 4 09 175 14 5 10 190 16 1 11 205 19	9.5 269 28.6 56.4 1.9 284 27.9 57.2 4.4 299 27.1 . 58.0 5.9 314 26.4 58.8	165 09.7 56.6 180 11.4 56.2 195 13.0 55.7 210 14.6 55.2	325 18.0 N 7 31.3 340 20.1 31.2 355 22.2 31.0 10 24.3 . 30.9 25 26.3 30.7 40 28.4 30.6	25 51.0 N22 03.5 40 53.5 03.5 55 56.0 03.5 70 58.5 . 03.5 86 01.0 03.5 101 03.5 03.5	Elnath 278 22. Eltanin 90 50. Enif 33 54.	0 N61 43 0 N28 36 0 N51 29 5 N 9 53 0 S29 36
12 220 23 13 235 24 14 250 26	1.8 344 24.9 \$20 00.4 4.3 359 24.2 01.2 5.7 14 23.4 02.0 9.2 29 22.7 02.7 1.7 44 22.0 03.5	255 19.5 53.7 270 21.1 53.2 285 22.7 52.7 300 24.3 52.2	55 30.5 N 7 30.4 70 32.6 30.3 85 34.7 30.1 100 36.8 . 30.0 115 38.8 29.8 130 40.9 29.7	116 06.0 N22 03.5 131 08.5 03.5 146 11.0 03.5 161 13.5 . 03.5 176 16.0 03.5 191 18.5 03.6	Gienah 176 00. Hadar 148 59. Hamal 328 09.	
18 310 30 19 325 30 20 340 43	5.6 74 20.5 \$20 05.1 9.0 89 19.8 05.9 1.5 104 19.0 06.7 4.0 119 18.3 07.5 6.4 134 17.5 08.3	345 29.2 50.7 0 30.8 50.2 15 32.4 49.7 30 34.0 49.2	145 43.0 N 7 29.5 160 45.1 29.4 175 47.2 29.2 190 49.3 29.1 205 51.3 28.9 220 53.4 28.8	206 21.0 N22 03.6 221 23.5 03.6 236 26.0 03.6 251 28.5 . 03.6 266 31.0 03.6 281 33.5 03.6	Markab 13 45. Menkar 314 22. Menkent 148 17.	7 N 4 0
200 40 5 01 55 5 02 70 5 03 85 5 04 101 0 05 116 0	6.3 194 14.6 11.4 8.8 209 13.8 12.2 1.2 224 13.1 13.0	75 38.9 47.7 90 40.5 47.2 105 42.1 46.7 120 43.7 46.2	235 55.5 N 7 28.6 250 57.6 28.5 265 59.7 28.3 281 01.8 28.2 296 03.8 28.0 311 05.9 27.9	296 36.0 N22 03.6 311 38.5 03.6 326 41.0 03.6 341 43.5 . 03.6 356 46.0 03.6 11 48.5 03.6	Nunki 76 07 Peacock 53 31	1 S56 43 9 N28 03
06 131 0 07 146 0 08 161 1 6 09 176 1 J 10 191 1 J 11 206 1	8.6 269 10.8 15.3 1.1 284 10.1 16.1 3.5 299 09.3 . 16.9 6.0 314 08.6 17.7	165 48.5 44.7 180 50.1 44.2 195 51.7 . 43.7 210 53.3 43.2	326 08.0 N 7 27.7 341 10.1 27.6 356 12.2 27.4 11 14.3 27.3 26 16.3 27.1 41 18.4 27.0	26 51.0 N22 03.6 41 53.5 03.6 56 56.0 03.6 71 58.5 . 03.6 87 01.0 03.6 102 03.5 03.6	Regulus 207 51 Rigel 281 19 Rigil Kent. 140 03	8 N12 3 7 N11 5 1 S 8 1 2 S60 5 6 S15 4
12 221 2 4 13 236 2 7 14 251 2 15 266 2 16 281 3 17 296 3	0.9 344 07.1 \$20 19.2 3.4 359 06.4 20.6 5.9 14 05.6 20.8 8.3 29 04.9 . 21.6 0.8 44 04.1 22.3	255 58.1 41.7 270 59.7 41.2 286 01.3 40.7 301 02.9 40.2	56 20.5 N 7 26.8 71 22.6 26.7 86 24.7 26.5 101 26.8 26.4 116 28.9 26.2 131 30.9 26.1	117 06.0 N22 03.6 132 08.5 03.6 147 11.0 03.6 162 13.5 . 03.6 177 16.0 03.6 192 18.5 03.7	Shaula 96 32 Sirius 258 40 Spica 158 39	0 N56 3 6 S37 0 3 S16 4 6 S11 1 2 S43 2
18 311 3 19 326 3 20 341 4 21 356 4 22 11 4	5.7 74 02.6 \$20 23.9 8.2 89 01.8 24.6 0.6 104 01.1 25.4 3.1 119 00.3 26.2	346 07.7 38.7 1 1 09.3 38.2 2 16 10.9 37.7	146 33.0 N 7 26.0 161 35.1 25.8 176 37.2 25.7 191 39.3 25.5 206 41.4 25.4	207 21.0 N22 03.7 222 23.5 03.7 237 26.0 03.7 252 28.5 . 03.7 267 31.0 03.7	Zuben'ubi 137 14 SHA Venus 124 41	
23 26 4	8.0 148 58.8 27.3 m	46 14.1 36.7	221 43.5 25.2 v 2.1 d 0.1	282 33.5 03.7 v 2.5 d 0.0	Mars 20 06 Jupiter 195 13	.1 19 58 .3 8 18

UT	S	UN		Α.	/OON		, i	Lat.	Twi	light	Cumaina		Mo	onrise	
0.	GHA		0114	_				Lat.	Naut.	Civil	Sunrise	31	1	2	3
d h	0 /	Dec 。 /	GHA ,	v	Dec ,	d,	HP	N 72	h m	h m	h m 08 54	h m	h m	h m 18 00	h m 16 53
31 00 01 02 03	184 05.0 199 05.1 214 05.1 229 05.1	\$13 53.9 54.8 55.6 56.4	104 08.8 118 32.9 132 57.1 147 21.5	5.1 5.2 5.4 5.4	\$26 12.7 26 08.4 26 03.8 25 59.1	4.3 4.6 4.7 4.8	58.7 58.7 58.6 58.6	N 70 68 66 64	06 00 05 57 05 54 05 51	07 14 07 04 06 55 06 48	08 28 08 09 07 53 07 41	16 28	17 36 16 43 16 10	17 13 16 42 16 18 16 00	16 32 16 16 16 03 15 52
04 05	244 05.2 259 05.2	57.2 58.0	161 45.9 176 10.4	5.5 5.6	25 54.3 25 49.2	5.1 5.1	58.6 58.5	62 60	05 49 05 46	06 42 06 36	07 30 07 21	15 44 15 14	15 45 15 26	15 45 15 32	15 43 15 35
06 07	289 05.2		190 35.0 204 59.8	5.8 5.8	S25 44.1 25 38.7	5.4 5.4	58.5 58.5	N 58 56	05 44 05 42	06 31 06 26	07 13 07 06	14 51 14 33	15 10 14 56	15 21 15 11	15 28 15 22
F 09	304 05.3 319 05.3	14 00.5	219 24.6 233 49.5	5.9 6.1	25 33.3 25 27.6	5.7 5.8	58.4 58.4	54 52	05 40 05 39	06 22 06 18	07 00 06 54	14 17 14 04	14 °44 14 34	15 03 14 55	15 16 15 11
R 10	334 05.3 349 05.4	02.1 02.9	248 14.6 262 39.7	6.1	25 21.8 25 15.9	5.9 6.1	58.4 58.3	50 45	05 37 05 32	06 15 06 07	06 49 06 38	13 52 13 27	14 24 14 04	14 48 14 33	15 06 14 56
D 12 A 13	4 05.4 19 05.4 34 05.4	\$14 03.7 04.5 05.3	277 04.9 291 30.3 305 55.8	6.4 6.5 6.5	\$25 09.8 25 03.6 24 57.2	6.2 6.4 6.5	58.3 58.3 58.2	N 40 35 30	05 28 05 24 05 21	06 00 05 54 05 49	06 28 06 21	13 07 12 51	13 48 13 34	14 20 14 10	14 47 14 40
Y 15	49 05.5 64 05.5	06.1	320 21.3 334 47.0	6.7	24 57.2 24 50.7 24 44.0	6.7	58.2 58.2	20 N 10	05 21 05 12 05 04	05 49 05 39 05 29	06 13 06 01 05 50	12 37 12 12 11 51	13 22 13 01 12 43	14 01 13 44 13 30	14 34 14 23 14 13
17 18	79 05.5 94 05.5	07.8 \$14 08.6	349 12.8 3 38.7	6.9 7.0	24 37.2 S24 30.2	7.0	58.1 58.1	0 S 10	04 54	05 19 05 08	05 40 05 30	11 31	12 27	13 17	14 04
19 20	109 05.6 124 05.6	09.4 10.2	18 04.7 32 30.9	7.2 7.2	24 23.1 24 15.9	7.2	58.1 58.0	20 30	04 29	04 56 04 41	05 19 05 06	10 50 10 25	11 51 11 30	12 50 12 33	13 44 13 33
21 22 23	139 05.6 154 05.6 169 05.7	11.0 11.8 12.6	46 57.1 61 23.5 75 49.9	7.4	24 08.6 24 01.1	7.5 7.6	58.0 58.0	35 40	03 59 03 45	04 31 04 21	04 58 04 50	10 11 09 54	11 18 11 04	12 23 12 13	13 26 13 19
100		S14 13.4 14.2	90 16.5 104 43.2		23 53.5 S23 45.7	7.9	57.9 57.9	\$ 50	03 28 03 05	04 08 03 51	04 40 04 27	09 34 09 08	10 47 10 26	12 00 11 44	13 10 12 59
02	214 05.7 229 05.7	15.0	119 10.0 133 36.9	7.8 7.9 8.1	23 37.8 23 29.8 23 21.7		57.8 57.8 57.8	52 54 56	02 54 02 41 02 26	03 43 03 35 03 25	04 22 04 15 04 08	08 56 08 41 08 25	10 16 10 04 09 51	11 36 11 28 11 18	12 54 12 49 12 42
04 05	244 05.8 259 05.8	16.7 17.5	148 04.0 162 31.1	8.1 8.3	23 13.4 23 05.0	8.4	57.7 57.7	58 S 60	02 07 01 42	03 13 03 00	04 00 03 51	08 05 07 40	09 36 09 18	11 18 11 08 10 55	12 36 12 28
06	274 05.8 289 05.8	S14 18.3 19.1	176 58.4 191 25.8	8.4 8.5	S22 56.5 22 47.9	8.6 8.7	57.7 57.6	Lat.	Sunset		ight			onset	
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T 10 U 11	334 05.9 349 05.9 4 05.9	21.5 22.3	249 16.5	8.9 8.9	22 21.4 22 12.3	9.2	57.5 57.5	N 72	h m 14 32	h m 15 58	h m 17 21	h m	h m	h m 21 19	h m 24 02
R 12 D 13	19 05.9 34 06.0	\$14 23.1 23.9 24.7	263 44.4 278 12.5 292 40.7	9.1 9.2 9.3	\$22 03.1 21 53.8 21 44.4	9.4	57.5 57.4 57.4	N 70 68 66	14 58 15 17 15 33	16 11 16 22 16 31	17 25 17 29 17 32		19 58 20 50	22 05 22 35 22 57	24 20 24 34
A 15 Y 16	49 06.0 64 06.0	25.5	307 09.0	9.4 9.5	21 34.9	9.6	57.4 57.4	64 62	15 45 15 56	16 38 16 45	17 35 17 37	19 11 19 55	20 50 21 22 21 46	22 57 23 14 23 28	24 46 24 55 25 03
17 18	79 06.0 94 06.0	27.1 \$14 27.9	336 05.9 350 34.5	9.6 9.8	21 15.5 \$21 05.7		57.3 57.3	60 N 58	16 05 16 13	16 50 16 55	17 40 17 42	20 24	22 04 22 20	23 40 23 50	25 10 25 16
19 20	109 06.0 124 06.1	28.7 29.5	5 03.3 19 32.1 1	9.8	20 45.8	10.0 10.2	57.3 57.2	56 54	16 20 16 27	17 00 17 04	17 44 17 46	21 04 21 20	22 33 22 44	23 59 24 07	25 21 00 07
21 22 23	139 06.1 154 06.1 169 06.1	31.1 31.9	34 01.1 1 48 30.2 1 62 59.4 1	0.2	20 35.6 20 25.4 20 15.1	10.3	57.2 57.2 57.1	52 50 45	16 32 16 38 16 49	17 08 17 12	17 48 17 50	21 33 21 44	22 54 23 03	24 14 24 20	00 14 00 20
200	184 06.1 199 06.1	S14 32.7 33.5	77 28.7 1 91 58.1 1	0.4	S20 04.7 19 54.2	10.5	57.1	N 40 35	16 58	17 19 17 26	17 54 17 58	22 08	23 22 23 37	24 34 24 45	00 34 00 45
02	214 06.1 229 06.2	34.3	106 27.6 1 120 57.2 1	0.6	19 43.6 19 32.9	10.7	57.1 57.0 57.0	30 20	17 06 17 13 17 26	17 32 17 38 17 48	18 02 18 06 18 15	22 43 22 57 23 20	23 50 24 01 24 20	24 54 00 01 00 20	00 54 01 02 01 16
04 05	244 06.2 259 06.2	35.9 36.7	135 27.0 1 149 56.8 1	8.0	19 22.2 19 11.3	10.9	57.0 56.9	N 10 0	17 37 17 47	17 58 18 08	18 23 18 33	23 40 23 58	24 36 24 51	00 36 00 51	01 28 01 40
06 07	274 06.2 289 06.2	38.2	164 26.8 1 178 56.8 1	1.2	S19 00.4 18 49.4	11.1	56.9 56.9	S 10 20	17 58 18 09	18 19 18 32	18 45 18 59	24 17 24 36	00 17 00 36	01 06 01 22	01 51 02 03
S 09 U 10	304 06.2 319 06.2 334 06.2	39.0 39.8 40.6	193 27.0 1 207 57.2 1	1.4	18 38.3 18 27.1	11.3	56.8 56.8	30 35 40	18 22 18 30	18 47 18 56	19 17 19 29	00 09 00 24	00 59 01 12	01 41 01 51	02 17 02 24
N 11 D 12	349 06.3	41.4 S14 42.2	222 27.6 1 236 58.1 1	1.5	18 15.8	11.4	56.8 56.8	45	18 38 18 48	19 07 19 21	19 43 20 00	00 42 01 02	01 27 01 45	02 04 02 18	02 33 02 43
A 13	19 06.3 34 06.3	43.0 43.8	251 28.6 1 265 59.3 1 280 30.1 1	1.8	\$17 53.1 17 41.6 17 30.0	11.6	56.7 56.7 56.7	S 50 52 54	19 01 19 07 19 13	19 37 19 45 19 54	20 23 20 35 20 48	01 29 01 41 01 56	02 07 02 18 02 30	02 35 02 43 02 52	02 56 03 02 03 08
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254		2003 DE	CEMBER 18	3, 19, 20 (TI	HURS., FRI.,	SAT.)			20	03 DECEMBE	R 18,	19, 2	20 (TH
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	GHA	GHA Dec	GHA Dec	GHA Dec	GHA Dec	Name	SHA Dec	d h	GHA Dec	GHA v Dec	d HP	N 72	h m 08 24
18 00 01 02 03 04 05	86 11.8 101 14.2 116 16.7 131 19.2 146 21.6 161 24.1	147 53.2 S22 41.9 162 52.4 41.4 177 51.6 40.8 192 50.7 40.3 207 49.9 39.7 222 49.1 39.2	85 18.4 N 0 03.0 100 19.6 03.7 115 20.7 04.3 130 21.9 . 05.0 145 23.0 05.6 160 24.2 06.3	276 22.3 N 5 37.4 291 24.6 37.4 306 27.0 37.3 321 29.3 . 37.3 336 31.6 37.2 351 34.0 37.2	344 25.0 N22 18.2 359 27.7 18.2 14 30.4 18.3 29 33.1 18.3 44 35.7 18.3 59 38.4 18.3	Acrux Adhara Aldebaran	315 23.6 S40 17.5 335 31.8 S57 13.3 173 18.2 S63 06.9 255 18.1 S28 58.5 290 57.7 N16 31.1	1800 01 02 03 04 05	180 57.5 \$23 22.1 195 57.2 22.2 210 56.9 22.2 225 56.6 22.3 240 56.3 22.4 255 56.0 22.5	254 18.2 12.5 S 1 35.5 268 49.7 12.5 1 51.3 283 21.2 12.4 2 07.3 297 52.6 12.3 2 22.5 312 23.9 12.3 2 38.3 326 55.2 12.3 2 54.5	3 15.8 58.8 1 15.8 58.8 9 15.8 58.8 7 15.8 58.9 5 15.8 58.9	N 70 68 66 64 62 60	08 04 07 48 07 35 07 24 07 14 07 06
06 07 T 08 H 09 U 10 R 11	221 33.9 236 36.4 251 38.9	282 45.8 36.9 297 45.0 36.4 312 44.1 35.8	175 25.4 N 0 06.9 190 26.5 07.5 205 27.7 08.2 220 28.8 . 08.8 235 30.0 09.5 250 31.2 10.1 265 32 3 N 0 10.8	6 36.3 N 5 37.2 21 38.6 37.1 36 41.0 37.1 51 43.3 37.0 66 45.7 37.0 81 48.0 37.0 96 50.3 N 5 36.9	74 41.1 N22 18.3 89 43.8 18.3 104 46.4 18.4 119 49.1 . 18.4 134 51.8 18.4 149 54.5 18.4 164 57.1 N22 18.4	Alioth Alkaid Al Na'ir Alnilam Alphard	166 27.2 N55 56.1 153 04.9 N49 17.4 27 53.2 S46 56.8 275 53.6 S 1 11.9 218 03.3 S 8 40.4	U 10 R 11	270 55.7 S23 22.6 285 55.4 22.6 300 55.1 22.7 315 54.8 . 22.8 330 54.4 22.9 345 54.1 23.0 0 53.8 S23 23.0	10 28.8 12.1 3 42.0 24 59.9 12.0 3 57.8 39 30.9 11.9 4 13.6	1 15.9 59.0 0 15.8 59.0 3 15.8 59.0 5 15.9 59.1 5 15.8 59.1	N 58 56 54 52 50 45 N 40	06 58 06 52 06 45 06 40 06 34 06 23 06 12
S 12 D 13 A 14 Y 16	281 43.8 296 46.3 311 48.7 326 51.2 341 53.7	327 43.3 S22 35.2 342 42.5 34.7 357 41.7 34.1 12 40.8 33.5 27 40.0 33.0 42 39.2 32.4	265 32.3 N 0 10.8 280 33.5 11.4 295 34.6 12.1 310 35.8 . 12.7 325 36.9 13.4 340 38.1 14.0 355 39.2 N 0 14.7	96 50.3 N 5 36.9 111 52.7 36.9 126 55.0 36.8 141 57.4 . 36.8 156 59.7 36.8 172 02.0 36.7 187 04.4 N 5 36.7	179 59.8 18.5 195 02.5 18.5 210 05.2 18.5 225 07.8 18.5 240 10.5 18.5 255 13.2 N22 18.6	Alpheratz Altair Ankaa Antares	357 51.3 N29 06.8 62 15.8 N 8 52.7 353 22.8 S42 17.4 112 35.9 S26 26.4	S 12 D 13 A 14 Y 16 17 18	15 53.5 23.1 30 53.2 23.2 45 52.9 . 23.2 60 52.6 23.3 75 52.3 23.4	83 03.6 11.8 5 01.3 97 34.4 11.7 5 16.9 112 05.1 11.6 5 32.7 126 35.7 11.6 5 48.5	1 15.8 59.2 9 15.8 59.2 7 15.8 59.3 5 15.8 59.3 8 15.8 59.3	35 30 20 N 10 0 S 10	06 03 05 54 05 38 05 21 05 04 04 45
18 20 21 22 23	11 58.6 27 01.1 42 03.5 57 06.0 72 08.4	102 35.9 30.1 117 35.1 29.5 132 34.3 29.0	355 39.2 N 0 14.7 10 40.4 15.3 25 41.6 15.9 40 42.7 . 16.6 55 43.9 17.2 70 45.0 17.9 85 46.2 N 0 18.5	202 06.7 36.6 217 09.1 36.6 232 11.4 . 36.6 247 13.8 36.5 262 16.1 36.5	270 15.9 18.6 285 18.5 18.6 300 21.2 . 18.6 315 23.9 18.6 330 26.6 18.7 345 29.2 N22 18.7	Atria Avior Bellatrix Betelgeuse Canopus	107 45.1 S69 02.0 234 20.7 S59 31.0 278 39.7 N 6 21.3 271 09.1 N 7 24.5 263 58.9 S52 41.7	19 20 21 22 23	105 51.7 23.5 120 51.4 23.6 135 51.1 . 23.7 150 50.8 23.7	170 07.2 11.4 6 35.8 184 37.6 11.3 6 51.6 199 07.9 11.2 7 07.3	3 15.8 59.4 5 15.7 59.4 3 15.7 59.5 6 15.7 59.5 7 15.7 59.5	20 30 35 40 45 \$ 50	04 23 03 54 03 35 03 12 02 41 01 56
1900 02 04 05	102 13.4 117 15.8 132 18.3 147 20.8 162 23.2	162 32.6 27.8 177 31.8 27.2 192 31.0 26.6 207 30.2 26.1 222 29.4 25.5	100 47.3 19.2 115 48.5 19.8 130 49.6 20.5 145 50.8 21.1 160 51.9 21.8	292 20.8 36.4 307 23.1 36.4 322 25.5 . 36.3 337 27.8 36.3 352 30.2 36.2	0 31.9 18.7 15 34.6 18.7 30 37.3 . 18.7 45 39.9 18.8 60 42.6 18.8 75 45.3 N22 18.8	Capeila Deneb Denebola Diphda	280 45.1 N46 00.2 49 37.0 N45 17.7 182 41.2 N14 33.0 349 03.3 S17 58.1 194 00.4 N61 43.6	01 02 03 04 05	195 49.8 23.9 210 49.5 24.0 225 49.2 24.1 240 48.9 24.1	257 08.2 10.9 8 10.0 271 38.1 10.8 8 25.6 286 07.9 10.8 8 41.2 300 37.7 10.6 8 56.8	0 15.6 59.6 5 15.6 59.6 2 15.6 59.7 3 15.5 59.7 3 15.5 59.7	52 54 56 58 \$ 60	01 28 00 41 //// ////
00	192 28.2 207 30.6	252 27.7 24.3 267 26.9 23.7	175 53.1 N 0 22.4 190 54.3 23.1 205 55.4 23.7 220 56.6 24.4	7 32.5 N 5 36.2 22 34.8 36.2 37 37.2 36.1 52 39.5 36.1	90 48.0 18.8 105 50.6 18.8 120 53.3 18.9	Elnath Eltanin Enif	278 21.7 N28 36.7 90 50.2 N51 29.2 33 54.7 N 9 53.5	07 08	285 48.0 24.3 300 47.7 24.4		3 15.4 59.8 7 15.4 59.8	Lat.	Sunset
F 00 R 10 I 11 D 11 A 11 Y 1	237 35.6 252 38.0 267 40.5 3 282 42.9 4 297 45.4	297 25.3 22.5 312 24.5 22.0 327 23.7 S22 21.4 342 22.9 20.8 357 22.1 20.2 12 21.3 19.6	235 57.7 25.0 250 58.9 25.6 266 00.0 N 0 26.3 281 01.2 26.9 296 02.3 27.6 311 03.5 28.2	67 41.9 36.1 82 44.2 36.0 97 46.6 N 5 36.0 112 48.9 35.9 127 51.3 35.9 142 53.6 35.9	135 56.0 18.9 150 58.7 18.9 166 01.3 N22 18.9 181 04.0 18.9 196 06.7 18.9 211 09.4 . 19.0 226 12.1 19.0	Fomalhaut	15 32.2 S29 36.3 172 09.7 S57 07.8 176 00.1 S17 33.6 148 59.2 S60 23.2 328 09.1 N23 29.0 83 54.1 S34 23.	R 10 11 D 12 A 13 Y 14 15 16	330 47.0 24.5 345 46.7 24.5 0 46.4 \$23 24.6 15 46.1 24.6 30 45.8 24.7 45 45.5 24.7 60 45.2 24.8	27 34.2 10.2 10 29.5 42 03.4 10.0 10 44.8 56 32.4 9.9 \$11 00.1 71 01.3 9.8 11 15.3 85 30.1 9.8 11 30.5 99 58.9 9.6 11 45.6 114 27.5 9.5 12 00.7	5 15.3 59.9 3 15.3 59.9 1 15.2 59.9 3 15.2 60.0 5 15.1 60.0 5 15.1 60.0 7 15.0 60.1	N 72 N 70 68 66 64 62	13 21 14 03 14 32
	7 342 52.8 8 357 55.3 9 12 57.7 0 28 00.2 1 43 02.7 2 58 05.1	42 19.6 18.4 57 18.8 \$22 17.8 72 18.0 17.2 87 17.2 16.6 102 16.4 16.0 117 15.6 15.4	341 05.8 29.5 356 06.9 N 0 30.2 11 08.1 30.8 26 09.2 31.5 41 10.4 32.1 56 11.5 32.8	172 58.3 35.8 188 00.7 N 5 35.8 203 03.0 35.7 218 05.4 35.7 233 07.7 . 35.6 248 10.1 35.6	241 14.7 19.0 256 17.4 N22 19.0 271 20.1 19.0 286 22.8 19.1 301 25.4 19.1 316 28.1 19.1 331 30.8 19.1	Markab Menkar Menkent Miaplacidus	137 20.2 N74 08.1 13 45.9 N15 13 (314 22.6 N 4 06.1 148 16.8 S36 23.3 221 41.0 S69 43.0	19 20 21 22 23	135 43.6 25.0 150 43.3 25.1 165 43.0 25.1	172 21.0 9.2 13 00.5 186 49.2 9.0 13 15.3 201 17.2 8.9 13 30.0 215 45.1 8.8 13 44.7	7 14.9 60.1 5 14.9 60.1 5 14.8 60.2 3 14.7 60.2 7 14.6 60.3	60 N 58 56 54 52 50 45	14 53 15 11 15 26 15 38 15 49 15 59 16 20
200	0 88 10.0	147 14.0 S22 14.2 162 13.2 13.6 177 12.4 13.0 192 11.6 . 12.3 207 10.8 11.7	86 13.8 N 0 34.1 101 15.0 34.7 116 16.1 35.3 131 17.3 36.0 146 18.4 36.6 161 19.6 37.3	293 17.1 35.5 308 19.5 35.5 323 21.8 35.4 338 24.2 35.4 353 26.5 35.4	61 46.9 19.2	Nunki Peacock Pollux Procyon	308 50.8 N49 52 76 07.9 \$26 17, 53 31.3 \$56 43, 243 36.5 N28 01, 245 07.3 N 5 13,	01 02 03 04 05	210 42.1 25.3 225 41.8 25.3 240 41.5 25.4 255 41.2 25.4	244 40.6 8.6 14 13.8 259 08.2 8.5 14 28.3 273 35.7 8.4 14 42.7 288 03.1 8.2 14 57.0	3 14.5 60.3 3 14.4 60.3 7 14.3 60.4 9 14.3 60.4 3 14.2 60.4	N 40 35 30 20 N 10 0 S 10	16 37 16 51 17 03 17 25 17 43 18 01 18 18
S C A C T I	6 178 24.8 7 193 27.3 8 208 29.8 9 223 32.2 0 238 34.7 1 253 37.2	3 252 08.4 09.5 3 267 07.6 09.3 2 282 06.8 08.7 7 297 06.0 08.1	191 21.9 38.6 206 23.0 39.2 221 24.1 39.9 236 25.3 40.5	5 23 31.2 35.3 2 38 33.6 35.3 9 53 35.9 35.2 5 68 38.3 35.2 2 83 40.6 35.2	91 52.2 19.3 106 54.9 19.3 121 57.6 . 19.3 137 00.2 19.3 152 02.9 19.4	Regulus Rigel Rigil Kent. Sabik	96 13.8 N12 33. 207 51.3 N11 56. 281 18.9 \$ 8 11. 140 02.8 \$60 50. 102 21.5 \$15 43.	9 S 07 8 A 09 8 T 10 U 11	285 40.5 25.5 300 40.2 25.5 315 39.9 25.5 330 39.6 25.6 345 39.3 25.6	331 24.5 7.9 15 39.5 345 51.4 7.8 15 53.6 0 18.2 7.7 16 07.5 14 44.9 7.6 16 21.3	5 14.1 60.5 5 13.9 60.5 5 13.8 60.5 8 13.8 60.5 1 13.6 60.6	20 30 35 40 45 S 50	18 37 18 59 19 12 19 27 19 45 20 08
D A	2 268 39.6 3 283 42.3 4 298 44.5 5 313 47.6 6 328 49.5 7 343 51.6	1 342 03.6 06.3 5 357 02.8 05.6 0 12 02.0 05.6 5 27 01.2 04.3	2 281 28.7 42.5 5 296 29.9 43.1 0 311 31.0 . 43.8 3 326 32.2 44.4	5 113 45.3 35.1 1 128 47.7 35.0 3 143 50.0 35.0 4 158 52.4 35.0 1 173 54.7 34.9	182 08.3 19.4 19.7 11.0 19.4 19.5 19.5 19.5 19.5 19.5 19.5 19.5 19.5	Shaula Sirius Spica Suhail	349 49.2 N56 33. 96 32.5 \$37 06. 258 40.0 \$16 43. 158 39.3 \$11 10. 222 57.8 \$43 26.	4 D 13 2 A 14 8 Y 16 17	15 38.7 25.7 30 38.4 25.7 45 38.1 . 25.8 60 37.7 25.8 75 37.4 25.8	58 04.3 7.2 17 02.3 72 30.5 7.1 17 15.7 86 56.6 7.0 17 29.1 101 22.6 6.9 17 42.4	3 13.4 60.6 7 13.4 60.6 1 13.3 60.7 1 13.2 60.7 5 13.0 60.7	52 54 56 58 \$ 60	20 19 20 31 20 45 21 02 21 23
	.8 358 54. 9 13 56. 20 28 59.	9 71 58.8 02.5 3 86 58.0 01.5	5 11 35.6 46.4 3 26 36.7 47.0	4 203 59.5 34.9 0 219 01.8 34.8	272 24.4 19. 3 287 27.0 19.	Zuben'ubi	80 44.5 N38 47 137 14.0 S16 03 SHA Mer.Pas	19 s. 20 21	105 36.8 25.9 120 36.5 25.9 135 36.2 25.9	144 39.9 6.5 18 21.6 159 05.4 6.4 18 34.4 173 30.8 6.3 18 47.2	12.8 60.8 12.8 60.8 2 12.6 60.8	Day	Eqn. of
	21 44 01. 22 59 04. 23 74 06. h m	3 116 56.4 22 00. 7 131 55.6 S21 59.	5 56 39.0 48.1 9 71 40.2 49.1	3 249 06.5 34.8 0 264 08.9 34.7	3 317 32.4 19. 7 332 35.1 19.	6 Venus 6 Mars Jupiter	60 22.5 14 11 358 35.3 18 16 190 07.5 5 30 258 18.3 0 58	22 23		187 56.1 6.1 18 59.8 202 21.2 6.1 S19 12.3 SD 16.1 16.3		18 19 20	m s 03 51 03 21 02 51
Mer.	Pass. 18 08.	v - 0.8 d 0.	6 v 1.2 d 0.	0 2.3 4 0.1	1								

UT	SI	JN		MC	OON			Lat.	Twil	light	Sunrise			nrise	
0.	GHA	Dec	GHA	1)	Dec	d	HP	Lat.	Naut.	Civil	h m	18	19	20	21 h m
d h	0 /	0 /	o /	,	0 /	,	,	N 72	08 24	10,55		01 32	03 55	06 57	" m
1800 01 02 03 04 05	180 57.5 195 57.2 210 56.9 225 56.6 240 56.3 255 56.0	\$23 22.1 22.2 22.2 22.3 22.4 22.5	254 18.2 1 268 49.7 1 283 21.2 1 297 52.6 1 312 23.9 1 326 55.2 1	12.5 12.4 12.3 12.3	1 35.5 1 51.3 2 07.1 2 22.9 2 38.7 2 54.5	15.8 15.8 15.8 15.8	58.7 58.8 58.8 58.8 58.9 58.9	N 70 68 66 64 62 60	08 04 07 48 07 35 07 24 07 14 07 06	09 52 09 17 08 52 08 32 08 16 08 03	10 33 09 50 09 22 09 00	01 29 01 27 01 25 01 23 01 21 01 20	03 40 03 29 03 19 03 11 03 04 02 58	06 14 05 46 05 25 05 08 04 54 04 43	08 55 07 53 07 18 06 54 06 34
06 T 07 T 08 H 09 U 10 R 11	270 55.7 285 55.4 300 55.1 315 54.8 330 54.4 345 54.1	\$23 22.6 22.6 22.7 22.8 22.9 23.0	341 26.5 1 355 57.6 1 10 28.8 1 24 59.9 1 39 30.9 1 54 01.8 1	12.2 12.1 12.0 11.9	3 10.3 3 26.1 3 42.0 3 57.8 4 13.6 4 29.5	15.9 15.8 15.8 15.9	58.9 59.0 59.0 59.0 59.1 59.1	N 58 56 54 52 50 45	06 58 06 52 06 45 06 40 06 34 06 23	07 51 07 41 07 32 07 23 07 16 07 00	08 43 08 28 08 15 08 04 07 54 07 34	01 19 01 18 01 17 01 16 01 15 01 14	02 53 02 48 02 44 02 41 02 37 02 30	04 33 04 24 04 16 04 10 04 03 03 50	06 18 06 05 05 53 05 42 05 33 05 14
S 12 D 13 A 14 Y 16 17	15 53.5 30 53.2 45 52.9 60 52.6 75 52.3	\$23 23.0 23.1 23.2 23.2 23.3 23.4	68 32.7 1 83 03.6 1 97 34.4 1 112 05.1 1 126 35.7 1 141 06.3 1	11.8 11.7 11.6 11.6	4 45.3 5 01.1 5 16.9 5 32.7 5 48.5 6 04.3	15.8 15.8 15.8 15.8	59.2 59.2 59.2 59.3 59.3 59.3	N 40 35 30 20 N 10 0	06 12 06 03 05 54 05 38 05 21 05 04	06 46 06 35 06 24 06 05 05 48 05 31	07 17 07 03 06 50 06 29 06 11 05 53	01 12 01 11 01 10 01 08 01 07 01 05	02 24 02 19 02 14 02 07 02 00 01 54	03 39 03 30 03 22 03 09 02 57 02 46	04 58 04 45 04 34 04 15 03 58 03 42
18 19 20 21 22 23	105 51.7 120 51.4 135 51.1 150 50.8 165 50.4	\$23 23.5 23.5 23.6 23.7 23.7 23.8	155 36.8 1 170 07.2 1 184 37.6 1 199 07.9 1 213 38.1 1 228 08.2 1	11.4 11.3 11.2 11.1	6 35.8 6 51.6 7 07.3 7 23.0 7 38.7	15.8 15.7 15.7 15.7 15.7	59.4 59.4 59.4 59.5 59.5 59.5	\$ 10 20 30 35 40 45	04 45 04 23 03 54 03 35 03 12 02 41	05 12 04 52 04 27 04 12 03 54 03 31	05 36 05 17 04 55 04 42 04 26 04 08	01 04 01 03 01 01 01 00 00 59 00 58	01 48 01 41 01 34 01 30 01 25 01 20	02 35 02 23 02 10 02 03 01 54 01 44	03 27 03 11 02 52 02 41 02 29 02 15
1900 01 02 03 04 05	180 50.1 195 49.8 210 49.5 225 49.2 240 48.9 255 48.6	\$23 23.9 23.9 24.0 24.1 24.1 24.2	242 38.3 1 257 08.2 1 271 38.1 1 286 07.9 1 300 37.7 1 315 07.3 1	10.9 10.8 10.8 10.6	7 54.4 8 10.0 8 25.6 8 41.2 8 56.8 9 12.3	15.6 15.6 15.6 15.5	59.6 59.6 59.6 59.7 59.7 59.7	\$ 50 52 54 56 58 \$ 60	01 56 01 28 00 41 //// ////	03 01 02 46 02 28 02 06 01 36 00 46	03 46 03 35 03 23 03 08 02 52 02 31	00 57 00 56 00 55 00 55 00 54 00 53	01 13 01 10 01 07 01 03 01 00 00 55	01 32 01 27 01 21 01 14 01 07 00 59	01 57 01 49 01 40 01 30 01 18 01 05
06 07 08 F 09	270 48.3 285 48.0 300 47.7 315 47.4	\$23 24.2 24.3 24.4 24.4	329 36.9 1 344 06.4 1 358 35.7 1 13 05.0 1	10.3	9 27.8 9 43.3 9 58.7 10 14.1	15.4 15.4	59.8 59.8 59.8 59.8	Lat.	Sunset	Twil Civil	light Naut.	18	Mod 19	nset 20	21
R 10	330 47.0 345 46.7	24.5 24.5	27 34.2 1	10.2	10 29.5 10 44.8	15.3	59.9 59.9	N 72	h m	h m 12 59	h m 15 30	h m 12 24	h m 11 45	h m 10 34	h m
D 12 A 13 Y 14 Y 15 16 17	0 46.4 15 46.1 30 45.8 45 45.5 60 45.2 75 44.9	S23 24.6 24.6 24.7 24.7 24.8 24.8	56 32.4 71 01.3 85 30.1 99 58.9 114 27.5 128 56.0	9.8 9.8 9.6 9.5	11 00.1 11 15.3 11 30.5 11 45.6 12 00.7 12 15.7	15.2 15.1 15.1 15.0	59.9 60.0 60.0 60.0 60.1 60.1	N 70 68 66 64 62 60	13 21 14 03 14 32 14 53	14 01 14 36 15 02 15 21 15 37 15 51	15 50 16 06 16 19 16 30 16 39 16 48	12 31 12 36 12 41 12 45 12 48 12 52	12 02 12 17 12 28 12 38 12 47 12 54	11 19 11 49 12 12 12 30 12 45 12 58	10 41 11 44 12 19 12 45 13 05
18 19 20 21 22 23	90 44.6 105 44.3 120 44.0 135 43.6 150 43.3 165 43.0	\$23 24.9 24.9 25.0 25.0 25.1 25.1	143 24.5 157 52.8 172 21.0 186 49.2 201 17.2 215 45.1	9.2 9.2 9.0 8.9	12 30.7 12 45.6 13 00.5 13 15.3 13 30.0 13 44.7	14.9 14.8 14.7	60.1 60.2 60.2 60.2 60.2 60.3	N 58 56 54 52 50 45	15 11 15 26 15 38 15 49 15 59 16 20	16 03 16 13 16 22 16 30 16 38 16 54	16 55 17 02 17 08 17 14 17 19 17 31	12 54 12 57 12 59 13 01 13 03 13 07	13 00 13 06 13 11 13 16 13 20 13 30	13 09 13 18 13 27 13 35 13 42 13 56	13 22 13 37 13 49 14 00 14 10 14 30
20 00 01 02 03 04 05	180 42.7 195 42.4 210 42.1 225 41.8 240 41.5 255 41.2	\$23 25.2 25.2 25.3 25.3 25.4 25.4	230 12.9 244 40.6 259 08.2 273 35.7 288 03.1 302 30.3	8.6 8.5 8.4 8.2	13 59.3 14 13.8 14 28.3 14 42.7 14 57.0 15 11.3	14.5 14.4 14.3 14.3	60.3 60.3 60.4 60.4 60.4	N 40 35 30 20 N 10 0	16 37 16 51 17 03 17 25 17 43 18 01	17 07 17 19 17 30 17 49 18 06 18 23	17 42 17 51 18 00 18 16 18 32 18 49	13 10 13 13 13 16 13 20 13 24 13 28	13 37 13 44 13 50 14 00 14 09 14 18	14 09 14 19 14 29 14 45 14 59 15 12	14 47 15 01 15 14 15 35 15 54 16 11
06 S 07 S 08 A 09 T 10 U 11	270 40.9 285 40.5 300 40.2 315 39.9 330 39.6 345 39.3	\$23 25.4 25.5 25.5 25.5 25.6 25.6	345 51.4 0 18.2 14 44.9	7.9 7.8 7.7 7.6	15 25.5 15 39.5 15 53.6 16 07.5 16 21.3 16 35.1	14.1 13.9 13.8 13.8	60.4 60.5 60.5 60.5 60.5 60.6	S 10 20 30 35 40 45	18 18 18 37 18 59 19 12 19 27 19 45	18 41 19 02 19 27 19 42 20 00 20 23	19 08 19 31 20 00 20 19 20 42 21 13	13 32 13 36 13 40 13 43 13 46 13 50	14 27 14 36 14 46 14 52 14 59 15 08	15 25 15 40 15 56 16 06 16 17 16 30	16 28 16 47 17 09 17 22 17 36 17 54
R 12 D 13 A 14 Y 15 Y 16 17	0 39.0 15 38.7 30 38.4 45 38.1 60 37.7 75 37.4	\$23 25.7 25.7 25.7 25.8 25.8 25.8	72 30.5 86 56.6 101 22.6 115 48.5	7.2 7.1 7.0 6.9 6.8	16 48.7 17 02.3 17 15.7 17 29.1 17 42.4 17 55.6	13.4 13.4 13.3 13.2 13.0	60.6 60.6 60.7 60.7 60.7	\$ 50 52 54 56 58 \$ 60	20 08 20 19 20 31 20 45 21 02 21 23	20 53 21 08 21 26 21 48 22 18 23 09	21 58 22 26 23 13 //// ////	13 54 13 56 13 58 14 00 14 03 14 06	15 17 15 22 15 27 15 33 15 39 15 46	16 45 16 53 17 01 17 11 17 21 17 34	18 16 18 26 18 38 18 52 19 07 19 27
18 19	105 36.8	S23 25.9 25.9	130 14.3 144 39.9	6.5	18 08.6 18 21.6	12.8	60.7 60.8		Egn. c	SUN of Time	Mer.	Mer.		ON I	
20 21	120 36.5 135 36.2	25.9 25.9	159 05.4 173 30.8	6.3	18 34.4 18 47.2	12.6	60.8 60.8	Day	00 ^h	12 ^h	Pass.	Upper	Lower		hase
	150 35.9 165 35.6	26.0 26.0	187 56.1 202 21.2	6.1 S	18 59.8 19 12.3	12.4	60.8	18 19	m s 03 51 03 21	m s 03 36 03 06	h m 11 56 11 57	h m 07 17 08 06	h m 19 41 20 32	d % 25 31 26 21	
I Han	SD 16.3	d 0.1	SD 1	16.1	16.3		16.5	20	02 51	02 37	11 57	08 59	21 27	27 12	

POLARIS (POLE STAR) TABLES, 2003 FOR DETERMINING LATITUDE FROM SEXTANT ALTITUDE AND FOR AZIMUTH

LHA	0° -	10° -	20° -	30° -	40° -	50° -	60° –	70° -	80° –	90° -	100° –	110° -
ARIES	9°	19°	29°	39°	49°	59°	69°	79°	89°	99°	109°	119°
۰	a _o	a ₀	ao	a _o	a ₀	a _o	a_0					
0	0 25.3	0 21.0	0 17.9	0 16.1	0 15.6	0 16.4	0 18.6	0 21.9	0 26.4	0 31.9	0 38.2	۰ ,
1	24.8	20.7	17.7	16.0	15.6	16.6	18.8	22.3	26.9	32.5	38.9	732
2	24.3	20.3	17.5	15.9	15.7	16.8	19.1	22.7	27.5	33.1	39.6	45.9
3	23.9	20.0	17.3	15.8	15.7	16.9	19.5	23.2	28.0	33.7	40.3	46.6
4	23.4	19.6	17.1	15.8	15.8	17.1	19.8	23.6	28.5	34.4	40.9	47·3 48·1
5	0 23.0	0 19.3	0 16.9	0 15.7	0 15.9	0 17.3	0 20.1	0 24·I	0 29.1	0 35.0	0 41.6	0 48.8
	22.6	19.0	16.7	15.7	15.9	17.6	20.4	24.5	29.6	35.6	42.3	49.5
7	22.2	18.7	16.5	15.6	16.0	17.8	20.8	25.0	30.2	36.3	43.0	50.3
	21.8	18.5	16.4	15.6	16.2	18.0	21.2	25.5	30.8	36.9	43.7	51.0
9	21.4	18.2	16.2	15.6	16.3	18.3	21.5	25.9	31.3	37.6	44.5	51.8
10	0 21.0	0 17.9	0 16.1	0 15.6	0 16.4	0 18.6	0 21.9	0 26.4	0 31.9	0 38.2	0 45.2	0 52.5
Lat.	<i>a</i> ₁	a_1										
0	0.5	0.2	0.6	0.6	0.6	0.6	0.2	0.2	0.4	0.4	0.3	0.3
10	.2	.6	.6	.6	.6	-6	·5 ·6	.2	.2	.4	.4	.3
20	.5	.6	.6	.6	.6	.6		.5	.2	•4	·4	.4
30	.5	.6	.6	.6	.6	.6	.6	.2	.2	.2	.2	.4
40	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.5	0.5	0.5
45	.6	.6	.6	.6	.6	.6	.6	.6	.6	.6	.6	.6
50	.6	.6	.6	.6	.6	.6	.6	.6	.6	.6	.6	.6
55	-6	.6	.6	-6	.6	.6	.6	-6	-6	.6	.7	.7
60	-6	.6	.6	.6	.6	.6	.6	.7	.7	.7	.7	.7
62	0.7	0.6	0.6	0.6	0.6	0.6	0.6	0.7	0.7	0.7	0.8	0.8
64	.7	.6	·6	.6	.6	.6	.6	-7	.7	·8	-8	.8
66 68	·7 0·7	·6	0.6	·6 o·6	·6 o·6	·6 o·6	·7 0·7	·7 0·7	·7 o·8	0.8	·8	.9
Month	a ₂	a_2	a ₂	a ₂	a ₂	0.9						
	,	,	,	,	,	,	,	,	,	1	,	a ₂
Jan.	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.6
Feb.	.6	.7	.7	.7	.8	-8	.8	-8	.8	.8	.8	-8
Mar.	.2	.2	-6	.6	.7	.7	-8	-8	.9	.9	.9	.9
Apr.	0.3	0.4	0.2	0.5	0.6	0.6	0.7	0.8	0.8	0.9	0.9	0.9
May	·2	.3	.3	.4	-4	.2	-6	-6	.7	-8	.8	.9
June	·2	.5	.2	.3	.3	.4	.4	.2	.6	-6	.7	.8
July	0.3	0.5	0.5	0.5	0.3	0.3	0.3	0.4	0.4	0.2	0.2	0.6
Aug.	.4	.3	.3	.3	.3	.3	.3	.3	.3	.4	.4	.4
Sept.	-6	.5	.2	.4	-4	.3	.3	.3	.3	.3	.3	.3
Oct.	0.8	0.7	0.6	0.6	0.5	0.5	0.4	0.4	0.3	0.3	0.3	0.3
Nov.	0.9	0.9	0.8	.8	.7	.6	.6	.2	.4	.4	.3	.3
Dec.	1.0	1.0	1.0	0.9	0.9	0.8	0.7	0.7	0.6	0.5	0.4	0.4
Lat.					1	AZIM	1					
0	0.4	0.3	0.2	0.0	359.9	359.8	359.7	359.6	359.5	359.4	359.3	359.3
20	0.4	0.3	0.5	0.1	359.9	359.8	359 7	359.5	359.4	359 4	359.3	359.3
40	0.5	0.4	0.2	0.1	359.9	359.7	359.6	359.4	359.3	359.2	359.1	359.1
50	0.6	0.5	0.3	0.1	359.9	359.7	359.5	359.3	359.2		359.0	358-9
55	0.0	0.5	0.3	0.1	359.9	359.6	359.4	359.3	359·1	359·I	358.8	358.8
60	0.8	0.6	0.4	0.1	359.8	359.6	359.4	359.1	358.9	358.8	358.7	358.6
65	1.0	0.7	0.4	0.1	359.8	359.5	359.2	359.0	358.7	358.6	358.4	358.3
~5		/			337 3	3373	339 ~	339 3	3301	350 5	330 4	3323

Latitude = Apparent altitude (corrected for refraction) $-1^{\circ} + a_0 + a_1 + a_2$

The table is entered with LHA Aries to determine the column to be used; each column refers to a range of 10° . a_0 is taken, with mental interpolation, from the upper table with the units of LHA Aries in degrees as argument; a_1 , a_2 are taken, without interpolation, from the second and third tables with arguments latitude and month respectively. a_0 , a_1 , a_2 , are always positive. The final table gives the azimuth of *Polaris*.

POLARIS (POLE STAR) TABLES, 2003 FOR DETERMINING LATITUDE FROM SEXTANT ALTITUDE AND FOR AZIMUTH

LHA	120° –	130° -	140° -	150° -	160° –	170° -	180° –	190° –	200° –	210° -	220° –	230°
ARIES	129°	139°	149°	159°	169°	179°	189°	199°	209°	219°	229°	23
٥	a ₀	a ₀	ao	ao	ao	ao	ao	a_0	a _o	ao	ao	a_{o}
0	0 52.5	I 00·0	1 07.5	I 14·7	0 / I 21·4	1 27·4	7 006	0 /	0 /	0 /	0 /	0
I	53.3	00.8	08.2	15.4	22.1	1 27·4 28·0	I 32·6	I 36·7	1 39·7 40·0	1 41.5	I 42.0	I 41
2	54.0	01.5	09.0	16.1	22.7	28.5	33.5	37.4	40.2	41.6	42·0 41·9	40
3	54.8	02.3	09.7	16.8	23.3	29.1	33.9	37.8	40.4	41.8	41.9	40
4	55.5	03.0	10.4	17.5	23.9	29.6	34.4	38.1	40.6	41.9	41.8	40
5	0 56.3	1 03.8	I II-2	1 18-1	I 24.5	1 30.1	1 34.8	1 38.4	1 40.8	1 41.9	1 41.8	1 40
6	57.0	04.5	11.9	18.8	25.1	30.6	35.2	38.7	40.9	41.9	41.7	40
7	57.8	05.3	12.6	19.5	25.7	31.1	35.6	39.0	41.1	42.0	41.6	39
8	58.5	06.0	13.3	20·I	26.3	31.6	36.0	39.2	41.2	42.0	41.5	39
9	0 59.3	06.8	14.0	20.8	26.9	32.1	36.4	39.5	41.4	42.0	41.3	39
10	I 00.0	I 07·5	I 14·7	I 21.4	I 27·4	I 32·6	I 36·7	I 39·7	1 41.5	I 42·0	I 41·2	1 39
Lat.	a_1	$a_{\rm I}$	$a_{\rm I}$	$a_{\rm I}$	a_1	$a_{\rm I}$	$a_{\rm I}$	$a_{\rm I}$	$a_{\scriptscriptstyle \rm I}$	$a_{\rm I}$	$a_{\rm I}$	$a_{\scriptscriptstyle \rm I}$
0	0.3	0.3	0.3	0.3	0.4	0.4	0.5	0.5	0.6	0.6	0.6	0.6
10	.3	.3	.3	.4	•4	.5	.5	.6	.6	.6	.6	.6
20	.4	.4	.4	-4	.5	.5	.5	.6	.6	-6	-6	.6
30	·4	•4	.4	-5	.5	.5	.5	.6	.6	.6	.6	.6
40	0.5	0.5	0.5	0.5	0.5	0.6	0.6	0.6	0.6	0.6	0.6	0.6
45	·5 ·6	·5	.6	.6	.6	.6	-6	.6	-6	.6	.6	.6
50		-6	.6	·6	.6	.6	-6	-6	-6	.6	.6	.6
55	.7	.7	.7	.7	-6	·6	.6	.6	-6	-6	-6	.6
60	.7	.7	.7	.7	.7	.7	.6	.6	.6	.6	.6	.6
62	0.8	0.8	0.8	0.8	0.7	0.7	0.7	0.6	0.6	0.6	0.6	0.6
64	.8	.8	.8	-8	-8	.7	.7	.6	-6	.6	.6	-6
68	.9	.9	.9	-8	·8	.7	.7	.6	.6	.6	.6	.6
Month	0.9	0.9	0.9	0.9		0.8	0.7	0.7	0.6	0.6	0.6	0.6
	a ₂	a ₂	a ₂	a ₂								
Jan.	0.6	0.6	0.6	0.6	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
Feb.	-8	.7	.7	.7	-6	.6	.6	.5	.5	.5	.4	.4
Mar.	0.9	0.9	0.9	0.8	-8	.8	.7	.7	.6	.6	.5	.5
Apr.	I.0	1.0	I.O	1.0	0.9	0.9	0.9	0.8	0.7	0.7	0.6	0.6
May	0.9	1.0	1.0	1.0	1.0	I .O	I.O	0.9	0.9	-8	.8	·7 ·8
June	-8	0.9	0.9	I.O	1.0	1.0	1.0	I.0	1.0	0.9	.9	.8
July	0.7	0.7	0.8	0.8	0.9	0.9	0.9	1.0	1.0	1.0	0.9	0.9
Aug.	.5	-6	-6	.7	.7	-8	.8	0.9	0.9	0.9	.9	.9
Sept.	.4	.4	.4	.5	.5	.6	.6	.7	.7	.8	.8	.9
Oct.	0.3	0.3	0.3	0.3	0.4	0.4	0.4	0.5	0.6	0.6	0.7	0.7
Nov. Dec.	.2	.2	.2	·2	.5	.5	.3	.3	.4	.4	.5	.6
	0.3	0.2	0.2	0.5	0.5	0.2	0.5	0.5	0.5	0.3	0.3	0.4
Lat.	ř	1				AZIM	JTH					
0	250.2	0 0 0	0	0		0	٥	0	۰	۰	٥	0
20	359·3 359·2	359·3 359·2	359.3	359.4	359.4	359.5	359.6	359.7	359.8	0.0	O. I	0.5
40	359·I	359.1	359·1	359.3	359.4	359.5	359.6	359.7	359.8	359.9	0·I	0.5
				359.2	359.2	359.4	359.5	359.6	359.8	359.9	O. I	0.3
50	358.9	358.9	358.9	359.0	359.1	359.2	359.4	359.6	359.7	359.9	0.1	0.3
55 60	358·7 358·6	358·8 358·6	358.8	358.9	359.0	359.1	359.3	359.5	359.7	359.9	0.1	0.3
65	358.3	358.3	358·6 358·4	358·7 358·5	358·9 358·6	359.0	359.2	359.4	359.7	359.9	0.2	0.4
-5	3303	2202	330 4	220 2	2200	358.8	359·I	359.3	359.6	359.9	0.2	0.5

ILLUSTRATION
On 2003 April 21 at
23h 18m 56s UT in longitude
W 37° 14' the apparent altitude
(corrected for refraction), Ho, of
Polaris was 49° 31'6

From the daily pages:	0	,
GHA Aries (23h)		35.9
Increment (18 ^m 56 ^s)	4	44.8
Longitude (west)	-37	14
LHA Aries	162	07

H_{O}	49	31.6	
a_0 (argument 162° 07')	I	22.8	
a_1 (Lat 50° approx.)		0.6	
a ₂ (April)		0.9	
$Sum - 1^{\circ} = Lat =$	49	55.9	

POLARIS (POLE STAR) TABLES, 2003 FOR DETERMINING LATITUDE FROM SEXTANT ALTITUDE AND FOR AZIMUTH

LHA	240° –	250° -	260° –	270° –	280° –	290° –	300° -	310° -	320° –	330° -	340° -	350° -
ARIES	249°	259°	269°	279°	289°	299°	309°	319°	329°	339°	349°	359°
	a ₀	a ₀	a _o	a ₀	. a ₀	a ₀	a ₀ ,	. a ₀	. a _o	a ₀	a ₀	a _o
0	I 39·I	1 35.8	1 31.4	I 26·I	I 19·9	I 13·0	I 05·7	0 58.2	0 50.7	0 43.5	0 36.7	0 30.5
I	38.8	35.4	30.9	25.5	19.2	12.3	05.0	57.5	50.0	42.8	36.0	30.0
2	38.6	35.0	,30.4	24.9	18.5	11.6	04.2	56.7	49.2	42·I	35.4	29.4
3	38.3	34.6	29.9	24.3	17.9	10.9	03.2	56.0	48.5	41.4	34.7	28.8
4	37.9	34.2	29.4	23.7	17.2	10.1	02.7	55.2	47.8	40.7	34.1	28-
5	I 37·6	I 33·8	1 28.9	I 23·I	1 16.5	1 09.4	I 02.0	0 54.5	0 47·0 46·3	0 40.0	0 33.5	0 27.8
	37.3	33.3	28.3	22.4	15.8	08.7	01.2	53.7	45.6	39·3 38·6	32.9	27:
7	36·9 36·6	32.9	27·8 27·2	21.8	15·1 14·4	07·9 07·2	I 00·5	53·0 52·2	44.9	38.0	32.3	26.
	36.2	32·4 31·9	26.6	20.5	13.7	06.5	59.0	51.5	44.2	37.3	31.1	26.
9	I 35·8	I 31·4	1 26.1	I 19·9	I 13.0	1 05.7	0 58.2	0 50.7	0 43.5	0 36.7	0 30.5	0 25
Lat.	a ₁	a_1	$a_{\rm I}$	a _I	a _I	<i>a</i> ₁	ar	$a_{\scriptscriptstyle \rm I}$	a ₁	$a_{\rm I}$	$a_{\rm I}$	a ₁
0	0.5	0.5	0.4	0.4	0.3	0.3	0.3	0.3	0.3	0.3	0.4	0.4
10		.5	.5	·4	-4	.3	.3	.3	.3	.4	.4	.5
20	·5 ·6	.5	.5	-4	-4	-4	-4	-4	-4	.4	-5	.5
30	.6	.5	.5	.5	.5	•4	.4	•4	•4	.5	.5	.5
40	0.6	0.6	0.6	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.6
45	-6	.6	.6	.6	-6	-6	.5	.5	.6	.6	.6	.6
50	.6	.6	-6	-6	.6	.6	-6	-6	-6	.6	.6	.6
55	-6	-6	-6	-6	.7	.7	.7	.7	.7	.7	.6	.6
60	.6	.7	.7	.7	.7	.7	.7	.7	.7	.7	.7	.7
62	0.6	0.7	0.7	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.7	0.7
64	-6	.7	.7	-8	-8	.8	-8	-8	·8 ·9	-8	-8	.7
66 68	·7 0·7	·7 0·7	·7 o·8	·8	·8	0.9	0.9	0.9	0.9	0.9	0.8	·7 o·8
Month	a ₂	a ₂	a ₂	a ₂	a ₂	a ₂	a ₂	<i>a</i> ₂				
T	'-	,	,	,	0.5	0.6	0.6	0.6	0.6	0.6	0.7	0.7
Jan. Feb.	0·5 ·4	0.5	0.5	0.5	.4	.4	-4	.5	.5	.5	.6	.6
Mar.	.4	.4	-3	.3	-3	-3	-3	.3	-3	.4	.4	.4
Apr.	0.5	0.4	0.4	0.3	0.3	0.3	0.5	0.5	0.2	0.2	0.3	0.3
May	.6	.6		-4	.4	.3	-3	.2	.2	.2	.2	.2
June	-8	.7	.6	-6	.5	•4	•4	.3	.3	·2	·2	.2
July	0.9	0.8	0.8	0.7	0.7	0.6	0.5	0.5	0.4	0.4	0.3	0.3
Aug.	.9	.9	.9	-8	·8	.8	.7	-6	-6	.5	.5	.4
Sept.	.9	.9	.9	.9	.9	.9	.8	.8	.8	.7	.7	.6
Oct.	0.8	0.8	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.8	0.8
Nov.	.6	.7	.8	-8	-9	.9	1.0	I.0	I.0	I.0	1.0	1.0
Dec.	0.2	0.2	0.6	0.7	0.8	0.8	0.9	I.0	1.0	1.0	1.0	1.0
Lat.				7		i	IUTH		ĭ	F	r	314
0	0	۰		0	0	0.7	0.7	0.7	0.7	0.6	0.6	0.5
0	0.3	0.4	0.5	0.6	0.7	0.7	0.7	0.7	0.7	0.0	0.6	0.5
20 40	0.3	0.5	0.6	0.8	0.7	0.7	0.9	0.9	0.9	0.8	0.8	0.7
	1		0.8				1.1	1.1	I.I	1.0	0.9	0.8
50	0.5	0.7	0.8	0.9	I.I I.0	I·I I·2	1.1	1.3	1.1	1.1	1.0	0.9
55 60	0.5	0.8	1.0	1.0	1.3	1.4	1.4	1.4	1.4	1.3	1.2	1.0
65	0.7	1.0	1.2	1.4	1.5	1.6	1.7	1.7	1.6	1.5	1.4	1.2
	J ,	1	1		1 - 2		1 - /	1 -				1

Latitude = Apparent altitude (corrected for refraction) $-1^{\circ} + a_0 + a_1 + a_2$

The table is entered with LHA Aries to determine the column to be used; each column refers to a range of 10° . a_0 is taken, with mental interpolation, from the upper table with the units of LHA Aries in degrees as argument; a_1 , a_2 are taken, without interpolation, from the second and third tables with arguments latitude and month respectively. a_0 , a_1 , a_2 , are always positive. The final table gives the azimuth of *Polaris*.

Increments and Corrections

•					-		_	-		-	-	1		T I	-	1		T	-	-
ő	SUN PLANETS	ARIES	MOON	or Con	rro	or Co	rrn	or Co	orra		ī	SUN PLANETS	ARIES	моом	or C	_	or Co	orrn	or Co)Lha
00 01 02	0 00-0 0 00-3 0 00-5	0 00-0 0 00-3 0 00-5	0 00-0 0 00-2 0 00-5	0-1 (0.0	6·1 6·2	0.1	12 • 1 12 • 2	0·1 0·1 0·1 0·1		00 01 02 03	0 15-0 0 15-3 0 15-5 0 15-8	0 15-0 0 15-3 0 15-5 0 15-8	0 14-3 0 14-6 0 14-8 0 15-0	0.0 0.1 0.2 0.3	0-0 0-0 0-0 0-0	6-0 6-1 6-2 6-3	0·2 0·2 0·2 0·2	12-0 12-1 12-2 12-3	0·3 0·3 0·3 0·3
03 04	0 00-8	0 00-8	0 00-7 0 01-0 0 01-2	0-4 (0-0	6-4		12-4	0.1		04	0 16-0	0 16-0	0 15·3 0 15·5	0+4	0-0	6-4	0·2 0·2	12-4	0.3
05 06 07 08	0 01-3 0 01-5 0 01-8 0 02-0	0 01-3 0 01-5 0 01-8 0 02-0	0 01-4 0 01-7 0 01-9	0-6 (0-7 (0-8 (0-0 0-0	6-6 6-7 6-8	0·1 0·1 0·1	12·6 12·7 12·8	0·1 0·1 0·1		06 07 08 09	0 16-5 0 16-8 0 17-0 0 17-3	0 16-5 0 16-8 0 17-0 0 17-3	0 15-7 0 16-0 0 16-2 0 16-5	0-6 0-7 0-8 0-9	0-0 0-0 0-0	6-6 6-7 6-8 6-9	0·2 0·2 0·2 0·2	12-6 12-7 12-8 12-9	0·3 0·3 0·3 0·3
10 10 11	0 02-3 0 02-5 0 02-8	0 02-3 0 02-5 0 02-8	0 02-1 0 02-4 0 02-6	1.0	0-0 0-0	7-0	0·1 0·1	12·9 13·0 13·1	0·1 0·1		10 11	0 17-5 0 17-8	0 17-5 0 17-8	0 16-7 0 16-9	1.0	0-0	7-0 7-1	0-2 0-2	13-0 13-1	0.3
12 13 14	0 03-0 0 03-3 0 03-5	0 03·0 0 03·3 0 03·5	0 02-9 0 03-1 0 03-3	1-3	0-0 0-0 0-0	7·2 7·3 7·4	0·1 0·1 0·1	13 · 2 13 · 3 13 · 4	0·1 0·1 0·1		12 13 14	0 18-0 0 18-3 0 18-5	0 18-0 0 18-3 0 18-6	0 17-2 0 17-4 0 17-7	1·2 1·3 1·4	0-0 0-0	7·2 7·3 7·4	0·2 0·2 0·2	13·2 13·3 13·4	0·3 0·3 0·3
15 16 17 18	0 03-8 0 04-0 0 04-3 0 04-5	0 03-8 0 04-0 0 04-3 0 04-5	0 03-6 0 03-8 0 04-1 0 04-3	1.6 1.7 1.8	0-0 0-0 0-0	7-5 7-6 7-7 7-8	0·1 0·1 0·1 0·1	13 · 5 13 · 6 13 · 7 13 · 8	0·1 0·1 0·1 0·1		15 16 17 18	0 18-8 0 19-0 0 19-3 0 19-5	0 18-8 0 19-1 0 19-3 0 19-6	0 17-9 0 18-1 0 18-4 0 18-6	1.5 1.6 1.7 1.8	0-0 0-0 0-0 0-0	7·5 7·6 7·7 7·8 7·9	0·2 0·2 0·2 0·2 0·2	13·5 13·6 13·7 13·8 13·9	0·3 0·3 0·3
19 20 21 22	0 04-8 0 05-0 0 05-3 0 05-5	0 04-8 0 05-0 0 05-3 0 05-5	0 04-5 0 04-8 0 05-0 0 05-2	2·0 2·1	0-0	7·9 8·0 8·1 8·2	0·1 0·1 0·1	13·9 14·0 14·1 14·2	0·1 0·1 0·1 0·1		19 20 21 22	0 19-8 0 20-0 0 20-3 0 20-5	0 19-8 0 20-1 0 20-3 0 20-6	0 189 0 19·1 0 19·3 0 19·6	2·0 2·1 2·2	0·1 0·1 0·1	8-0 8-1 8-2 8-3	0·2 0·2 0·2 0·2	14-0 14-1 14-2	0-3 0-4 0-4
23 24 25	0 05-8 0 06-0 0 06-3	0 05-8 0 06-0 0 06-3	0 05-5 0 05-7 0 06-0		0-0	8-3 8-4 8-5	0·1 0·1	14-3 14-4 14-5	0·1 0·1		23 24 25	0 20-8 0 21-0 0 21-3	0 20·8 0 21·1 0 21·3	0 19-8 0 20-0 0 20-3	2·3 2·4 2·5	0·1 0·1	8-4	0.2	14-3 14-4 14-5	04 04 04
26 27 28 29	0 06-5 0 06-8 0 07-0 0 07-3	0 06-5 0 06-8 0 07-0 0 07-3	0 06-2 0 06-4 0 06-7 0 06-9	2·6 2·7 2·8 2·9	0-0 0-0 0-0	8-6 8-7 8-8 8-9	0·1 0·1 0·1 0·1	14-6 14-7 14-8 14-9	0·1 0·1 0·1 0·1		26 27 28 29	0 21-5 0 21-8 0 22-0 0 22-3	0 21-6 0 21-8 0 22-1 0 22-3	0 20-5 0 20-8 0 21-0 0 21-2	2.6 2.7 2.8 2.9	0·1 0·1 0·1	8-6 8-7 8-8 8-9	0·2 0·2 0·2 0·2	14-6 14-7 14-8 14-9	0-4 0-4 0-4
30 31 32 33 34	0 08-3	0 07-5 0 07-8 0 08-0 0 08-3 0 08-5	0 07-2 0 07-4 0 07-6 0 07-9 0 08-1	3·0 3·1 3·2 3·3	0·0 0·0 0·0 0·0	9+0 9+1 9+2 9+3 9+4	0·1 0·1 0·1 0·1 0·1	15-0 15-1 15-2 15-3 15-4	0·1 0·1 0·1 0·1		30 31 32 33 34	0 22·5 0 22·8 0 23·0 0 23·3 0 23·5	0 22-6 0 22-8 0 23-1 0 23-3 0 23-6	0 21·5 0 21·7 0 22·0 0 22·2 0 22·4	3·0 3·1 3·2 3·3 3·4	0·1 0·1 0·1 0·1	9-0 9-1 9-2 9-3 9-4	0·2 0·2 0·2 0·2 0·2	15·0 15·1 15·2 15·3 15·4	04 04 04 04 04
35 36 37 38	0 08-8 0 09-0 0 09-3 0 09-5	0 08-8 0 09-0 0 09-3 0 09-5	0 08-4 0 08-6 0 08-8 0 09-1	3·5 3·6 3·7 3·8	0-0 0-0 0-0	9+5 9+6 9+7 9+8	0·1 0·1 0·1	15-5 15-6 15-7 15-8 15-9	0·1 0·1 0·1 0·1		35 36 37 38 39	0 23-8 0 24-0 0 24-3 0 24-5 0 24-8	0 23-8 0 24-1 0 24-3 0 24-6 0 24-6	0 22 9 0 23·1 0 23·4	3.5 3.6 3.7 3.8 3.9	0·1 0·1 0·1 0·1	9-5 9-6 9-7 9-8 9-9	0.2 0.2 0.2 0.2 0.2	15-5 15-6 15-7 15-8 15-9	04 04 04 04
39 40 41 42	0 10-0 0 10-3 0 10-5	0 09-8 0 10-0 0 10-3 0 10-5	0 09-5 0 09-8 0 10-0	3-9 4-0 4-1 4-2	0-0 0-0 0-0	9-9 10-0 10-1 10-2	0·1 0·1 0·1	16-0 16-1 16-2 16-3	0·1 0·1 0·1 0·1	-	40 41 42 43	0 25-0 0 25-3 0 25-5 0 25-8	0 25-1 0 25-3 0 25-6	0 23-9 0 24-1 0 24-3	4-0 4-1 4-2 4-3	0·1 0·1 0·1		0·3 0·3 0·3	16-0 16-1 16-2 16-3	04 04 04 04
4:	0 11-0	0 10-8 0 11-0 0 11-3	0 10-5	4-3 4-4 4-5	0-0	10-3 10-4 10-5	0·1 0·1	16·4 16·5	0.1	-	44 45 46	0 26-0 0 26-3 0 26-5	0 26-3	0 24-8	4-4	0·1 0·1 0·1	10-4	0.3	16-4	0-4 0-4 0-4
41	7 0 11-8 3 0 12-0	0 11-5 0 11-6 0 12-0 0 12-3	0 11-2	4·6 4·7 4·8 4·9	0-0 0-0 0-0	10-6 10-7 10-8 10-9	0·1 0·1 0·1	16·6 16·7 16·8 16·9	0·1 0·1 0·1		47 48 49	0 26-8 0 27-0	0 264	0 25-5	4-7 4-8 4-9	0-1 0-1 0-1	10-7	0.3	16-9	
5 5 5	1 0 12-8 2 0 13-0 3 0 13-3	0 13-0	0 12-2 0 0 12-4 0 0 12-6	5+0 5+1 5+2 5+3 5+4	0-0 0-0 0-0 0-0	11-0 11-1 11-2 11-3 11-4	0·1 0·1 0·1 0·1	17·0 17·1 17·2 17·3 17·4	0·1 0·1 0·1 0·1		50 51 52 53 54	0 27-8 0 28-0 0 28-3	0 274 0 28- 0 28-	0 26-5 0 26-7 0 27-0	5-1 5-2 5-1	0·1 0·1 0·1	11-1	0-3 0-3 0-3	17-1	0-4 0-4 0-4
5 5 5	5 0 13-8 6 0 14-0 7 0 14-3	0 134 0 144 0 144	0 13-1 0 0 13-4 3 0 13-6	5-5 5-6 5-7	0-0 0-0 0-0	11·5 11·6 11·7 11·8	0·1 0·1 0·1		0.1		55 56 57 58	0 29-0	0 29-	0 27-7	5-	0-1 7 0-1 8 0-1	11-	0.3	17 · 17 · 17 · 17 · 17 · 17 · 17 · 17 ·	04
5	9 0 14-8	0 14	8 0 14-1	5-9	0-0	11.9	0.1	17-9	0-1	1	59				11					
_				-		-	-	-	-	-										

INCREMENTS	AND	CORREC	CTIONS

2	SUN PLANETS	ARIES	моом	or Corra	or Corra	or Corra	3	SUN PLANETS	ARIES	моом	or Corra	or Corra	or Corra
00 01 02 03	0 30-0 0 30-3 0 30-5 0 30-8	0 30-1 0 30-3 0 30-6 0 30-8	0 28-6 0 28-9 0 29-1 0 29-3	, , 0-0 0-0 0-1 0-0 0-2 0-0 0-3 0-0	6-0 0-3 6-1 0-3 6-2 0-3 6-3 0-3	, , 12-0 0-5 12-1 0-5 12-2 0-5 12-3 0-5	00 01 02 03	0 45-0 0 45-3 0 45-5 0 45-8	0 45-1 0 45-4 0 45-6 0 45-9	0 43-0 0 43-2 0 43-4 0 43-7	, , 0-0 0-0 0-1 0-0 0-2 0-0 0-3 0-0	6-0 0-4 6-1 0-4 6-2 0-4 6-3 0-4	, , 12·0 0·7 12·1 0·7 12·2 0·7 12·3 0·7
04	0 31-0	0 31-1	0 29-6	0+4 0+0	6-4 0-3	12-4 0-5	04	0 46-0	0 46-1	0 43-9	0-4 0-0	6-4 0-4	12-4 0-7
05	0 31-3	0 31-3	0 29-8	0+5 0+0	6-5 0-3	12-5 0-5	05	0 46-3	0 46-4	0 44-1	0-5 0-0	6-5 0-4	12-5 0-7
06	0 31-5	0 31-6	0 30-1	0+6 0+0	6-6 0-3	12-6 0-5	06	0 46-5	0 46-6	0 44-4	0-6 0-0	6-6 0-4	12-6 0-7
07	0 31-8	0 31-8	0 30-3	0+7 0+0	6-7 0-3	12-7 0-5	07	0 46-8	0 46-9	0 44-6	0-7 0-0	6-7 0-4	12-7 0-7
08	0 32-0	0 32-1	0 30-5	0+8 0+0	6-8 0-3	12-8 0-5	08	0 47-0	0 47-1	0 44-9	0-8 0-0	6-8 0-4	12-8 0-7
09	0 32-3	0 32-3	0 30-8	0+9 0+0	6-9 0-3	12-9 0-5	09	0 47-3	0 47-4	0 45-1	0-9 0-1	6-9 0-4	12-9 0-8
10	0 32-5	0 32-6	0 31-0	1-0 0-0	7-0 0-3	13·0 0·5	10	0 47-5	0 47-6	0 45-3	1.0 0.1	7·0 0·4	13-0 0-8
11	0 32-8	0 32-8	0 31-3	1-1 0-0	7-1 0-3	13·1 0·5	11	0 47-8	0 47-9	0 45-6	1.1 0.1	7·1 0·4	13-1 0-8
12	0 33-0	0 33-1	0 31-5	1-2 0-1	7-2 0-3	13·2 0·6	12	0 48-0	0 48-1	0 45-8	1.2 0.1	7·2 0·4	13-2 0-8
13	0 33-3	0 33-3	0 31-7	1-3 0-1	7-3 0-3	13·3 0·6	13	0 48-3	0 48-4	0 46-1	1.3 0.1	7·3 0·4	13-3 0-8
14	0 33-5	0 33-6	0 32-0	1-4 0-1	7-4 0-3	13·4 0·6	14	0 48-5	0 48-6	0 46-3	1.4 0.1	7·4 0·4	13-4 0-8
15	0 33-8	0 33-8	0 32-2	1-5 0-1	7-5 0-3	13-5 0-6	15	0 48-8	0 48-9	0 46-5	1.5 0.1	7-5 0-4	13-5 0-8
16	0 34-0	0 34-1	0 32-5	1-6 0-1	7-6 0-3	13-6 0-6	16	0 49-0	0 49-1	0 46-8	1.6 0.1	7-6 0-4	13-6 0-8
17	0 34-3	0 34-3	0 32-7	1-7 0-1	7-7 0-3	13-7 0-6	17	0 49-3	0 49-4	0 47-0	1.7 0.1	7-7 0-4	13-7 0-8
18	0 34-5	0 34-6	0 32-9	1-8 0-1	7-8 0-3	13-8 0-6	18	0 49-5	0 49-6	0 47-2	1.8 0.1	7-8 0-5	13-8 0-8
19	0 34-8	0 34-8	0 33-2	1-9 0-1	7-9 0-3	13-9 0-6	19	0 49-8	0 49-9	0 47-5	1.9 0.1	7-9 0-5	13-9 0-8
20	0 35-0	0 35-1	0 33-4	2.0 0.1	8-0 0-3	14-0 0-6	20	0 50-0	0 50·1	0 47-7	2-0 0-1	8-0 0-5	14-0 0-8
21	0 35-3	0 35-3	0 33-6	2.1 0.1	8-1 0-3	14-1 0-6	21	0 50-3	0 50·4	0 48-0	2-1 0-1	8-1 0-5	14-1 0-8
22	0 35-5	0 35-6	0 33-9	2.2 0.1	8-2 0-3	14-2 0-6	22	0 50-5	0 50·6	0 48-2	2-2 0-1	8-2 0-5	14-2 0-8
23	0 35-8	0 35-8	0 34-1	2.3 0.1	8-3 0-3	14-3 0-6	23	0 50-8	0 50·9	0 48-4	2-3 0-1	8-3 0-5	14-3 0-8
24	0 36-0	0 36-1	0 34-4	2.4 0.1	8-4 0-4	14-4 0-6	24	0 51-0	0 51·1	0 48-7	2-4 0-1	8-4 0-5	14-4 0-8
25	0 36-3	0 36-3	0 34-6.	2.5 0.1	8-5 0-4	14-5 0-6	25	0 51-3	0 51-4	0 48-9	2-5 0-1	8-5 0-5	14-5 0-8
26	0 36-5	0 36-6	0 34-8	2.6 0.1	8-6 0-4	14-6 0-6	26	0 51-5	0 51-6	0 49-2	2-6 0-2	8-6 0-5	14-6 0-9
27	0 36-8	0 36-9	0 35-1	2.7 0.1	8-7 0-4	14-7 0-6	27	0 51-8	0 51-9	0 49-4	2-7 0-2	8-7 0-5	14-7 0-9
28	0 37-0	0 37-1	0 35-3	2.8 0.1	8-8 0-4	14-8 0-6	28	0 52-0	0 52-1	0 49-6	2-8 0-2	8-8 0-5	14-8 0-9
29	0 37-3	0 37-4	0 35-6	2.9 0.1	8-9 0-4	14-9 0-6	29	0 52-3	0 52-4	0 49-9	2-9 0-2	8-9 0-5	14-9 0-9
30	0 37-5	0 37-6	0 35-8	3.0 0.1	9-0 0-4	15-0 0-6	30	0 52-5	0 52-6	0 50-1	3-0 0-2	9-0 0-5	15-0 0-9
31	0 37-8	0 37-9	0 36-0	3.1 0.1	9-1 0-4	15-1 0-6	31	0 52-8	0 52-9	0 50-3	3-1 0-2	9-1 0-5	15-1 0-9
32	0 38-0	0 38-1	0 36-3	3.2 0.1	9-2 0-4	15-2 0-6	32	0 53-0	0 53-1	0 50-6	3-2 0-2	9-2 0-5	15-2 0-9
33	0 38-3	0 38-4	0 36-5	3.3 0.1	9-3 0-4	15-3 0-6	33	0 53-3	0 53-4	0 50-8	3-3 0-2	9-3 0-5	15-3 0-9
34	0 38-5	0 38-6	0 36-7	3.4 0.1	9-4 0-4	15-4 0-6	34	0 53-5	0 53-6	0 51-1	3-4 0-2	9-4 0-5	15-4 0-9
35	0 38-8	0 38-9	0 37-0	3-5 0-1	9-5 0-4	15-5 0-6	35	0 53-8	0 53-9	0 51-3	3-5 0-2	9-5 0-6	15-5 0-9
36	0 39-0	0 39-1	0 37-2	3-6 0-2	9-6 0-4	15-6 0-7	36	0 54-0	0 54-1	0 51-5	3-6 0-2	9-6 0-6	15-6 0-9
37	0 39-3	0 39-4	0 37-5	3-7 0-2	9-7 0-4	15-7 0-7	37	0 54-3	0 54-4	0 51-8	3-7 0-2	9-7 0-6	15-7 0-9
38	0 39-5	0 39-6	0 37-7	3-8 0-2	9-8 0-4	15-8 0-7	38	0 54-5	0 54-6	0 52-0	3-8 0-2	9-8 0-6	15-8 0-9
39	0 39-8	0 39-9	0 37-9	3-9 0-2	9-9 0-4	15-9 0-7	39	0 54-8	0 54-9	0 52-3	3-9 0-2	9-9 0-6	15-9 0-9
40	0 40·0	0 40-1	0 38-2	4-0 0-2	10-0 0-4	16-0 0-7	40	0 55-0	0 55-2	0 52-5	4-0 0-2	10·0 0·6	16-0 0-9
41	0 40·3	0 40-4	0 38-4	4-1 0-2	10-1 0-4	16-1 0-7	41	0 55-3	0 55-4	0 52-7	4-1 0-2	10·1 0·6	16-1 0-9
42	0 40·5	0 40-6	0 38-7	4-2 0-2	10-2 0-4	16-2 0-7	42	0 55-5	0 55-7	0 53-0	4-2 0-2	10·2 0·6	16-2 0-9
43	0 40·8	0 40-9	0 38-9	4-3 0-2	10-3 0-4	16-3 0-7	43	0 55-8	0 55-9	0 53-2	4-3 0-3	10·3 0·6	16-3 1-0
44	0 41·0	0 41-1	0 39-1	4-4 0-2	10-4 0-4	16-4 0-7	44	0 56-0	0 56-2	0 53-4	4-4 0-3	10·4 0·6	16-4 1-0
45	0 41-3	0 41-4	0 39-4	4-5 0-2	10-5 0-4	16·5 0·7	45	0 56-3	0 56-4	0 53-7	4-5 0-3	10-5 0-6	16-5 1-0
46	0 41-5	0 41-6	0 39-6	4-6 0-2	10-6 0-4	16·6 0·7	46	0 56-5	0 56-7	0 53-9	4-6 0-3	10-6 0-6	16-6 1-0
47	0 41-8	0 41-9	0 39-8	4-7 0-2	10-7 0-4	16·7 0·7	47	0 56-8	0 56-9	0 54-2	4-7 0-3	10-7 0-6	16-7 1-0
48	0 42-0	0 42-1	0 40-1	4-8 0-2	10-8 0-5	16·8 0·7	48	0 57-0	0 57-2	0 54-4	4-8 0-3	10-8 0-6	16-8 1-0
49	0 42-3	0 42-4	0 40-3	4-9 0-2	10-9 0-5	16·9 0·7	49	0 57-3	0 57-4	0 54-6	4-9 0-3	10-9 0-6	16-9 1-0
50	0 42·5	0 42-6	0 40-6	5-0 0-2	11-0 0-5	17-0 0-7	50	0 57-5	0 57-7	0 54-9	5-0 0-3	11-0 0-6	17-0 1-0
51	0 42·8	0 42-9	0 40-8	5-1 0-2	11-1 0-5	17-1 0-7	51	0 57-8	0 57-9	0 55-1	5-1 0-3	11-1 0-6	17-1 1-0
52	0 43·0	0 43-1	0 41-0	5-2 0-2	11-2 0-5	17-2 0-7	52	0 58-0	0 58-2	0 55-4	5-2 0-3	11-2 0-7	17-2 1-0
53	0 43·3	0 43-4	0 41-3	5-3 0-2	11-3 0-5	17-3 0-7	53	0 58-3	0 58-4	0 55-6	5-3 0-3	11-3 0-7	17-3 1-0
54	0 43·5	0 43-6	0 41-5	5-4 0-2	11-4 0-5	17-4 0-7	54	0 58-5	0 58-7	0 55-8	5-4 0-3	11-4 0-7	17-4 1-0
55	0 43-8	0 43-9	0 41-8	5-5 0-2	11-5 0-5	17·5 0·7	55	0 58-8	0 58-9	0 56·1	5-5 0-3	11-5 0-7	17.5 1-0
56	0 44-0	0 44-1	0 42-0	5-6 0-2	11-6 0-5	17·6 0·7	56	0 59-0	0 59-2	0 56·3	5-6 0-3	11-6 0-7	17.6 1-0
57	0 44-3	0 44-4	0 42-2	5-7 0-2	11-7 0-5	17·7 0·7	57	0 59-3	0 59-4	0 56·6	5-7 0-3	11-7 0-7	17.7 1-0
58	0 44-5	0 44-6	0 42-5	5-8 0-2	11-8 0-5	17·8 0·7	58	0 59-5	0 59-7	0 56·8	5-8 0-3	11-8 0-7	17.8 1-0
59	0 44-8	0 44-9	0 42-7	5-9 0-2	11-9 0-5	17·9 0·7	59	0 59-8	0 59-9	0 57·0	5-9 0-3	11-9 0-7	17.9 1-0
60	0 45-0	0 45-1	0 43-0	6-0 0-3	12-0 0-5	18-0 0-8	60	1 00-0	1 00-2	0 57-3	6-0 0-4	12-0 0-7	18-0 1-1

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20 21 22 23 24	1 05-0 1 05-3 1 05-5 1 05-8 1 06-0	1 05-2 1 05-4 1 05-7 1 05-9 1 06-2	1 02·0 1 02·3 1 02·5 1 02·8	2+0 0-2 2+1 0-2 2+2 0-2 2+3 0-2 2+4 0-2	8-0 0-6 8-1 0-6 8-2 0-6 8-3 0-6	14-1 1-1 14-2 1-1 14-3 1-1	20 21 22 23 24	1 20-0 1 20-3 1 20-5 1 20-8 1 21-0	1 20-2 1 20-5 1 20-7 1 21-0 1 21-2	1 16-4 1 16-6 1 16-8 1 17-1 1 17-3	2·0 0·2 2·1 0·2 2·2 0·2 2·3 0·2 2·4 0·2	8-3 0-8	14-0 1-3 14-1 1-3 14-2 1-3 14-3 1-3 14-4 1-3	2 2 2 2 2 2 2	1 13 2 13 3 13 4 13	35-3 35-5 35-8 36-0	1 35-5 1 35-8 1 36-0 1 36-3	1 30-9 1 31-1 1 31-4 1 31-6	2-1 0-2 2-2 0-2 2-3 0-2 2-4 0-3 2-5 0-3	8-1 0-9 8-2 0-9 8-3 0-9 8-4 0-9 8-5 0-9	14-1 1-5 14-2 1-5 14-3 1-5 14-4 1-6	21 22 23 24 25	1 50-3 1 50-5 1 50-8 1 51-0	1 50-6 1 50-8 1 51-1 1 51-3	1 45-2 1 45-5 1 45-7 1 45-9	2·1 0·3 2·2 0·3 2·3 0·3 2·4 0·3	8-1 1 8-2 1 8-3 1 8-4 1	0 14-1 0 14-2 0 14-3 1 14-4	1-8
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30 31 32 33	1 07-3 1 07-5 1 07-8 1 08-0 1 08-3	1 07-4 1 07-7 1 07-9 1 08-2 1 08-4	1 05-1	3-9 0-2 3-0 0-2 3-1 0-2 3-2 0-2 3-3 0-2	9-0 0-7 9-1 0-7 9-2 0-7 9-3 0-7	7 15-0 1-1 7 15-1 1-1 7 15-2 1-1 7 15-3 1-1	30 31 32 33 34	1 22·5 1 22·8 1 23·0	1 22-7 1 23-0 1 23-2 1 23-5 1 23-7	1 18-7 1 19-0 1 19-2 1 19-5 1 19-7	3-0 0-3 3-1 0-3 3-2 0-3 3-3 0-3 3-4 0-3	9-1 0-8 9-2 0-8 9-3 0-9	15-0 1-4 15-1 1-4 15-2 1-4 15-3 1-4 15-4 1-4	3 3 3 3 3	1 13 2 13 3 13 4 13	17-8 18-0 18-3 18-5	1 37-8 1 38-0 1 38-3 1 38-5 1 38-8		3·0 0·3 3·1 0·3 3·2 0·3 3·3 0·4 3·4 0·4	9-0 1-0 9-1 1-0 9-2 1-0 9-3 1-0 9-4 1-0	15-0 1-6 15-1 1-6 15-2 1-6 15-3 1-7 15-4 1-7	30 31 32 33 34	1 52-5 1 52-8 1 53-0 1 53-3 1 53-5	1 52-8 1 53-1 1 53-3 1 53-6 1 53-8	1 47-4 1 47-6 1 47-9 1 48-1 1 48-3	3-0 0-4 3-1 0-4 3-2 0-4 3-3 0-4 3-4 0-4	9-0 1 9-1 1 9-2 1 9-3 1 9-4 1	1 15-1 2 15-2 2 15-3 2 15-4	1.9
34 35 36 37 38	1 08-5 1 08-8 1 09-0 1 09-3 1 09-5	1 08-7 1 08-9 1 09-2 1 09-4 1 09-7	1 05-9 1 06-1 1 06-3	3-4 0-3 3-5 0-3 3-6 0-3 3-7 0-3 3-8 0-3 3-9 0-3	9-5 0-1 3 9-6 0-1 3 9-7 0-1 5 9-8 0-1	7 15.5 1.2 7 15.6 1.2 7 15.7 1.2 7 15.8 1.2	35 36 37 38	1 23-8	1 24-0 1 24-2 1 24-5 1 24-7 1 25-0	1 19-9 1 20-2 1 20-4 1 20-7 1 20-9	3-5 0-3 3-6 0-3 3-7 0-3 3-8 0-3 3-9 0-4	9-6 0-9 9-7 0-9 9-8 0-9	15-5 1-4 15-6 1-4 15-7 1-4 15-8 1-4 15-9 1-5	33 33 34 44	6 13 7 13 8 13 9 13	19-0 19-3 19-5 19-8	1 39-0 1 39-3 1 39-5 1 39-8 1 40-0 1 40-3	1 34-3 1 34-5 1 34-7 1 35-0 1 35-2 1 35-4	3.5 0.4 3.6 0.4 3.7 0.4 3.8 0.4 3.9 0.4 4.0 0.4	9-5 1-0 9-6 1-0 9-7 1-1 9-8 1-1 9-9 1-1	15·5 1·7 15·6 1·7 15·7 1·7 15·8 1·7 15·9 1·7	35 36 37 38 39 40	1 53-8 1 54-0 1 54-3 1 54-5 1 54-8	1 54-1 1 54-3 1 54-6 1 54-8 1 55-1	1 48-6 1 48-8 1 49-0 1 49-3 1 49-5	3·5 0·4 3·6 0·5 3·7 0·5 3·8 0·5 3·9 0·5	9-5 1 9-6 1 9-7 1 9-8 1 9-9 1	2 15-6 2 15-7 2 15-8 2 15-9	2-0 2-0 2-0 2-0
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00 01 02 03 04	00-0 200-3 200-5 200-8 201-0	2 00-3 2 00-6 2 00-8 2 01-1 2 01-3	0 , 1 54-5 1 54-8 1 55-0, 1 55-2 1 55-5	0·1 0·2 0·3	, 0-0 0-0 0-0 0-0 0-1	6-0 6-1 6-2 6-3 6-4	, 09 09 09 09	12-0 12-1 12-2 12-3 12-4	, 1·7 1·7 1·7 1·7 1·8		00 01 02 03 04	2 15-0 2 15-3 2 15-5 2 15-8 2 16-0	2 15-4 2 15-6 2 15-9 2 16-1 2 16-4	2 08-9 2 09-1 2 09-3 2 09-6 2 09-8	0.0 0.0 0.1 0.0 0.2 0.0 0.3 0.0 0.4 0.0	0 6	6-0 1-0 6-1 1-0 6-2 1-0 6-3 1-0 6-4 1-0	12-0 12-1 12-2 12-3 12-4	, 19 19 19 19	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	s 00 20 11 22 12 13 22 13 22 13
05 06 07 08 09	2 01·3 2 01·5 2 01·8 2 02·0 2 02·3	2 01-6 2 01-8 2 02-1 2 02-3 2 02-6	1 55-7 1 56-0 1 56-2 1 56-4 1 56-7	0+6 0+7 0+8	0·1 0·1 0·1 0·1 0·1	6+5 6+6 6+7 6+8 6+9	0.9 0.9 0.9 1.0 1.0	12·5 12·6 12·7 12·8 12·9	1-8 1-8 1-8 1-8		05 06 07 08 09	2 16-3 2 16-5 2 16-8 2 17-0 2 17-3	2 16-6 2 16-9 2 17-1 2 17-4 2 17-6	2 10·0 2 10·3 2 10·5 2 10·8 2 11·0	0.5 O- 0.6 O- 0.7 O- 0.8 O- 0.9 O-	1 6	5-5 1-0 5-6 1-0 5-7 1-1 5-8 1-1 5-9 1-1	12·5 12·6 12·7 12·8 12·9	2·0 2·0 2·0 2·0 2·0 2·0	0: 0: 0: 0: 0:	5 2 6 2 7 2 8 2
10 11 12 13 14	2 02·5 2 02·8 2 03·0 2 03·3 2 03·5	2 02-8 2 03-1 2 03-3 2 03-6 2 03-8	1 56-9 1 57-2 1 57-4 1 57-6 1 57-9	1·1 1·2 1·3	0·1 0·2 0·2 0·2 0·2 0·2	7-0 7-1 7-2 7-3 7-4	1.0 1.0 1.0 1.0 1.0	13·0 13·1 13·2 13·3 13·4	18 19 19 19		10 11 12 13 14	2 17-5 2 17-8 2 18-0 2 18-3 2 18-5	2 17-9 2 18-1 2 18-4 2 18-6 2 18-9	2 11-2 2 11-5 2 11-7 2 12-0 2 12-2	1.0 O- 1.1 O- 1.2 O- 1.3 O- 1.4 O-	2 1	7-0 1-1 7-1 1-1 7-2 1-1 7-3 1-2 7-4 1-2	13.0 13.1 13.2 13.3 13.4	2·1 2·1 2·1 2·1 2·1 2·1	09 10 11 12	0 2 1 2 2 2 3 2
15 16 17 18 19	2 03-8 2 04-0 2 04-3 2 04-5 2 04-8	2 04-1 2 04-3 2 04-6 2 04-8 2 05-1	1 58·1 1 58·4 1 58·6 1 58·8 1 59·1	1.6 1.7 1.8 1.9	0·2 0·2 0·2 0·3 0·3	7·5 7·6 7·7 7·8 7·9	1·1 1·1 1·1 1·1	13·5 13·6 13·7 13·8 13·9	19 19 19 20 20		15 16 17 18 19	2 18-8 2 19-0 2 19-3 2 19-5 2 19-8	2 19·1 2 19·4 2 19·6 2 19·9 2 20·1	2 12-4 2 12-7 2 12-9 2 13-1 2 13-4	1.5 0. 1.6 0. 1.7 0. 1.8 0. 1.9 0.	3 7 7 3 7 3 7 3 7 3 7 3 7 3 7 3 7 3 7 3	7·5 1·2 7·6 1·2 7·7 1·2 7·8 1·2 7·9 1·3	13·5 13·6 13·7 13·8 13·9	2·1 2·2 2·2 2·2 2·2 2·2	14 15 16 17 18	5 2 6 2 7 2 8 2
20 21 22 23 24	2 05·0 2 05·3 2 05·5 2 05·8 2 06·0	2 05-3 2 05-6 2 05-8 2 06-1 2 06-3	1 59·3 1 59·5 1 59·8 2 00·0 2 00·3	2·1 2·2 2·3	0·3 0·3 0·3 0·3 0·3	8-0 8-1 8-2 8-3 8-4	1·1 1·1 1·2 1·2 1·2	14-0 14-1 14-2 14-3 14-4	2·0 2·0 2·0 2·0 2·0 2·0		20 21 22 23 24	2 20-0 2 20-3 2 20-5 2 20-8 2 21-0	2 20-4 2 20-6 2 20-9 2 21-1 2 21-4	2 13-6 2 13-9 2 14-1 2 14-3 2 14-6	2-0 0- 2-1 0- 2-2 0- 2-3 0- 2-4 0-	3 4 4 4 4	B-0 1-3 B-1 1-3 B-2 1-3 B-9 1-3 B-4 1-3	14+0 14+1 14+2 14+3 14+4	2-2 2-2 2-2 2-3 2-3	20 21 22 23	0 2 1 2 2 2 3 2
25 26 27 28 29	2 06·3 2 06·5 2 06·8 2 07·0 2 07·3	2 06-6 2 06-8 2 07-1 2 07-3 2 07-6	2 00·5 2 00·7 2 01·0 2 01·2 2 01·5	2•6 2•7 2•8	0-4 0-4 0-4 0-4	8-5 8-6 8-7 8-8 8-9	1·2 1·2 1·2 1·2 1·3	14-5 14-6 14-7 14-8 14-9	2·1 2·1 2·1 2·1 2·1		25 26 27 28 29	2 21-3 2 21-5 2 21-8 2 22-0 2 22-3	2 21-6 2 21-9 2 22-1 2 22-4 2 22-6	2 14-8 2 15-1 2 15-3 2 15-5 2 15-8	2+5 0- 2+6 0- 2+7 0- 2+8 0- 2+9 0-	4 4 4 5 5	8-5 1-3 8-6 1-4 8-7 1-4 8-6 1-4 8-9 1-4	14-5 14-6 14-7 14-8 14-9	2·3 2·3 2·3 2·3 2·3 2·4	24 25 26 27 28	5 2 2 7 2 3 2
30 31 32 33 34	2 07-5 2 07-8 2 08-0 2 08-3 2 08-5	2 07-8 2 08-1 2 08-4 2 08-6 2 08-9	2 01-7 2 01-9 2 02-2 2 02-4 2 02-6	3·1 3·2 3·3	0-4 0-4 0-5 0-5 0-5	9-0 9-1 9-2 9-3 9-4	1·3 1·3 1·3 1·3	15·0 15·1 15·2 15·3 15·4	2·1 2·1 2·2 2·2 2·2		30 31 32 33 34	2 22-5 2 22-8 2 23-0 2 23-3 2 23-5	2 22-9 2 23-1 2 23-4 2 23-6 2 23-9	2 16-0 2 16-2 2 16-5 2 16-7 2 17-0	3+0 0 3+1 0 3+2 0 3+3 0 3+4 0	5 5	9.0 1.4 9.1 1.4 9.2 1.5 9.3 1.5 9.4 1.5	15-0 15-1 15-2 15-3 15-4	24 24 24 24 24	29 30 31 32 33	2 2 2 3 2
35 36 37 38 39	2 08·8 2 09·0 2 09·3 2 09·5 2 09·8	2 09-1 2 09-4 2 09-6 2 09-9 2 10-1	2 02-9 2 03-1 2 03-4 2 03-6 2 03-8	3·6 3·7 3·8	0.5 0.5 0.5 0.5 0.6	9-5 9-6 9-7 9-8 9-9	1·3 1·4 1·4 1·4	15·5 15·6 15·7 15·8 15·9	2·2 2·2 2·2 2·2 2·3		35 36 37 38 39	2 23-8 2 24-0 2 24-3 2 24-5 2 24-8	2 24-1 2 24-4 2 24-6 2 24-9 2 25-1	2 17-2 2 17-4 2 17-7 2 17-9 2 18-2	3-5 0 3-6 0 3-7 0 3-8 0 3-9 0	6 6 6	9-5 1-5 9-6 1-5 9-7 1-5 9-8 1-6 9-9 1-6	15·5 15·6 15·7 15·8 15·9	2·5 2·5 2·5 2·5 2·5	34 35 36 37 38	2 2 2 2
40 41 42 43 44	2 10-0 2 10-3 2 10-5 2 10-8 2 11-0	2 10-4 2 10-6 2 10-9 2 11-1 2 11-4	2 04·1 2 04·3 2 04·6 2 04·8 2 05·0	4-1 4-2 4-3	0-6 0-6 0-6 0-6	10-0 10-1 10-2 10-3 10-4	14 14 15 15	16-0 16-1 16-2 16-3 16-4	2·3 2·3 2·3 2·3 2·3		40 41 42 43 44	2 25-0 2 25-3 2 25-5 2 25-8 2 26-0	2 25-4 2 25-6 2 25-9 2 26-1 2 26-4	2 18-4 2 18-6 2 18-9 2 19-1 2 19-3	4-0 0 4-1 0 4-2 0 4-3 0 4-4 0	6 1 7 1 7 1	0.0 1.6 0.1 1.6 0.2 1.6 0.3 1.6 0.4 1.6	16-0 16-1 16-2 16-3 16-4	2·5 2·5 2·6 2·6 2·6	39 40 41 42 43	2 2 2 2
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50 51 52 53 54	2 12-5 2 12-8 2 13-0 2 13-3 2 13-5	2 12-9 2 13-1 2 13-4 2 13-6 2 13-9	2 06·5 2 06·7 2 06·9 2 07·2 2 07·4	5•1 5•2 5•3	0·7 0·7 0·7 0·8 0·8	11 · 0 11 · 1 11 · 2 11 · 3 11 · 4	1-6 1-6 1-6 1-6	17·0 17·1 17·2 17·3 17·4	2-4 2-4 2-5 2-5		50 51 52 53 54	2 27-5 2 27-8 2 28-0 2 28-3 2 28-5	2 27-9 2 28-2 2 28-4 2 28-7 2 28-9	2 20-8 2 21-0 2 21-3 2 21-5 2 21-7	5-1 0 5-2 0 5-3 0 5-4 0	-8 1 -8 1 -8 1	1.0 1.7 1.1 1.8 1.2 1.8 1.3 1.8 1.4 1.8	17-0 17-1 17-2 17-3 17-4	2·7 2·7 2·7 2·7 2·8	50 51 52 53	2 2 2 2 2
55 56 57 58 59	2 13-8 2 14-0 2 14-3 2 14-5 2 14-8	2 14·1 2 14·4 2 14·6 2 14·9 2 15·1	2 07-7 2 07-9 2 08-1 2 08-4 2 08-6		0-8 0-8 0-8 0-8	11.5 11.6 11.7 11.8 11.9	1-6 1-6 1-7 1-7	17·5 17·6 17·7 17·8 17·9	2·5 2·5 2·5 2·5 2·5		55 56 57 58 59	2 28-8 2 29-0 2 29-3 2 29-5 2 29-8	2 29-2 2 29-4 2 29-7 2 29-9 2 30-2	2 22-0 2 22-2 2 22-5 2 22-7 2 22-9	5-6 0 5-7 0 5-8 0 5-9 0	9 1	1.5 1.8 1.6 1.8 1.7 1.9 1.8 1.9 1.9 1.9	17·5 17·6 17·7 17·8 17·9	2-8 2-8 2-8 2-8 2-8	54 55 56 57 58	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
60	2 15-0	2 15-4	2 08-9	6-0	0.9	12.0	1.7	18-0	2-6]	60	2 30-0	2 30-4	2 23-2	6-0 1	-0 1	12-0 1-9	18+0	2-9	59 60	2

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ıô	SUN PLANETS	ARIES	MOON	or d	Corra	v or d	Corra	v or d	Corrª		ıïı	SUN PLANETS	ARIES	MOON	v or d	Corra	or d	Corr	v or d	Corra
00 01 02 03 04	2 30-0 2 30-3 2 30-5 2 30-8 2 31-0	2 30-4 2 30-7 2 30-9 2 31-2 2 31-4	2 23-2 2 23-4 2 23-6 2 23-9 2 24-1	0.0 0.1 0.2 0.3 0.4	0.0 0.0 0.0 0.0 0.1	6.0 6.1 6.2 6.3 6.4	1·1 1·1 1·1 1·1 1·1	12·0 12·1 12·2 12·3 12·4	2·1 2·1 2·1 2·2 2·2		00 01 02 03 04	0 , 2 45-0 2 45-3 2 45-5 2 45-8 2 46-0	2 45-5 2 45-7 2 46-0 2 46-2 2 46-5	2 37-5 2 37-7 2 38-0 2 38-2 2 38-4	0.0 0.1 0.2 0.3 0.4	0-0 0-0 0-0 0-1 0-1	6-0 6-1 6-2 6-3 6-4	1·2 1·2 1·2 1·2 1·2	12·0 12·1 12·2 12·3 12·4	2·3 2·3 2·3 2·3 2·4 2·4
05 06 07 08 09	2 31·3 2 31·5 2 31·8 2 32·0 2 32·3	2 31.7 2 31.9 2 32.2 2 32.4 2 32.7	2 24-4 2 24-6 2 24-8 2 25-1 2 25-3	0.5 0.6 0.7 0.8 0.9	0·1 0·1 0·1 0·1 0·2	6·5 6·6 6·7 6·8 6·9	1·1 1·2 1·2 1·2 1·2	12-5 12-6 12-7 12-8 12-9	2·2 2·2 2·2 2·2 2·3		05 06 07 08 09	2 46·3 2 46·5 2 46·8 2 47·0 2 47·3	2 46-7 2 47-0 2 47-2 2 47-5 2 47-7	2 38-7 2 38-9 2 39-2 2 39-4 2 39-6	0.5 0.6 0.7 0.8 0.9	0·1 0·1 0·1 0·2 0·2	6·5 6·6 6·7 6·8 6·9	1.2 1.3 1.3 1.3 1.3	12·5 12·6 12·7 12·8 12·9	2-4 2-4 2-4 2-5 2-5
10 11 12 13 14	2 32-5 2 32-8 2 33-0 2 33-3 2 33-5	2 32-9 2 33-2 2 33-4 2 33-7 2 33-9	2 25-6 2 25-8 2 26-0 2 26-3 2 26-5	1.0 1.1 1.2 1.3 1.4	0·2 0·2 0·2 0·2 0·2	7·0 7·1 7·2 7·3 7·4	1·2 1·3 1·3 1·3	13·0 13·1 13·2 13·3 13·4	2·3 2·3 2·3 2·3 2·3		10 11 12 13 14	2 47-5 2 47-8 2 48-0 2 48-3 2 48-5	2 48-0 2 48-2 2 48-5 2 48-7 2 49-0	2 39-9 2 40-1 2 40-3 2 40-6 2 40-8	1.0 1.1 1.2 1.3 1.4	0·2 0·2 0·2 0·2 0·3	7·0 7·1 7·2 7·3 7·4	1·3 1·4 1·4 1·4 1·4	13·0 13·1 13·2 13·3 13·4	2·5 2·5 2·5 2·5 2·6
15 16 17 18 19	2 33-8 2 34-0 2 34-3 2 34-5 2 34-8	2 34-2 2 34-4 2 34-7 2 34-9 2 35-2	2 26-7 2 27-0 2 27-2 2 27-5 2 27-7	1.5 1.6 1.7 1.8 1.9	0·3 0·3 0·3 0·3	7.5 7.6 7.7 7.8 7.9	1·3 1·3 1·3 1·4 1·4	13·5 13·6 13·7 13·8 13·9	24 24 24 24 24		15 16 17 18 19	2 48-8 2 49-0 2 49-3 2 49-5 2 49-8	2 49-2 2 49-5 2 49-7 2 50-0 2 50-2	2 41·1 2 41·3 2 41·5 2 41·8 2 42·0	1.5 1.6 1.7 1.8 1.9	0-3 0-3 0-3 0-3 0-4	7·5 7·6 7·7 7·8 7·9	14 15 15 15	13·5 13·6 13·7 13·8 13·9	2-6 2-6 2-6 2-6 2-7
20 21 22 23 24	2 35-0 2 35-3 2 35-5 2 35-8 2 36-0	2 35-4 2 35-7 2 35-9 2 36-2 2 36-4	2 27-9 2 28-2 2 28-4 2 28-7 2 28-9	2·0 2·1 2·2 2·3 2·4	0-4 0-4 0-4 0-4	8-0 8-1 9-2	14 14 14 15	14-0 14-1 14-2 14-3 14-4	2-5 2-5 2-5 2-5 2-5		20 21 ?2 23 24	2 50-0 2 50-3 2 50-5 2 50-8 2 51-0	2 50-5 2 50-7 2 51-0 2 51-2 2 51-5	2 42·3 2 42·5 2 42·7 2 43·0 2 43·2	2·0 2·1 2·2 2·3 2·4	0-4 0-4 0-4 0-4 0-5	8-0 8-1 8-2 8-3 8-4	1.5 1.6 1.6 1.6 1.6	14-0 14-1 14-2 14-3 14-4	2·7 2·7 2·7 2·7 2·8
25 26 27 28 29	2 36·3 2 36·5 2 36·8 2 37·0 2 37·3	2 36·7 2 36·9 2 37·2 2 37·4 2 37·7	2 29·1 2 29·4 2 29·6 2 29·8 2 30·1	2·5 2·6 2·7 2·8 2·9	0-4 0-5 0-5 0-5 0-5	8-5 8-6 8-7 8-8 8-9	1.5 1.5 1.5 1.5	14-5 14-6 14-7 14-8 14-9	2·5 2·6 2·6 2·6 2·6		25 26 27 28 29	2 51·3 2 51·5 2 51·8 2 52·0 2 52·3	2 51-7 2 52-0 2 52-2 2 52-5 2 52-7	2 43-4 2 43-7 2 43-9 2 44-2 2 44-4	2·5 2·6 2·7 2·8 2·9	0-5 0-5 0-5 0-5	8·5 8·6 8·7 8·8	1-6 1-6 1-7 1-7	14-5 14-6 14-7 14-8 14-9	2-8 2-8 2-8 2-8 2-9
30 31 32 33 34	2 37-5 2 37-8 2 38-0 2 38-3 2 38-5	2 37-9 2 38-2 2 38-4 2 38-7 2 38-9	2 30·3 2 30·6 2 30·8 2 31·0 2 31·3	3·0 3·1 3·2 3·3 3·4	0.5 0.5 0.6 0.6 0.6	9-0 9-1 9-2 9-3 9-4	16 16 16 16 16	15·0 15·1 15·2 15·3 15·4	2-6 2-6 2-7 2-7 2-7		30 31 32 33 34	2 52-5 2 52-8 2 53-0 2 53-3 2 53-5	2 53-0 2 53-2 2 53-5 2 53-7 2 54-0	2 44-6 2 44-9 2 45-1 2 45-4 2 45-6	3·0 3·1 3·2 3·3 3·4	0-6 0-6 0-6 0-6 0-7	9-0 9-1 9-2 9-3 9-4	1.7 1.7 1.8 1.8	15-0 15-1 15-2 15-3 15-4	2·9 2·9 2·9 2·9 3·0
35 36 37 38 39	2 38-8 2 39-0 2 39-3 2 39-5 2 39-8	2 39·2 2 39·4 2 39·7 2 39·9 2 40·2	2 31.5 2 31.8 2 32.0 2 32.2 2 32.5	3·5 3·6 3·7 3·8 3·9	0-6 0-6 0-6 0-7 0-7	9+5 9+6 9+7 9+8 9+9	1.7 1.7 1.7 1.7 1.7	15·5 15·6 15·7 15·8 15·9	2·7 2·7 2·7 2·8 2·8		35 36 37 38 39	2 53-8 2 54-0 2 54-3 2 54-5 2 54-8	2 54-2 2 54-5 2 54-7 2 55-0 2 55-2	2 45-8 2 46-1 2 46-3 2 46-6 2 46-8	3·5 3·6 3·7 3·8 3·9	0·7 0·7 0·7 0·7 0·7	9+5 9+6 9+7 9+8 9+9	1-8 1-8 1-9 1-9	15·5 15·6 15·7 15·8 15·9	3·0 3·0 3·0 3·0 3·0
40 41 42 43 44	2 40-0 2 40-3 2 40-5 2 40-8 2 41-0	2 40-4 2 40-7 2 40-9 2 41-2 2 41-4	2 32-7 2 32-9 2 33-2 2 33-4 2 33-7	4·0 4·1 4·2 4·3 4·4	0-7 0-7 0-7 0-8 0-8	10-0 10-1 10-2 10-3 10-4	1-8 1-8 1-8 1-8	16·0 16·1 16·2 16·3 16·4	2-8 2-8 2-8 2-9 2-9		40 41 42 43 44	2 55-0 2 55-3 2 55-5 2 55-8 2 56-0	2 55-5 2 55-7 2 56-0 2 56-2 2 56-5	2 47-0 2 47-3 2 47-5 2 47-7 2 48-0	4-0 4-1 4-2 4-3 4-4	0-8 0-8 0-8 0-8	10·0 10·1 10·2 10·3 10·4	1.9 1.9 2.0 2.0 2.0	16·0 16·1 16·2 16·3 16·4	3·1 3·1 3·1 3·1 3·1
45 46 47 48 49 50	2 41-3 2 41-5 2 41-8 2 42-0 2 42-3	2 41·7 2 41·9 2 42·2 2 42·4 2 42·7	2 33-9 2 34-1 2 34-4 2 34-6 2 34-9	4-5 4-6 4-7 4-8 4-9	0-8 0-8 0-8 0-8 0-9	10-5 10-6 10-7 10-8 10-9	1-8 1-9 1-9 1-9	16·5 16·6 16·7 16·8 16·9	2-9 2-9 2-9 2-9 3-0		45 46 47 48 49	2 56-3 2 56-5 2 56-8 2 57-0 2 57-3	2 56-7 2 57-0 2 57-2 2 57-5 2 57-7	2 48-2 2 48-5 2 48-7 2 48-9 2 49-2	4-5 4-6 4-7 4-8 4-9	0.9 0.9 0.9 0.9	10·5 10·6 10·7 10·8 10·9	2·0 2·0 2·1 2·1 2·1	16·5 16·6 16·7 16·8 16·9	3·2 3·2 3·2 3·2 3·2
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07	5 31-8	5 32-7	5 16-6	0.6	0.2	6.7	2.5	12.6	4.7	1	06	5 46-5	5 47-4	5 30-7	0-6	0.2	6.6			
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09	5 32-3	5 33-2	5 17-1	0.9	0.3	6.9	2-6	12.9	4-8	1	09	5 47-3	5 48-2	5 31-4	0.9	0.4	6.9		12.9	20
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12	5 33-0	5 33-9	5 17-8	1.2	0.5	7.2	2.7	13-2	5.0	ı	12	5 48-0	5 49-0	5 32-1	1.2	0.5	7.2	2.8	13-1	5·1 5·2
13	5 33-3	5 34-2	5 18-1	1.3	0.5	7-3	2.7	13-3	5-0	ı	13	5 48-3	5 49-2	5 324	1.3	0.5	7-3	2.9	13-3	
14	5 33-5	5 34-4	5 18-3	1-4	0.5	7-4	2-8	13-4	5-0	1	14	5 48-5	5 49-5	5 32-6	1.4	0.5	7.4	2.9	13-4	5.2
15	5 33-8	5 34-7	5 18-5	1.5	0-6	7.5	2.8	13.5	5-1	1	15	5 48-8	5 49-7	5 32-9	1.5	0.6	7.5	2-9	13.5	5.3
16	5 34-0	5 34-9	5 18-8	1.6	0-6	7-6	2.9	13-6	5.1	ı	16	5 49-0	5 50-0	5 33.1	1.6	0.6	7.6	3-0	13-6	5.3
17	5 34-3	5 35-2	5 19-0	1.7	0-6	7-7	2-9	13-7	5.1	ı	17	5 49-3	5 50-2	5 33-3	1.7	0.7	7.7	3-0	13-7	5-4
18	5 34-5	5 35-4	5 19-3	1-8	0.7	7-8	2-9	13-8	5.2	L	18	5 49-5	5 50-5	5 33-6	1.8	0.7	7-8	3-1	13-8	5-4
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20	5 35-0	5 35-9	5 19-7	2.0	0-8	8-0	3-0	14-0	5.3	ı	20	5 50-0	5 51-0	5 34-1	2:0	0-8	8-0	3.1	14-0	5.5
21	5 35-3	5 36-2	5 20-0	5.1	0.8	8-1	3-0	14-1	5.3		21	5 50-3	5 51-2	5 34-3	2.1	0-8	8-1	3.2	14-1	5.5
23	5 35-5 5 35-8	5 36-4 5 36-7	5 20·2 5 20·5	2.2	0.8	8-2	3.1	14-2	5.3	ı	22	5 50-5	5 51-5	5 34-5	2.2	0.9	8-2	3.2	14-2	5.6
24	5 36-0	5 36-9	5 20-5	2-3	0-9	8-3	3·1 3·2	14-3	5-4 5-4		23	5 50-8	5 51.7	5 34-8	2.3	0.9	8-3	3.3	14-3	5-6
25							-					5 51-0	5 52-0	5 35-0	2-4	0.9	8-4	3.3	14-4	5-6
26	5 36·3 5 36·5	5 37-2 5 37-4	5 20-9	2.5	0-9	8-5	3-2	14-5	5-4	1	25	5 51-3	5 52-2	5 35-2	2.5	1.0	8-5	3.3	14-5	5.7
27	5 36-8	5 37-7	5 21·2 5 21·4	2.6	1.0	8-6	3-2	14-6	5·5 5·5	1	26 27	5 51-5	5 52-5	5 35-5	2.6	1.0	8-6	3-4	14-6	5.7
28	5 37-0	5 37-9	5 21-6	2-8	1.1	8-8	3.3	14-8	5-6		28	5 51-8 5 52-0	5 52·7 5 53·0	5 35.7	2-7	1.1	8.7	3-4	14-7	5-8
29	5 37-3	5 38-2	5 21-9	2.9	1.1	8.9	3.3	14-9	5-6		29	5 52-3	5 53-2	5 36-0 5 36-2	2.9	1.1	8-8	3·4 3·5	14-8	5-8 5-8
30	5 37-5	5 38-4	5 22-1	3+0	1.1	9-0	3-4	15-0	5-6		30			120 120 120	1		Call Ca	2000		
31	5 37-8	5 38-7	5 224	3-1	1.2	9-1	34	15-0	5.7		31	5 52-5 5 52-8	5 53·5 5 53·7	5 36-4 5 36-7	3.0	1.2	9-0	3·5 3·6	15-0	5.9
32	5 38-0	5 38-9	5 22-6	3.2	1.2	9-2	3.5	15-2	5.7		32	5 53-0	5 54-0	5 36-9	3.2	1.3	9-2	3-6	15-1	5-9
33	5 38-3	5 39-2	5 22-8	3-3	1.2	9-3	3.5	15-3	5-7		33	5 53-3	5 54-2	5 37-2	3.3	1.3	9-3	3-6	15-3	6-0
34	5 38-5	5 39-4	5 23-1	3-4	1.3	9-4	3-5	15-4	5-8		34	5 53-5	5 54-5	5 37-4	3-4	1.3	9-4	3.7	15-4	6-0
35	5 38-8	5 39-7	5 23-3	3.5	1.3	9-5	3-6	15-5	5-8		35	5 53-8	5 54-7	5 37-6	3-5	1-4	9.5	3.7	15-5	6-1
36	5 39-0	5 39-9	5 23-6	3-6	1-4	9.6	3-6	15-6	5-9		36	5 54-0	5 55-0	5 37-9	3-6	1-4	9.6	3-8	15-6	6.1
37 38	5 39-3	5 40-2	5 23-8	3.7	1-4	9-7	3-6	15-7	5-9		37	5 54-3	5 55-2	5 38-1	3.7	1-4	9-7	3-8	15-7	6.1
39	5 39·5 5 39·8	5 40-4	5 24-0	3-8	1-4	9-8	3.7	15-8	5-9		38	5 54-5	5 55-5	5 38-4	3.8	1.5	9-8	3.8	15-8	6.2
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40	5 40-0	5 40-9	5 24-5	4-0	15	10-0	3-8	16.0	6-0		40	5 55-0	5 56-0	5 38-8	4-0	1.6	10-0	3.9	16-0	6-3
41 42	5 40·3 5 40·5	5 41·2 5 41·4	5 24·7 5 25·0	4-1	1.5	10-1	3-8	16-1	6.0		41	5 55-3	5 56-2	5 39-1	4-1	1.6	10-1	4-0	16-1	6.3
43	5 40-8	5 41-7	5 25-2	4.2		10-2	3-8	16-2	6.1		42 43	5 55-5	5 56-5	5 39-3	4-2	1.6	10-2	4-0	16-2	6.3
44	5 41-0	5 41-9	5 25.5	4.4	2.3	10-4	3-9	16-4	6.2		44	5 55 - 8 5 56-0	5 56·7 5 57·0	5 39·5 5 39·8	4-3	1.7	10-3	4.0	16-3	6-4
45	5 41-3	5 42-2			000 00													4.1	16-4	6-4
46	5 41-5	5 42-2	5 25·7 5 25·9	4.5	1.7	10-5	3-9	16-5	6-2		45 46	5 56-3	5 57-2	5 40-0	4-5	1.8	10-5	4.1	16-5	6-5
47	5 41-8	5 42-7	5 26-2	4.7		10-7	4-0	16-7	6.3		47	5 56-5 5 56-8	5 57·5 5 57·7	5 40·3 5 40·5	4-6	1-8	10.6	4.2	16-6	6.5
48	5 42-0	5 42-9	5 26-4	4-8		10-8	4.1	16-8	6.3		48	5 57-0	5 58-0	5 40-7	4-8	1.9	10.7	4.2	16-7	6.5
49	5 42-3	5 43-2	5 26-7	4-9	1-8	10-9	4-1	16-9	6-3		49	5 57-3	5 58-2	5 41-0	4-9	1.9	10.9	4-3	16.9	6-6
50	5 42-5	5 43-4	5 26-9	5-0	19	11.0	4-1	17-0	6-4	-	50	5 57-5	5 58-5	5 41-2	5-0	2-0	11.0	4.3	17-0	6.7
51	5 42-8	5 43-7	5 27-1		19	11.1	4.2	17-1	6.4	1	51	5 57-8	5 58.7	5 41-5	5-1	2-0	11.1	4.3	17-0	6-7
52	5 43-0	5 43-9	5 27-4	5-2		11-2	4-2	17-2	6.5	1	52	5 58-0	5 59-0	5 41-7	5-2	2-0	11-2	44	17-2	6.7
53	5 43·3 5 43·5	5 44-2	5 27-6	5-3		11.3	4-2	17-3	6.5	- 1	53	5 58-3	5 59-2	5 41-9	5.3	2.1	11-3	4-4	17-3	6-8
		5 44-4	5 27-9	5-4		11-4	4-3	17-4	6.5	1	54	5 58-5	5 59-5	5 42-2	5-4	2.1	11-4	4-5	17-4	6-8
55	5 43-8	5 44-7	5 28-1	5-5		11.5	4-3	17-5	6-6		55	5 58-8	5 59-7	5 42-4	5-5	2.2	11.5	4.5	17-5	6-9
56 57	5 44·0 5 44·3	5 44-9	5 28-3	5-6		11-6	4-4	17-6	6-6		56	5 59-0	6 00-0	5 42-6	5-6	2.2	11.6	4.5	17-6	6.9
58	5 44-5	5 45-2 5 45-4	5 28-6 5 28-8			11.7	44	17-7 17-8	6-6	1	57 58	5 59-3	6 00-2	5 42-9	5.7	2-2	11.7	4-6	17-7	6.9
59	5 44-8	5 45-7	5 29-0				4-5	17-8	6.7	1	59	5 59-5 5 59-8	6 00.5	5 43·1 5 43·4	5-8	2.3	11.8	4-6	17-8	7.0
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05 06 07 08 09	6 01·3 6 01·5 6 01·8 6 02·0 6 02·3	6 02·2 6 02·5 6 02·7 6 03·0 6 03·2	5 44·8 5 45·0 5 45·3 5 45·5 5 45·7	0.5 0.6 0.7 0.8 0.9	0·2 0·3 0·3 0·4	6·5 6·6 6·7 6·8 6·9	2·7 2·7 2·7 2·8 2·8	12·5 12·6 12·7 12·8 12·9	5·1 5·2 5·2 5·3		05 06 07 08 09	6 16-3 6 16-5 6 16-8 6 17-0 6 17-3	6 17·3 6 17·5 6 17·8 6 18·0 6 18·3	5 59·1 5 59·3 5 59·6 5 59·8 6 00·1	0.5 0.6 0.7 0.8 0.9	0·2 0·3 0·3 0·3 0·4	6·5 6·6 6·7 6·8 6·9	2-8 2-8 2-8 2-9 2-9	12·5 12·6 12·7 12·8 12·9	5·3 5·4 5·4 5·5
10 11 12 13 14	6 02·5 6 02·8 6 03·0 6 03·3 6 03·5	6 03-5 6 03-7 6 04-0 6 04-2 6 04-5	5 46·0 5 46·2 5 46·5 5 46·7 5 46·9	1.0 1.1 1.2 1.3 1.4	0·4 0·4 0·5 0·5 0·6	7·0 7·1 7·2 7·3 7·4	2·9 2·9 3·0 3·0	13·0 13·1 13·2 13·3 13·4	5·3 5·3 5·4 5·4 5·5		10 11 12 13 14	6 17·5 6 17·8 6 18·0 6 18·3 6 18·5	6 18-5 6 18-8 6 19-0 6 19-3 6 19-5	6 00·3 6 00·5 6 00·8 6 01·0 6 01·3	1.0 1.1 1.2 1.3 1.4	0.4 0.5 0.5 0.6 0.6	7·0 7·1 7·2 7·3 7·4	3·0 3·0 3·1 3·1 3·1	13·0 13·1 13·2 13·3 13·4	5.5 5.6 5.7 5.7
15 16 17 18 19	6 03-8 6 04-0 6 04-3 6 04-5 6 04-8	6 04-7 6 05-0 6 05-2 6 05-5 6 05-7	5 47-2 5 47-4 5 47-7 5 47-9 5 48-1	1.5 1.6 1.7 1.8 1.9	0·6 0·7 0·7 0·7 0·8	7·5 7·6 7·7 7·8 7·9	3·1 3·1 3·1 3·2 3·2	13·5 13·6 13·7 13·8 13·9	5·5 5·6 5·6 5·7		15 16 17 18 19	6 18·8 6 19·0 6 19·3 6 19·5 6 19·8	6 19-8 6 20-0 6 20-3 6 20-5 6 20-8	6 01.5 6 01.7 6 02.0 6 02.2 6 02.5	1.5 1.6 1.7 1.8 1.9	0·6 0·7 0·7 0·8 0·8	7·5 7·6 7·7 7·8 7·9	3·2 3·3 3·3 3·4	13·5 13·6 13·7 13·8 13·9	5·7 5·8 5·8 5·9 5·9
20 21 22 23 24	6 05-0 6 05-3 6 05-5 6 05-8 6 06-0	6 06-0 6 06-3 6 06-5 6 06-8 6 07-0	5 48-4 5 48-6 5 48-8 5 49-1 5 49-3	2·0 2·1 2·2 2·3 2·4	0.8 0.9 0.9 0.9 1.0	8-0 8-1 8-2 8-3 8-4	3·3 3·3 3·3 3·4 3·4	14·0 14·1 14·2 14·3 14·4	5·7 5·8 5·8 5·8 5·9		20 21 22 23 24	6 20·0 6 20·3 6 20·5 6 20·8 6 21·0	6 21-0 6 21-3 6 21-5 6 21-8 6 22-0	6 02-7 6 02-9 6 03-2 6 03-4 6 03-6	2·0 2·1 2·2 2·3 2·4	0.9 0.9 0.9 1.0 1.0	8·0 8·1 8·2 8·3 8·4	3-4 3-5 3-5 3-6	14-0 14-1 14-2 14-3 14-4	6·0 6·0 6·1 6·1
25 26 27 28 29	6 06·3 6 06·5 6 06·8 6 07·0 6 07·3	6 07-3 6 07-5 6 07-8 6 08-0 6 08-3	5 49-6 5 49-8 5 50-0 5 50-3 5 50-5	2·5 2·6 2·7 2·8 2·9	1·0 1·1 1·1 1·1 1·2	8-5 8-6 8-7 8-8 8-9	3-5 3-5 3-6 3-6 3-6	14·5 14·6 14·7 14·8 14·9	5-9 6-0 6-0 6-1		25 26 27 28 29	6 21-3 6 21-5 6 21-8 6 22-0 6 22-3	6 22-3 6 22-5 6 22-8 6 23-0 6 23-3	6 03-9 6 04-1 6 04-4 6 04-6 6 04-8	2·5 2·6 2·7 2·8 2·9	1·1 1·1 1·1 1·2 1·2	8·5 8·6 8·7 8·8 8·9	3·6 3·7 3·7 3·7 3·8	14-5 14-6 14-7 14-8 14-9	6·2 6·2 6·3 6·3
30 31 32 33 34	6 07-5 6 07-8 6 08-0 6 08-3 6 08-5	6 08-5 6 08-8 6 09-0 6 09-3 6 09-5	5 50-8 5 51-0 5 51-2 5 51-5 5 51-7	3·0 3·1 3·2 3·3 3·4	1·2 1·3 1·3 1·3 1·4	9-0 9-1 9-2 9-3 9-4	3·7 3·7 3·8 3·8 3·8	15·0 15·1 15·2 15·3 15·4	6·1 6·2 6·2 6·2 6·3		30 31 32 33 34	6 22·5 6 22·8 6 23·0 6 23·3 6 23·5	6 23-5 6 23-8 6 24-0 6 24-3 6 24-5	6 05·1 6 05·3 6 05·6 6 05·8 6 06·0	3·0 3·1 3·2 3·3 3·4	1·3 1·3 1·4 1·4 1·4	9-0 9-1 9-2 9-3 9-4	3-8 3-9 3-9 4-0 4-0	15-0 15-1 15-2 15-3 15-4	6·4 6·5 6·5
35 36 37 38 39	6 08-8 6 09-0 6 09-3 6 09-5 6 09-8	6 09-8 6 10-0 6 10-3 6 10-5 6 10-8	5 52-0 5 52-2 5 52-4 5 52-7 5 52-9	3·5 3·6 3·7 3·8 3·9	1.4 1.5 1.5 1.6 1.6	9-5 9-6 9-7 9-8 9-9	3-9 3-9 4-0 4-0 4-0	15·5 15·6 15·7 15·8 15·9	6-3 6-4 6-5 6-5		35 36 37 38 39	6 23-8 6 24-0 6 24-3 6 24-5 6 24-8	6 24-8 6 25-1 6 25-3 6 25-6 6 25-8	6 06·3 6 06·5 6 06·7 6 07·0 6 07·2	3·5 3·6 3·7 3·8 3·9	1.5 1.5 1.6 1.6 1.7	9·5 9·6 9·7 9·8 9·9	4-0 4-1 4-1 4-2 4-2	15·5 15·6 15·7 15·8 15·9	6.6 6.7 6.7 6.8
40 41 42 43 44	6 10·0 6 10·3 6 10·5 6 10·8 6 11·0	6 11·0 6 11·3 6 11·5 6 11·8 6 12·0	5 53·1 5 53·4 5 53·6 5 53·9 5 54·1	4-0 4-1 4-2 4-3 4-4	1.6 1.7 1.7 1.8 1.8	10·0 10·1 10·2 10·3 10·4	4·1 4·1 4·2 4·2 4·2	16·0 16·1 16·2 16·3 16·4	6·5 6·6 6·7 6·7		40 41 42 43 44	6 25·0 6 25·3 6 25·5 6 25·8 6 26·0	6 26·1 6 26·3 6 26·6 6 26·8 6 27·1	6 07-5 6 07-7 6 07-9 6 08-2 6 08-4	4·0 4·1 4·2 4·3 4·4	1.7 1.7 1.8 1.8 1.9	10·0 10·1 10·2 10·3 10·4	4·3 4·3 4·3 4·4 4·4	16·0 16·1 16·2 16·3 16·4	6-8 6-9 6-9 7-0
45 46 47 48 49	6 11·3 6 11·5 6 11·8 6 12·0 6 12·3	6 12·3 6 12·5 6 12·8 6 13·0 6 13·3	5 54·3 5 54·6 5 54·8 5 55·1 5 55·3	4·5 4·6 4·7 4·8 4·9	1.8 1.9 1.9 2.0 2.0	10·5 10·6 10·7 10·8 10·9	4·3 4·3 4·4 4·4 4·5	16·5 16·6 16·7 16·8 16·9	6·7 6·8 6·8 6·9 6·9		45 46 47 48 49	6 26-3 6 26-5 6 26-8 6 27-0 6 27-3	6 27·3 6 27·6 6 27·8 6 28·1 6 28·3	6 08·7 6 08·9 6 09·1 6 09·4 6 09·6	4·5 4·6 4·7 4·8 4·9	1·9 2·0 2·0 2·0 2·1	10·5 10·6 10·7 10·8 10·9	4·5 4·5 4·6 4·6	16·5 16·6 16·7 16·8 16·9	7·0 7·1 7·1 7·1 7·2
50 51 52 53 54	6 12-5 6 12-8 6 13-0 6 13-3 6 13-5	6 13-5 6 13-8 6 14-0 6 14-3 6 14-5	5 55·5 5 55·8 5 56·0 5 56·2 5 56·5	5-0 5-1 5-2 5-3 5-4	2·0 2·1 2·1 2·2 2·2	11·0 11·1 11·2 11·3 11·4	4-5 4-5 4-6 4-7	17·0 17·1 17·2 17·3 17·4	6-9 7-0 7-0 7-1 7-1		50 51 52 53 54	6 27-5 6 27-8 6 28-0 6 28-3 6 28-5	6 28-6 6 28-8 6 29-1 6 29-3 6 29-6	6 09·8 6 10·1 6 10·3 6 10·6 6 10·8	5·0 5·1 5·2 5·3 5·4	2·1 2·2 2·2 2·3 2·3	11.0 11.1 11.2 11.3 11.4	4·7 4·7 4·8 4·8 4·8	17-0 17-1 17-2 17-3 17-4	7·2 7·3 7·3 7·4 7·4
55 56 57 58 59	6 13-8 6 14-0 6 14-3 6 14-5 6 14-8	6 14-8 6 15-0 6 15-3 6 15-5 6 15-8	5 56·7 5 57·0 5 57·2 5 57·4 5 57·7	5+5 5+6 5+7 5+8 5+9	2·2 2·3 2·3 2·4 2·4	11.5 11.6 11.7 11.8 11.9	4.7 4.7 4.8 4.8 4.9	17·5 17·6 17·7 17·8 17·9	7·1 7·2 7·2 7·3 7·3		55 56 57 58 59	6 28-8 6 29-0 6 29-3 6 29-5 6 29-8	6 29·8 6 30·1 6 30·3 6 30·6 6 30·8	6 11·0 6 11·3 6 11·5 6 11·8 6 12·0	5·5 5·6 5·7 5·8 5·9	2·3 2·4 2·4 2·5 2·5	11·5 11·6 11·7 11·8 11·9	4-9 4-9 5-0 5-1	17·5 17·6 17·7 17·8 17·9	7-4 7-5 7-5 7-6 7-6
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26	SUN PLANETS	ARIES	MOON	v or d	Corra	or d	Corra	or d	Corra		27	SUN PLANETS	ARIES	моом	or d	Corra	or d	Corr	v or d	Corra
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05 06 07	6 31·3 6 31·5 6 31·8	6 32·3 6 32·6 6 32·8	6 13-4 6 13-7 6 13-9	0-5 0-6 0-7	0·2 0·3 0·3	6·5 6·6 6·7	2·9 2·9 3·0	12·5 12·6 12·7	5-5 5-6 5-6		05 06 07	6 46·3 6 46·5 6 46·8	6 47-4 6 47-6 6 47-9	6 27·7 6 28·0 6 28·2	0·5 0·6 0·7	0·2 0·3 0·3	6·5 6·6 6·7	3·0 3·0 3·1	12·5 12·6 12·7	5-8
08 09	6 32-0 6 32-3	6 33·1 6 33·3	6 14·1 6 14·4	0-8	0-4 0-4	6-8	3-0 3-0	12-8	5·7 5·7		08 09	6 47-0 6 47-3	6 48·1 6 48·4	6 28-5 6 28-7	0-8	0-4 0-4	6-8	3·1 3·2	12-8	5·9 5·9
10 11 12 13	6 32·5 6 32·8 6 33·0 6 33·3	6 33.8 6 34.1 6 34.3	6 14-6 6 14-9 6 15-1 6 15-3	1·0 1·1 1·2	0.4 0.5 0.5	7·0 7·1 7·2 7·3	3·1 3·1 3·2	13·0 13·1 13·2	5·7 5·8 5·8		10 11 12	6 47-5 6 47-8 6 48-0	6 48-6 6 48-9 6 49-1	6 28·9 6 29·2 6 29·4	1·0 1·1 1·2	0·5 0·5 0·6	7·0 7·1 7·2	3·2 3·3 3·3	13·0 13·1 13·2	6-0 6-1
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60	7 15-0	7 16-2	6 55-2	6.0	2.9	12.0	5.7	18-0	8-6	L	60	7 30-0	7 31-2	7 09-5	6.0	3-0	12-0	5-9	18-0	8-9

TABLES FOR INTERPOLATING SUNRISE, MOONRISE, ETC.

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4	30	2	15	0	54	2	4	7	9	II	13	15	16	18	19	21	22	23		22	22
5	00	2	30	I	00	2	5	7	IO	12	14	16	18	20	22	23		-	24	25	26
5	30	2		_				- 1						20	44	43	25	26	27	28	29
6	20	-	40	I		3	5	8	II	13	16	18	20	22	24	26	28	0 29	0 30	0 31	0 32
_	-	3	00	I		3	6	9	12	14	17	20	22	24	26	29	31	32	33		
6	30	3	-	H	18	3	6	IO	13	16	19	22	24	26	29	31	34	36		34	36
7	00	3	30	I	24	3	7	IO	14	17	20	23	26	29	31	34	37		37	38	40
7	30	3	45	I	30	4	7	II	15	18	22	25	28	31	34	72.5	1700	39	41	42	44
8	00	4	-									~5	20	3.	34	37	40	43	44	46	48
_	3262		00		36	4	8	12	16	20	23	27	30	34	37	41	44	0 47	0 48	0 51	0.53
	30	- 5	15	I	42	4	8	13	17	21	25	29	33	36	40	44	48	0 51	0 53	0 56	0 53
•	00	4	30	I	48	4	9	13	18	22	27	31	35	39		47	52	0 55	0 58	1 01	0 58
	30	4	45	I	54	5	9	14	19	24	28	33	38	42	47	51	56	I 00			1 04
0	00	5	00	2	00	5	IO	15	20	25	30	35	-	45	50	55	60	I 05	I 04	I 08	I 12

Table I is for interpolating the L.M.T. of sunrise, twilight, moonrise, etc., for latitude. It is to be entered, in the appropriate column on the left, with the difference between true latitude and the nearest tabular latitude which is less than the true latitude; and with the argument at the top which is the nearest value of the difference between the times for the tabular latitude and the next higher one; the correction so obtained is applied to the time for the tabular latitude, and the next higher one; the correction is to be noted that the interpolation is not linear, so that when using this table it is essential to take out the tabular phenomenon for the latitude less than the true latitude.

TABLE II-FOR LONGITUDE

Long. East or			I	Differ	ence	betw or	een t	he ti	mes date	for g	iven follov	date ving	and	pred (for	cedi	ng d	ate gitu	(for e	ast	longi	tud	e)		-
West	10	m 20	m 30m	40 ¹	50m	60т	IOm	Ih +	30 ^m		1h + 50m		2h	IOm	2h	20 ^m	2h	30 ^m	2h	40 ^m	2h	50 ^m	2h	oon
0	m	m O	m O	m		m	m	m	m	m	m	m	h	m	h	m	h	m	h	m	h	m	h	m
IO	0	1	1	I		0	0	0	0	0	0	0	0	00	0	00	0	00	0	00	0	00	ő	00
20	I	ï	2	2	-	2	2	2	2	3	3	3		04		04		04		04		05		05
30	1	2	2	1	3	3	6	4	5	6	6	7		07		08		08		09		09		IO
40	1	2	3	3	6	5	8	7	7	8	9	10		II		12		12		13		14		15
	1		3	4	U	7	0	9	10	11	12	13		14		16		17		18		19		20
50	I	3	4	6	7	8	10	II	12	14	15	17	0	18	0	19	0	21	0	22		200		
60	2	3	5	7	8	10	12	13	15	17	18	20		22	-	23	-	25	U		0	24		25
70	2	4	6	8	IO	12	14	16	17	19	21	23		25		27		29		27		28		30
80	2	4	7	9	II	13	16	18	20	22	24	27		29		31		- 1		31 36		33		35
90	2	5	7	10	12	15	17	20	22	25	27	30		32		35		33		- 1		38		40
IOO	3	6	8	11	14	17	19	22		-0		- 1						3/		40		42	4	45
IIO	3	6	9	12	15	18	21		25	28	31	33		36		39	0	42	0	44	0	47	0 5	50
120	3	7	10	13	17	20	23	24	27	31	34	37		40		43		46		49	0	52	0	
130	4	7	II	14	18	22	25	27	30	33		40		43		47		50		53	0	57	I	
140	4	8	12	16	19	23	27		32			43		47		51		54	0	58	1	10	1 0	05
	4	100		10	19	23	4/	31	35	39	43	47		51		54	0	58	I	02	1	06	1 1	01
150	4	8	13	17	21	25	29	33	38	42	46	50	0	54	0	58	1	00	I	~ 1		1		
160	4	9	13	18	22	27	31	36	40			53		58		02	I	-	-	07	I	- 1	II	
170	5	9	14	19	24	28	33	38	42			57		OI		06	I			16		16	I 2	
180	5	10	15	20	25	30	35	- K. C.	45			60		05		10		15		20		20	I 2	

Table II is for interpolating the L.M.T. of moonrise, moonset and the Moon's meridian passage for longitude. It is entered with longitude and with the difference between the times for the given date and for the preceding date (in east longitudes) or following date (in west longitudes). The correction is normally added for west longitudes and subtracted for east longitudes, but if, as occasionally happens, the times become earlier each day instead of later, the signs of the corrections must be reversed.

ALTITUDE CORRECTION TABLES 0°-35°- MOON

App. Alt.	0°-4°	5°-9°	10°-14°	15°-19°	20°-24°	25°-29°	30°-34°	App. Alt.
Alt.	Corrn	Corrn	Corrn	Corrn	Corrn	Corrn	Corrn	
,	0/-	5 50'2	10 62'	15 (2'0	20 62:2	25 ₆₀ ′8	30 58.9	00
00	33'8	38.2	02-1	62.8	62.2	60.8	58.9	10
10	35.9	58-5	62.2	62.8	62-1		1,000,000,000,000	20
20	37.8	58.7	62.2	62.8		60.7	58-8	30
30	39.6	58-9	62.3	62.8	62-1	60·7 60·6	58·7 58·6	40
40	41.2	59-1	62.3	62.8	62.0		E 51.72 5.11	50
50	42.6	59-3	62.4	62.7	62.0	60.6	58.5	50
00	1 44.0	6 59.5	11 62.4	16 62.7	21 62-0	26 60·5	31 58-5	00
10	45-2	59.7	62.4	62.7	61.9	60-4	58-4	10
20	46.3	59.9	62.5	62.7	61.9	60.4	58-3	20
30	47.3	60.0	62.5	62.7	61.9	60.3	58-2	30
40	48-3	60.2	62.5	62.7	61.8	60.3	58-2	40
50	49.2	60.3	62.6	62.7	61.8	60.2	58-1	50
	² 50·0	7	12	17 62.7	22 61.7	27 60-1	32 58.0	00
00		60.5	02.0			60.1	57.9	10
10	50.8	60.6	62-6	62.6	61.7		57.8	20
20	51.4	60.7	62.6	62.6	61.6	60.0	57.8	30
30	52.1	60-9	62.7	62.6	61.6	59.9 59.9	57.7	40
40	52.7	61.0	62.7	62.6	61.5	59.9	57.6	50
50	53.3	61.1	62.7	62.6	61.5	20	22	
00	3 53.8	8 61.2	13 62.7	18 62.5	23 61.5	28 59.7	33 57·5	00
10	54-3	61.3	62.7	62.5	61.4	59.7	57-4	10
20	54-8	61-4	62.7	62.5	61.4	59.6	57.4	20
30	55-2		62-8	62.5	61.3	59-6	57-3	30
40	55-6	61.6	62.8	62-4	61.3	59.5	57-2	40
50	56-0		62.8	62-4	61.2	59.4	57-1	50
00	4	0	14 62-8	19 62.4	24 61-2	29 59-3	34 57.0	00
00	30.4	- CEC	62.8	62.4	61-2	59.3	56.9	10
10	56-7			62.3	61-1	59.2	56.9	20
20	57-1	61.9	62-8	62.3	61.0	59.1	56.8	30
30	57-4		62.8		60.9	59.1	56.7	40
40	57-7		62.8	62.2	60.9	59.0	56.6	50
50	57.9	1	62.8	62-2		100000		-
HP	L U	L U	L U	L U	L U	L U	L U	HP
,	0000	10000	10110	05 11	0.6 1.2	0.7 1.3		54-0
54.0	0.3 0.9		0.4 1.0	0.5 1.1			1.2 1.7	54.3
54-3	0.7 1.		1		0.9 1.4	1.1 1.5	1 prompt 31 32	54.0
54.6	1.1 1.4				1.3 1.6	1.4 1.7		1 40 60 60
54.9	1.4 1.0					1.8 1.9		1
55.2	1.8 1.	1.8 1.8	1.9 1.9	1.9 1.9	2.0 2.0	2.1 2.1	2.2 2.2	55-2
55-5	2.2 2.	2.2 2.0	2.3 2.1	2.3 2.1	2.4 2.2	2.4 2.3	2.5 2.4	55-5
55.8	2.6 2.			The state of the same		2.8 2.4	2.9 2.5	55-8
56-1	3.0 2.					3-1 2-6	3.2 2.7	56-1
56.4	3.4 2.					3.5 2.8	3.5 2.9	56.4
56.7	3.7 2.			-		3.8 3.0	3.9 3.0	56.
						4.2 3.2	4-2 3-2	57.0
57.0	4.1 3.	and the second	A AND DESCRIPTION					
57.3	4.5 3.							
57.6	4.9 3.							
57.9	5.3 3.							- 3 CO 25 C
58-2	5.6 4.	5.6 4.0	5-6 4-0	5.6 4.0	5.6 3.9	5.6 3.9		
58-5	6.0 4.	2 6.0 4.2	6.0 4.2	6.0 4.2	6.0 4.1	5.9 4.1	5.9 4.1	58
58-8	6.4 4.			6.3 4.4	6.3 4.3	6.3 4.3	6.2 4.2	
59.1	6.8 4.	Application of the			1 1 1 1 1 1 1 1 1		6.6 4.4	59.
59.4	7.2 4.				1			
59.7	7.5 5.		The state of the s					
-		the sale	0 - 1 - 1					
60.0	7.9 5.			150 700 700				
	8.3 5.			100				
60.3		7 8.7 5.	8.6 5.	8.6 5.6				
60-6	8.7 5			1 2 23 2 3				
60-6 60-9	9.1 5	9 9.0 5.9	9.0 5.9					
60-6		9 9.0 5.9	9.0 5.9	9.3 6.0	9.2 5.9	9-1 5-8	8.9 5.0	61.

D	IP
Ht. of Corr ⁿ Ht. of Eye Eye	Ht. of Corrn Ht. of Eye
m ft. 2-4 - 2'8 8-6 2-8 -2-9 9-2 3-0 3-1 10-5 3-4 -3-3 11-9 3-8 -3-6 13-3 4-3 -3-6 13-3 4-3 -3-6 14-1 4-5 -3-8 15-7 5-0 -3-9 16-5 5-2 -4-0 17-4 18-3 18-3	m ft. 9-5 -5/5 31-5 9-9 -5/5 32-7 10-3 -5-7 33-9 10-6 -5-8 35-1 11-0 -5-9 37-6 11-8 -6-0 38-9 12-2 -6-2 40-1 12-6 -6-3 41-5 13-0 -6-4 42-8 13-4 -6-5 44-2 13-8 -6-6 45-5 14-2 -6-7 48-4 15-1 -6-8 49-8
5.8 -4.2 19.1 6.1 -4.3 20.1 6.3 -4.4 21.1 6.6 -4.5 22.0 6.9 -4.6 22.9 7.2 -4.8 24.9 7.9 -4.9 26.0 8.2 -5.0 27.1 8.5 -5.2 28.1 8.8 -5.2 29.2 9.2 -5.4 30.4 9.5 31.5	15.5 - 6.9 16.0 - 7.0 16.5 - 7.1 16.5 - 7.2 16.5 - 7.2 16.7 - 7.2 17.4 - 7.4 17.9 - 7.4 18.4 - 7.5 18.4 - 7.6 18.8 - 7.6 62.1 19.3 - 7.8 63.8 19.8 - 7.8 66.8 20.4 - 8.0 68.8 21.4 - 70.5

MOON CORRECTION TABLE

The correction is in two parts; the first correction is taken from the upper part of the table with argument apparent altitude, and the second from the lower part, with argument HP, in the same column as that from which the first correction was taken. Separate corrections are given in the lower part for lower (L) and upper (U) limbs. All corrections are to be added to apparent altitude, but 30' is to be subtracted from the altitude of the upper limb.

For corrections for pressure and temperature see page A4.

For bubble sextant observations ignore dip, take the mean of upper and lower limb corrections and subtract 15' from the altitude.

App. Alt. = Apparent altitude = Sextant altitude corrected for index error and dip.

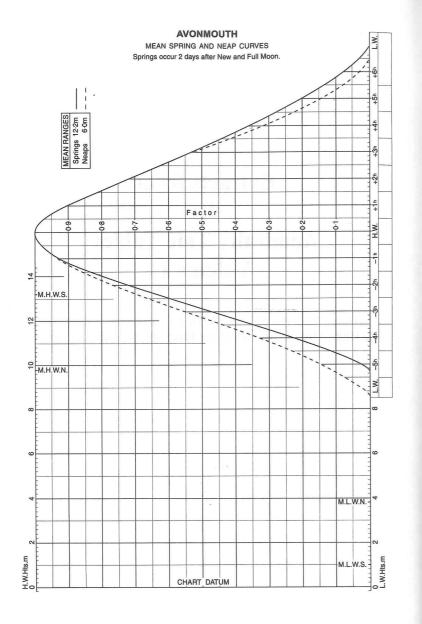
ALTITUDE CORRECTION TABLES 35°-90°- MOON

	_					1011	تابابادد	5 55 -	70 -	MOO	TA	
App. Alt.	35°-39°	40°-44°	45°-49°	50°-54°	55°-59°	60°-64°	65°-69°	70°-74°	75°-79°	80°-84°	85°-89°	App
Alt.	Corrn	Corrn	Corrn	Corrn	Corrn	Corrn	Corrn	Corrn	Corrn	Corrn	Corrn	App. Alt.
oó	35 /-	40	45 -0/-	50°46′9	55 42',	60 ,	65	70 .	75	80 00/5	85	,
10	35 56.5 56.4	53.7	50.5	46.9	43.1	60 38.9	65 34:6	70 30 ¹ 1	75 ₂₅ ′ ₃	20.5	15.6	00
20	56-3	53·6 53·5	50·4 50·2	46·8 46·7	42.9 42.8	38.8	34.4	29.9	25.2	20-4		10
30	56.2	53.4	50-1	46.5	42.7	38·7 38·5	34·3 34·1	29.7 29.6	25·0 24·9	20.2	15.3	20
40	56.2	53.3	50-0	46.4	42.5	38.4	34.0	29.6	24.9	20·0 19·9	15·1 15·0	30 40
50	56-1	53-2	49.9	46.3	42.4	38-2	33.8	29.3	24.5	19.7	14.8	50
00	36 56.0	41 53-1	46 49.8	51 46.2	56 42.3	61 38-1	66 33.7	71 29-1	76 24.4	81 19.6	04	
10	55.9	53.0	49.7	46.0	42.1	37.9	33.7	29.1	24.4	19.6	14.6 14.5	00
20	55-8	52.8	49.5	45.9	42.0	37.8	33.4	28.8	24.1	19.4	14.3	10 20
30	55.7	52.7	49.4	45.8	41.8	37.7	33-2	28.7	23.9	19.1	14.1	30
40	55.6	52.6	49.3	45.7	41.7	37.5	33-1	28.5	23.8	18.9	14-0	40
50	55.5	52.5	49.2	45.5	41.6	37.4	32.9	28.3	23.6	18-7	13.8	50
00	37 55.4	42 52-4	47 49.1	52 45.4	57 41.4	62 37.2	67 32.8	72 _{28·2}	77 23.4	82 18-6	87 13.7	00
10	55.3	52.3	49.0	45.3	41.3	37-1	32.6	28.0	23.3	18-4	13.5	10
20	55-2	52-2	48.8	45-2	41.2	36.9	32.5	27.9	23-1	18-2	13.3	20
30 40	55.1	52.1	48.7	45.0	41.0	36.8	32.3	27-7	22.9	18-1	13-2	30
50	55·0 55·0	52·0 51·9	48.6 48.5	44.9	40.9	36.6	32.2	27.6	22-8	17.9	13-0	40
	20	42	40	44·8 53	40·8 58	36.5	32.0	27.4	22.6	17.8	12.8	50
00 10	54.9 54.8	21.8	48.4	44.6	40.6	30.4	68 31.9	73 _{27·2}	78 _{22·5}	83 17.6	88 12.7	00
20	54.8	51.7 51.6	48·2 48·1	44.5	40.5	36.2	31.7	27-1	22.3	17.4	12.5	10
30	54.6	51.5	48.0	44.4 44.2	40·3 40·2	36·1 35·9	31.6	26.9	22.1	17.3	12.3	20
40	54.5	51.4	47.9	44.1	40.2	35.8	31·4 31·3	26·8 26·6	22·0 21·8	17.1	12.2	30
50	54.4	51.2	47.8	44.0	39.9	35.6	31.1	26.5	21.7	16·9 16·8	12·0 11·8	40 50
00	39 54-3	44 51-1	49 47.6	54 43.9	59 39.8	64 35·5	69 31.0	74 26.3	mo.	9.4	90	
10	54.2	51.0	47.5	43.7	39.6	35.3	30.8	26.3	21·5 21·3	16.6	11.7	00
20	54.1	50.9	47.4	43.6	39.5	35.2	30.7	26.0	21.3	16·5 16·3	11-5 11-4	10 20
30	54.0	50.8	47.3	43.5	39.4	35.0	30.5	25.8	21.0	16.1	11.4	30
40	53.9	50.7	47.2	43.3	39.2	34.9	30.4	25.7	20.9	16.0	11.0	40
50	53.8	50-6	47.0	43.2	39-1	34.7	30-2	25.5	20.7	15.8	10-9	50
HP	L U	L U	L U	L U	L U	L U	L U	L U	L U	L U	L U	HP
,	, ,	, ,	, ,	, ,	, ,	, ,	, ,	, ,	1 1	, ,	, ,	-,
54.0	1.1 1.7	1.3 1.9	1.5 2.1	1.7 2.4	2.0 2.6	2.3 2.9	2.6 3.2	2.9 3.5	3.2 3.8	3.5 4.1	3.8 4.5	54.0
54-3	1.4 1.8	1.6 2.0	1.8 2.2	2.0 2.5	2.3 2.7	2.5 3.0	2.8 3.2	3.0 3.5	3.3 3.8	3.6 4.1	3.9 4.4	54-3
54.6 54.9	1.7 2.0 2.0 2.2	1.9 2.2	2.1 2.4	2.3 2.6	2.5 2.8	2.7 3.0	3.0 3.3	3.2 3.5	3.5 3.8	3.7 4.1	4.0 4.3	54-6
55.2	2.0 2.2	2·2 2·3 2·5 2·4	2·3 2·5 2·6 2·6	2·5 2·7 2·8 2·8	2·7 2·9 3·0 2·9	2·9 3·1 3·2 3·1	3.2 3.3	3.4 3.5	3.6 3.8	3.9 4.0		54.9
					50-100		3.4 3.3	3.6 3.5	3.8 3.7	4.0 4.0	4.2 4.2	55.2
55·5 55·8	2·7 2·5 3·0 2·6	2·8 2·6 3·1 2·7	2.9 2.7	3.1 2.9	3.2 3.0	3.4 3.2		3.7 3.5	3.9 3.7	4.1 3.9		55.5
56.1	3.3 2.8	3.4 2.9	3·2 2·8 3·5 3·0	3·3 3·0 3·6 3·1	3·5 3·1 3·7 3·2	3.6 3.3			4.1 3.7	4.2 3.9		55.8
56.4	3.6 2.9	3.7 3.0		3.9 3.2	3.9 3.3	3·8 3·3 4·0 3·4			4.2 3.7	4.4 3.8		56.1
56.7	3.9 3.1	4.0 3.1	55. YES 755 555	4.1 3.3	4.2 3.3	4.0 3.4			4.4 3.7 4.5 3.7	4·5 3·8 4·6 3·8		56·4 56·7
57.0	4.3 3.2	4.3 3.3			10.000		1					- 1
57.3	4.6 3.4	4.6 3.4		4.4 3.4 4.6 3.5	4.4 3.4 4.7 3.5	4·5 3·5 4·7 3·5			4.7 3.6	4.7 3.7		57.0
57.6	4.9 3.6	4.9 3.6			4.7 3.5	4.7 3.5			4·8 3·6 5·0 3·6	4.8 3.7		57.3
57.9	5.2 3.7	5.2 3.7		5.2 3.7	5.2 3.7	5.1 3.6			5.1 3.6	5·0 3·6 5·1 3·6		57·6 57·9
58-2	5.5 3.9	5.5 3.8			5.4 3.7	5.4 3.7			5.2 3.6		S	58.2
58-5	5.9 4.0	5-8 4-0			5.6 3.8			1	1	1		
58-8	6.2 4.2	6.1 4.1			5.9 3.9	5·6 3·8 5·8 3·8			5.4 3.6 5.5 3.5			58.5
59.1	6.5 4.3	6.4 4.3			6.1 4.0	6.0 3.9			5.7 3.5			58·8 59·1
59.4	6.8 4.5	6.7 4.4			6.4 4.1	6.2 3.9			5.8 3.5			59.4
59.7	7-1 4-6	7.0 4.5			6.6 4.1	6.5 4.0			6.0 3.5			59.7
60.0	7-5 4-8	7.3 4.7	7-2 4-5	7.0 4.4	6.9 4.2	6.7 4.0						
60.3	7.8 5.0				7.1 4.3	6.9 4.1						60·0 60·3
60-6	8-1 5-1				7.3 4.4	7.1 4.2	7000 TO 150 1		6.4 3.4			60.6
60.9	8-4 5-3	The same of the same of			7.6 4.5	7.3 4.2		36.3 97 135	6.6 3.4			60.9
	0 =	0										
61-2	8.7 5.4				7.8 4.5	7.6 4.3	7.3 4.0	7.0 3.7	6.7 3.4	6.4 3.1	6-1 2-8	61.2
61·2 61·5	9.1 5.6											61·2 61·5

xxxv

Extracts from the Admiralty Tide Tables Volume I

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ENGLAND — **PORT OF BRISTOL (AVONMOUTH)**

LAT 51°30'N LONG 2°44'W

								-		00 14	LON	G Z	-0-0 00									
TIME Z	ONE	JT(GMT))				TIM	MES ANI	D HEIG	SHTS C	F HIGI	H AND	LOW V	VATERS	S					Y	EAR 20	02
		JANUA	RY				F	EBRUA	RY				. 1	MARCH	E				-	APRIL		
Time 0246 0820 TU 1513 2049	m 1.3 13.4 1.4 13.1	10	Time 0320 0855 1538 2114	m 1.8 12.5 2.0 12.1	I	Time 0409 0941 1634 2207	14.0	10		12.2	1	7ime 0315 0841 1542 2106	14.5 0.2	16		12.6	1	Time 0407 0940 4 1623 2158	14.0	16	0000	12.2
2 0330 0906 W 1556 2134	1.3 13.4 1.5 13.0	11/	0348 0928 1605 2144	2.1 12.2 2.2 11.8	2 SA	0445 1024 1709 2248	13.7 1.1	17		2.1 11.9 2.1 11.8	2 SA		14.5 0.4	17 su	0341 0909 1551 2121	1.9	2	0434 1016 1643 2232	13.1	17	0348 0939 1602 2152	1.9
3 0411 0951 TH 1637 2219	1.4 13.2 1.6 12.7		0409 0958 1628 2213	2.3 11.8 2.4 11.5	3	0519 1106 1741 2329	13.1	18	0434 1028 1654 2243	2.1 11.6 2.2 11.5	3 su	0430 1003 1649 2224		18		2.0 12.1 2.0 12.1	3		1.8 12.0 2.4 11.4	18 TH	0416 1015 1633 2231	1.9 11.6 2.1 11.6
0451 1037 F 1718 2305	1.7 12.8 1.8 12.3	19	0431 1027 1653 2242	2.4 11.5 2.5 11.2	4 M	0553 1150 1815	1.9 12.2 2.2	19 TU		2.3 11.2 2.5 11.1	4	0458 1041 1713 2300	1.0 13.3 1.5 12.6	19 TU	0409 1000 1625 2215	1.9 11.9 2.0 11.8	4	0526 1129 1 1738 2349	2.6 10.8 3.2 10.3	19	0451 1057 1711 2317	2.2 11.0 2.6 10.9
5 0532 1125 SA 1801 2354	2.0 12.3 2.2 11.7	20 su	0459 1058 1726 2316	2.6 11.1 2.7 10.9	5	0014 0632 1243 1856	11.5 2.6 11.3 3.0	20	0541 1143 1807	2.7 10.7 3.0	5	0525 1119 1739 2338	1.7 12.3 2.2 11.6	20	0436 1033 1655 2251	2.0 11.5 2.2 11.4	5	0608 1224 1826	3.5 9.6 4.1	20	0534 1152 1801	2.9 10.3 3.4
6 0618 1220 SU 1850	2.4 11.7 2.6	21 _M	0535 1136 1806 2358	2.8 10.7 3.0 10.5	6	0112 0723 1354 1954	10.6 3.3 10.5 3.7	21	0008 0627 1241 1903	10.5 3.3 10.1 3.6	6	0557 1202 1813	2.5 11.1 3.1	21 TH	0510 1115 1732 2336	2.3 10.9 2.7 10.8	6	0108 0714 1418 1950	9.3 4.3 9.1 4.7	21 su	0019 0636 1308 1921	10.2 3.6 9.8 4.0
7 0052 0712 M 1327 1949	11.1 2.9 11.2 3.0	22	0620 1226 1856	3.3 10.3 3.4	7	0235 0840 1517 2138	10.1 3.9 10.2 4.0	22	0113 0735 1358 2031	10.0 3.9 9.8 4.0	7	0025 0640 1304 1903	10.5 3.4 10.0 4.0	22	0552 1209 1822	3.0 10.2 3.5	7	0300 0904 1539 2210	9.4 4.4 9.5 4.2	22	0147 0831 1452 2131	10.0 3.8 10.0 3.6
0205 0822 TU 1441 2109	10.7 3.2 11.0 3.3	23	0054 0718 1333 2004	10.1 3.7 10.0 3.7	O	0353 1024 1627 2302	10.2 3.7 10.5 3.5	23	0240 0920 1536 2215	9.9 3.9 10.1 3.5	8	0149 0747 1448 2029	9.6 4.2 9.5 4.6	23	0038 0654 1325 1942	10.1 3.7 9.7 4.1	8	0408 1042 1639 2312	10.1 3.5 10.4 3.2	23	0330 1020 1616 2251	10.6 3.0 11.0 2.6
9 0318 0945 W 1549 2226	10.8 3.2 11.1 3.1	Z4	0207 0838 1453 2129	10.0 3.9 10.1 3.6	9	0458 1132 1728	10.8 3.0 11.1	24	0414 1055 1656 2331	10.6 3.2 11.0 2.7	9 SA	0327 0953 1606 2239	9.6 4.2 9.8 4.0	24 su	0205 0845 1511 2152	9.8 4.0 9.9 3.7	9 TU	0503 1136 1730	11.0 2.5 11.3	24	0441 1129 1716 2353	11.7 2.0 12.2 1.6
10 0422 1055 TH 1650 2329	11.1 2.9 11.5 2.7	4 3	0331 1005 1611 2247	10.3 3.5 10.6 3.1	SU	0002 0553 1228 1819	2.8 11.6 2.3 11.7	25 _M	0523 1208 1758	11.7 2.3 12.1	10 su	0437 1112 1709 2340	10.3 3.3 10.6 3.0	25	0351 1040 1639 2315	10.4 3.2 10.9 2.7	10 w	0001 0549 1225 1812	2.2 11.9 1.8 12.0	25 TH	0537 1227 1807	12.8 1.1 13.2
11 0519 1154 F 1745	11.6 2.4 11.9	SA	0443 1119 1716 2352	11.1 2.9 11.4 2.4	M	0054 0641 1318 1905	2.1 12.2 1.8 12.2	20	0036 0619 1311 1849	1.9 12.8 1.5 13.1	11	0534 1206 1800	11.3 2.4 11.5	20	0505 1154 1740	11.7 2.1 12.2	11	0048 0629 1310 1849	1.6 12.4 1.4 12.5	26	0048 0626 1320 1852	0.9 13.7 0.6 13.9
12 .0023 0609 SA 1247 1834	2.2 12.2 1.9 12.3	21	1222	12.0 2.2 12.3	TU	0142 0723 1405 1946	1.7 12.6 1.5 12.5	Z I	0135 0709 1407 1938	1.2 13.7 0.9 13.8	12	0031 0620 1255 1843	2.1 12.1 1.7 12.2	41	0019 0601 1254 1831	1.7 12.9 1.2 13.2	12 -	0132 0706 1353 1924	1.3 12.6 1.3 12.6	27 SA O	0140 0712 1408 1936	0.4 14.2 0.3 14.2
13 0114 0655 SU 1336 1919	1.8 12.6 1.7 12.5	40	1322	1.8 12.8 1.7 12.9	13	0227 0802 1448 2022	1.5 12.8 1.5 12.5	ZO TH	0228 0756 1458 2023	0.7 14.2 0.4 14.2	13	0119 0701 1341 1922	1.6 12.6 1.3 12.5	ZO TH	0116 0650 1348 1917	1.0 13.8 0.6 14.0		0214 0741 1432 1956	1.3 12.6 1.4 12.6	SU	1451	0.2 14.3 0.3 14.1
M 1422	1.6 12.7 1.6 12.5	29	1417	1.4 13.4 1.3 13.4	II 44	0306 0837 1525 2054	1.5 12.7 1.6 12.4				14 TH	0204 0738 1425 1956	1.3 12.8 1.2 12.6	29 F	1436	0.4 14.4 0.1 14.4	14	0249 0813 1504 2026	1.5 12.5 1.6 12.5	29	0837 1528	0.3 14.1 0.6 13.8
TU 1504	1.6 12.7 1.7 12.4	30 d	1509	1.0 13.8 0.9 13.7	15	1553	1.8 12.5 1.9 12.2				I D	0244 0812 1503 2027	1.3 12.8 1.4 12.6	3U SA	0254 0820 1519 2043	0.1 14.6 0.1 14.4	M G I	1525	1.8 12.3 1.9 12.4	JU TU	1557	0.7 13.5 1.2 13.1
		TH 1	1554	0.8 14.0 0.8 13.7										J I		0.1 14.5 0.3 14.1						

WALES; ENGLAND, WEST COAST

No	. PLACE	Lat. N	Long. W		Vater Zone l		Water	MHWS	MHWN	MLWN	METRES	S) ML S Z ₀ m	
523	PORT OF BRISTOL (AVONMOUTH)	(see p	age 162)	0600 and 1800	1100 and 2300	0300 and 1500	0800 and 2000	13.2	9.8	3.8	1.0		
513	Barry	51 23	3 16	-0030	-0015	-0125	-0030	-1.8	-1.3	+0.2	0.0	6.09	
513a	Flat Holm	51 23	3 07	-0015	-0015	-0045	-0045	-1.3	-1.1	-0.2	+0.2	6.2	
513b 514	Cardiff	51 20 51 27	3 06	-0020 -0015	-0020	-0050	-0050	-1.6 -1.0	-1.2	-0.2	-0.2	6.1	
515	Newport	51 33	2 59	-0020	-0015 -0010	-0100 0000	-0030 -0020	-1.1	-0.6 -1.0	+0.1 -0.6	0.0 -0.7	6.45	
	River Wye										0.,	0.03	
516	Chepstow	51 39	2 40	+0020	+0020	0	0	0	0	0	0	0	
523	PORT OF BRISTOL (AVONMOUTH)	(see p	age 162)	0000 and 1200	0600 and 1800	0000 and 1200	0700 and 1900	13.2	9.8	3.8	1.0		
	England River Severn												
517	Sudbrook	51 35	2 43	+0010	+0010	+0025	+0015	+0.2	+0.1	-0.1	+0.1	6.86	
518	Beachley (Aust)	51 36	2 38	+0010	+0015	+0040	+0025	-0.2	-0.2	-0.5	-0.3	6.42	
519 520	Inward Rocks	51 39	2 37	+0020	+0020	+0105 +0120	+0045	-1.0 -1.9	-1.1 -2.0	-1.4 -2.3	-0.6	5.74	
521	White House	51 40	2 33	+0025	+0025	+0145	+0120	-3.0	-3.1	-3.6	-0.8 -1.0	⊙ 3.94	
522	Berkeley	51 42	2 30	+0030	+0045	+0245	+0220	-38	-3.9	-3.4	0.5		
522a	Sharpness Dock	51 43	2 29	+0030	+0045	+0245	+0245	-3.8	-3.9 -4.2	-3.4 -3.3	-0.5 -0.4	3.44	
522b	Wellhouse Rock	51 44	2 29	+0040	+0055	+0320	+0305	-4.1	-4.4	-3.1	-0.2	3.25	
522c 522d	Epney Minsterworth	51 42 51 50	2 24 2 23	+0130	0	0	0	-9.4 -10.1	0	0	0	0	
522e	Lianthony	51 51	2 21	+0215	0	0	0	-10.1	0	0	0	0	
523	PORT OF BRISTOL (AVONMOUTH) (Royal Portbury Dock)	(see pa	age 162)	0200 and 1400	0800 and 2000	0300 and 1500	0800 and 2000	13.2	9.8	3.8	1.0	6.95	
523a	River Avon	200	200										
523b 524	Shirehampton Sea Mills Cumberland Basin Entrance	51 29	2 41 2 39 2 37	0000 +0005 +0010	+0005 +0010	+0035 +0105 §	+0010 +0030 §	-0.7 -1.4 -2.9	-0.7 -1.5 -3.0	-0.8 -1.7 §	0.0 -0.1 §	0 0	
524a 525	Portishead	51 30 51 27	2 45	-0002	0000	0	0	-0.1	-0.1	0	0	0	
525a	Clevedon		2 52	-0010 0000	-0020 0000	-0025 -0030	-0015 -0030	-0.4 -0.4	-0.2 -0.2	+0.2	+0.1	6.8 6.7	
526 527	English And Welsh Grounds Weston-super-Mare	51 28 51 21	2 59 2 59	-0008 -0020	-0008 -0030	-0030 -0130	-0030 -0030	-0.5 -1.2	-0.8 -1.0	-0.3 -0.8	0.0	6.5 6.1	
528	River Parrett Burnham-on-Sea	51 14	3 00	-0020	-0025	-0030	0000	-2.3	-1.9	-1.4	-1.1†	0	
529	Bridgwater	51 08	3 00	-0015	-0030	+0305	+0455	-8.6	-8.1	§	§	0	
530 531	Hinkley Point	51 13	3 08	-0020	-0025	-0100	-0040	-1.7	-1.4	-0.2	-0.2	6.0	
532	Watchet	51 11 51 13	3 20	-0035 -0037	-0050 -0052	-0145 -0155	-0040 -0045	-1.9 -2.6	-1.5 -1.9	+0.1	+0.1	5.87	
533	Porlock Bay	51 13	3 38	-0045	-0055	-0205	-0050	-3.0	-2.2	-0.1	-0.1	5.62	
534	Lynmouth	51 14	3 49	-0055	-0115	0	0	-3.6	-2.7	0	0	0	
496	MILFORD HAVEN	(see pa	ige 154)	0100 and 1300	0700 and 1900	0100 and 1300	0700 and 1900	7.0	5.2	2.5	0.7		
535	Ilfracombe	51 13	4 07	-0016	-0016	-0041	-0031	+2.3	+1.8	+0.6	+0.3	5.04	
536	Appledore	E4 00	4 40	0000	0000	. 05 : -	05:-		-	200	1900	2000	
537	Appledore	51 03	4 12 4 10	-0020 -0010	-0025 -0015	+0015	-0045 -0015	+0.5	0.0 -0.4	-0.9 -1.2	-0.5 -0.6	3.68	
538	Yelland Marsh	51 05	4 07	-0010	-0015	+0030	-0030	-1.1	-1.8	-2.2	-0.5	0	
539 540	Barnstaple	51 05	4 04	0000	-0015	-0155	-0245	-2.9	-3.8	-2.2	-0.4	0	
	Bideford	51 01	4 12	-0020	-0025	0000	0000	-1.1	-1.6	-2.5	-0.7	0	
541 542	Clovelly	51 00	4 24	-0030	-0030	-0020	-0040	+1.3	+1.1	+0.2	+0.2	0	
542 543	Lundy	51 10 50 50	4 40	-0025 -0040	-0025 -0040	-0020 -0035	-0035 -0045	+1.0	+0.7	+0.2 ⊙	0.0	4.28 ⊙	
544	Boscastle	50 41	4 42	-0045	-0010	-0110	-0100	+0.7	+0.6	+0.2	+0.2	4.02	
544a	Port Isaac	50 35	4 50	-0100	-0100	-0100	-0100	+0.5	+0.6	0.0	+0.2	4.13	
		1200000											
	No land Esh t Maria A		ONAL CH					0 4	0.1.6		_		
A7P		pr. 1	May 1	June 1	July	1 A		Sep. 1	Oct. 1	Nov. 1	Dec.		Jai
476 482a	- 482 +0.1 0.0 0.0 -	pr. 1 ·0.1	May 1 -0.1	June 1 -0.1	July 0.0	1 A	0.0	0.0	0.0	+0.1	+0.1		Jai
	- 482 +0.1 0.0 0.0 - a - 512 0.0 0.0 0.0	pr. 1	May 1	June 1	July	1 Au D I							+1

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